US005691621A

United States Patent [19]

Phuoc et al.

[11] **Patent Number: 5,691,621**

[45] **Date of Patent: *Nov. 25, 1997**

[54] **BATTERY PACK HAVING A PROCESSOR CONTROLLED BATTERY OPERATING SYSTEM**

[75] Inventors: **Duong Var Phuoc**, Eching; **Rudi Wieczorek**, Munich; **Elmar Zeising**, Haindlfing, all of Germany; **Louis W. Hruska**, Northboro, Mass.; **Alwyn H. Taylor**, Wellesley Hills, Mass.; **Daniel D. Friel**, Woburn, Mass.; **Matthew P. Hull**, Jamestown, R.I.

[73] Assignee: **Duracell, Inc.**, Needham, Mass.

[*] Notice: The term of this patent shall not extend beyond the expiration date of Pat. No. 5,652,502.

[21] Appl. No.: **473,341**

[22] Filed: **Jun. 7, 1995**

Related U.S. Application Data

[62] Division of Ser. No. 336,945, Nov. 10, 1994.

[51] **Int. Cl.**[6] **H02J 7/04**

[52] **U.S. Cl.** **320/31**; 320/48; 324/426

[58] **Field of Search** 320/5, 19, 20, 320/22, 30, 35, 48; 324/426; 365/96, 106

[56] **References Cited**

U.S. PATENT DOCUMENTS

3,971,980	7/1976	Jungfer et al. .	
4,238,839	12/1980	Redfern et al.	365/96
4,289,836	9/1981	Lemelson .	
4,333,149	6/1982	Taylor et al. .	
4,377,787	3/1983	Kikuoka et al. .	
4,387,334	6/1983	Loper .	
4,390,841	6/1983	Martin et al. .	
4,392,101	7/1983	Saar et al. .	
4,583,034	4/1986	Martin .	
4,595,880	6/1986	Patil .	
4,677,363	6/1987	Kopmann .	
4,709,202	11/1987	Koenck et al.	320/43
4,725,784	2/1988	Peled et al. .	
4,743,831	5/1988	Young .	
4,746,854	5/1988	Baker et al. .	
4,806,840	2/1989	Alexander et al. .	
4,885,523	12/1989	Koenck .	
4,947,123	8/1990	Minezawa .	
4,949,046	8/1990	Seyfang .	
4,961,043	10/1990	Koenck .	
4,965,738	10/1990	Bauer et al.	364/483
5,027,294	6/1991	Fakruddin et al. .	
5,043,651	8/1991	Tamura .	
5,047,961	9/1991	Simonsen .	
5,180,961	1/1993	Tsujino .	
5,196,779	3/1993	Alexandres et al. .	
5,200,689	4/1993	Interiano et al. .	

(List continued on next page.)

OTHER PUBLICATIONS

Markus Bullinger, "Quick Cahrging with Intelligence–An IC Controls NiCad and NiMH Battery Chargers," *Electronik*, 42, No. 6, Mar. 23, 1993, pp. 74–77.

Patrick Guelle, "Integrated Circuits for Rapid Chargers", *Electronique Radio Plans*, Feb. 1993, No. 543, pp. 57–64.

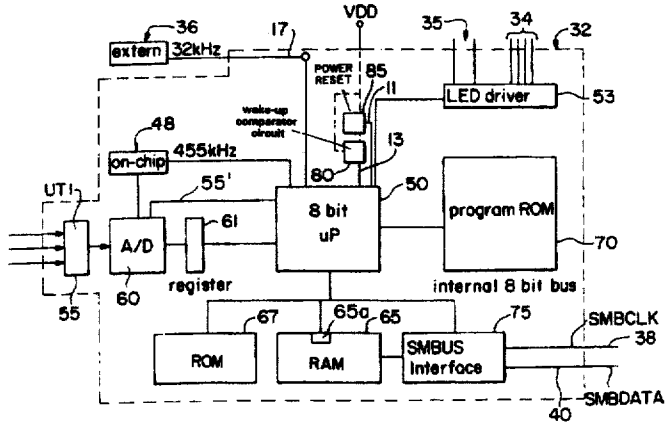
Jacques Robert, et al., "A 16–bit–Low–Voltage CMOS A/D Converter," *IEEE Journal of Solid State Circuits*, vol. SC–22, No. 2, Apr. 1987, pp. 157–159.

Primary Examiner—Peter S. Wong
Assistant Examiner—Gregory J. Toatley, Jr.
Attorney, Agent, or Firm—Scully, Scott, Murphy & Presser

[57] **ABSTRACT**

A battery pack and a method of operating a battery system. The battery pack includes a rechargeable battery and a processor for monitoring the battery during charging and discharging. The processor receives data values representing the battery voltage, temperature and current, and the processor performs a series of calculations using those data values. In one of these calculations, the processor determines the actual full capacity of the battery. Preferably, the processor also keeps track of an uncertainty value that represents an uncertainty in the capacity of the battery; and the processor calculates the actual full capacity of the battery at the end of each discharge cycle if, at that time, the uncertainty value is less than a given percentage of a nominal full capacity of the battery.

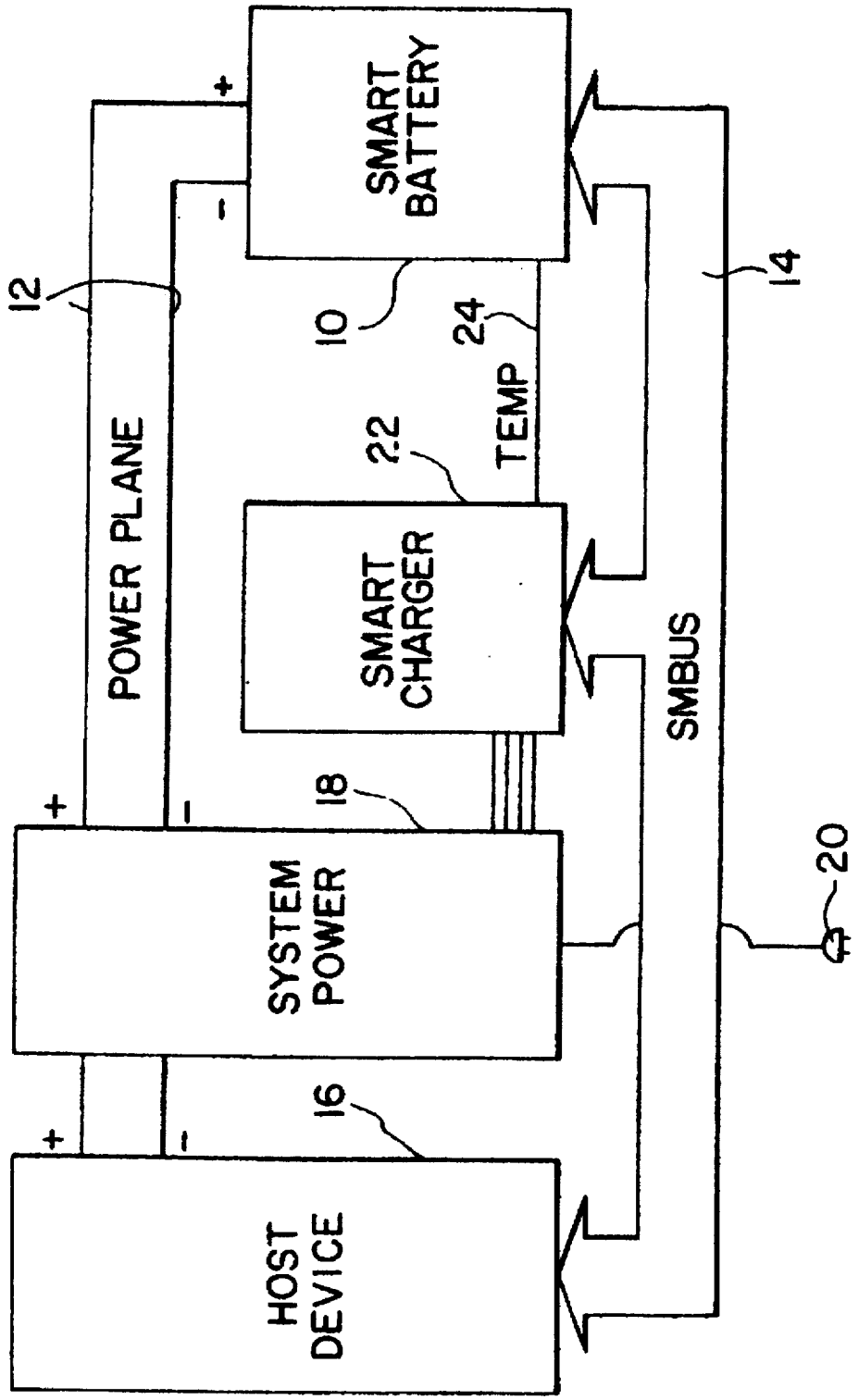
30 Claims, 31 Drawing Sheets



U.S. PATENT DOCUMENTS

5,216,371	6/1993	Nagai .	
5,254,928	10/1993	Young et al. .	
5,278,487	1/1994	Koenck .	
5,284,719	2/1994	Landau et al. .	
5,287,286	2/1994	Ninomiya .	
5,295,078	3/1994	Stich et al.	364/483
5,315,228	5/1994	Hess et al. .	
5,321,627	6/1994	Reher .	
5,325,041	6/1994	Briggs .	
5,341,084	8/1994	Gotoh et al.	320/44
5,349,282	9/1994	McClure .	
5,381,350	1/1995	Fiorina et al. .	

FIG.1


SMART BATTERY
+
-
12
10
24
TEMP
14
22
SMART CHARGER
POWER PLANE
SMBUS
18
+
-
SYSTEM POWER
20
16
+
-
HOST DEVICE

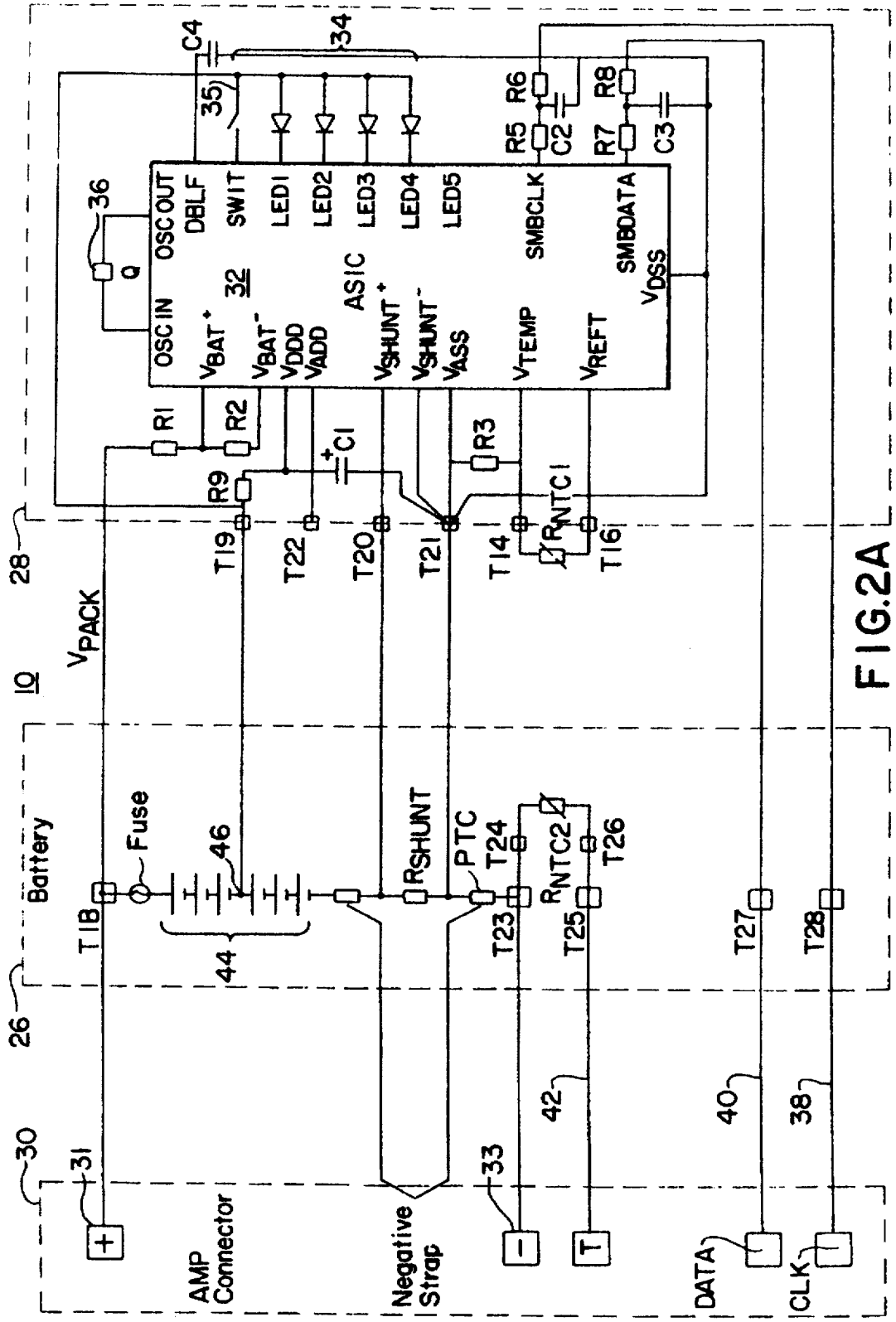
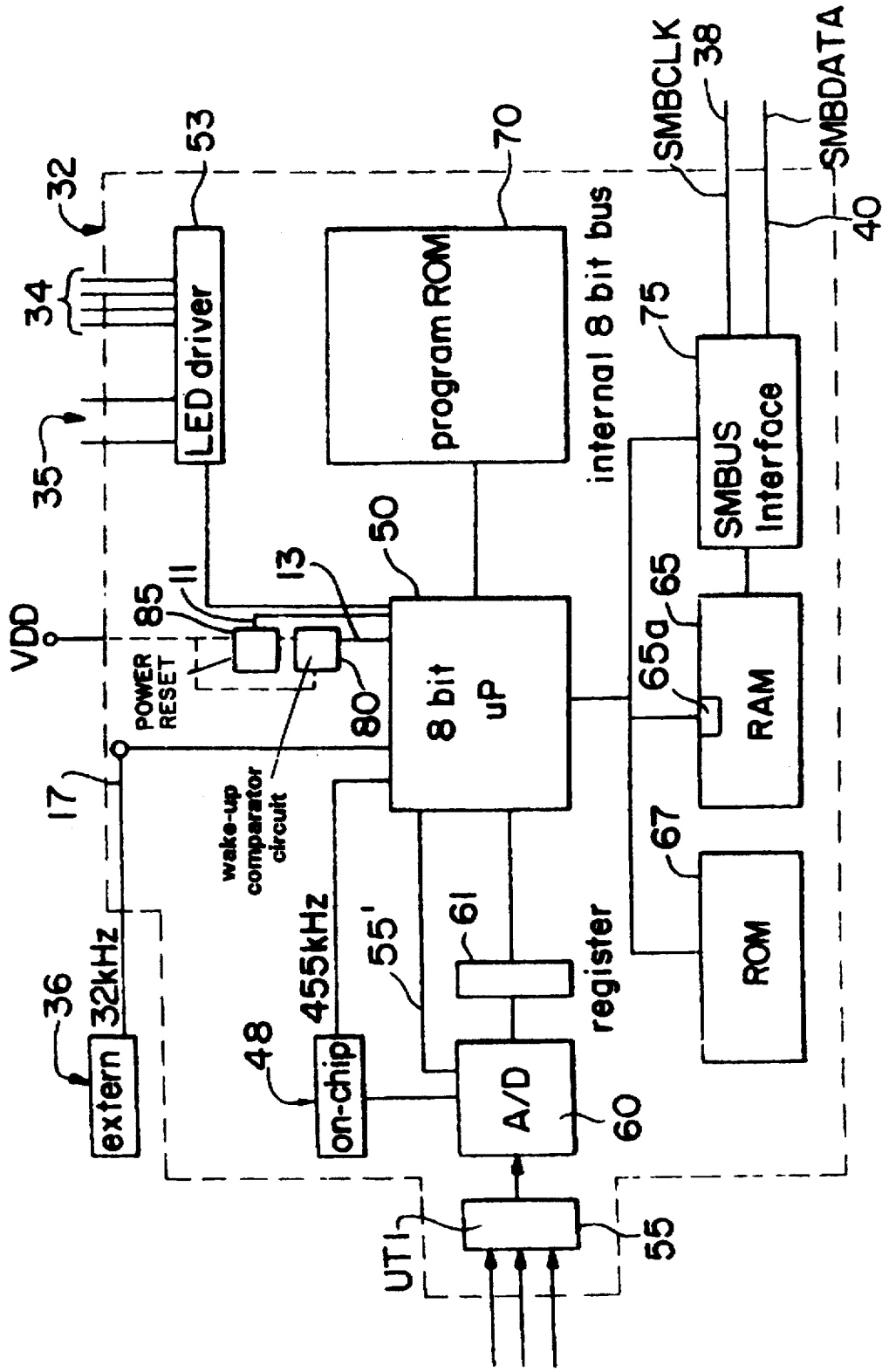

C4
34
35
R6
R8
R5
C2
R7
C3
36
Q
OSCOUT
DBLF
SWIT
LED1
LED2
LED3
LED4
LED5
SMBCLK
SMBDATA
OSCIN
32
ASIC
VBAT+
VBAT-
VDDD
VADD
VSHUNT+
VSHUNT-
VSS
VTEMP
VREFT
VDSS
R1
R2
C1
R3
R9
RNTC1
28
T19
T22
T20
T21
T14
T16
VPACK
10
Battery
Fuse
46
T18
RSHUNT
PTC
T24
RNTC2
T26
44
T23
T25
T27
T28
26
30
31
33
42
40
38
AMP Connector
Negative Strap
DATA
CLK
FIG.2A

FIG. 2B


32
53
70
SMBCLK
38
SMBDATA
34
LED driver
program ROM
internal 8 bit bus
40
35
75
SMBUS Interface
50
13
11
85
VDD
65
65a
POWER RESET
8 bit uP
RAM
80
17
wake-up comparator circuit
67
ROM
61
register
455kHz
55'
36
32kHz
48
extern
on-chip
A/D
60
UTI
55

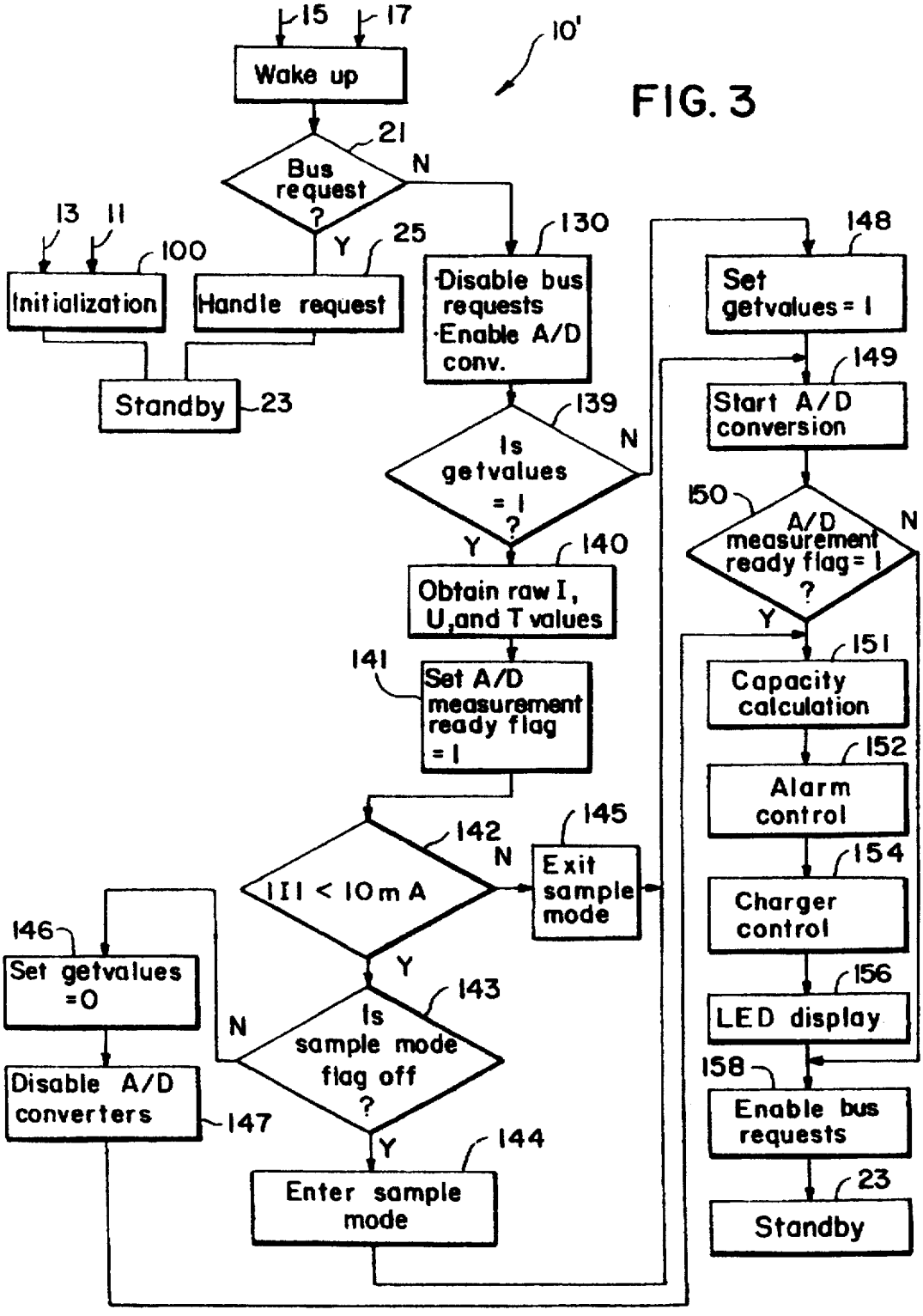

15
17
Wake up
10'
21
Bus request ?
N
Y
13
11
100
Initialization
Handle request
25
Standby
23
130
Disable bus requests
Enable A/D conv.
139
Is getvalues = 1 ?
N
Y
140
Obtain raw I, U, and T values
141
Set A/D measurement ready flag = 1
142
III < 10m A
N
145
Exit sample mode
Y
143
Is sample mode flag off ?
N
Y
144
Enter sample mode
146
Set getvalues = 0
Disable A/D converters
147
148
Set getvalues = 1
149
Start A/D conversion
150
A/D measurement ready flag = 1 ?
N
Y
151
Capacity calculation
152
Alarm control
154
Charger control
156
LED display
158
Enable bus requests
23
Standby

FIG. 3

FIG.4

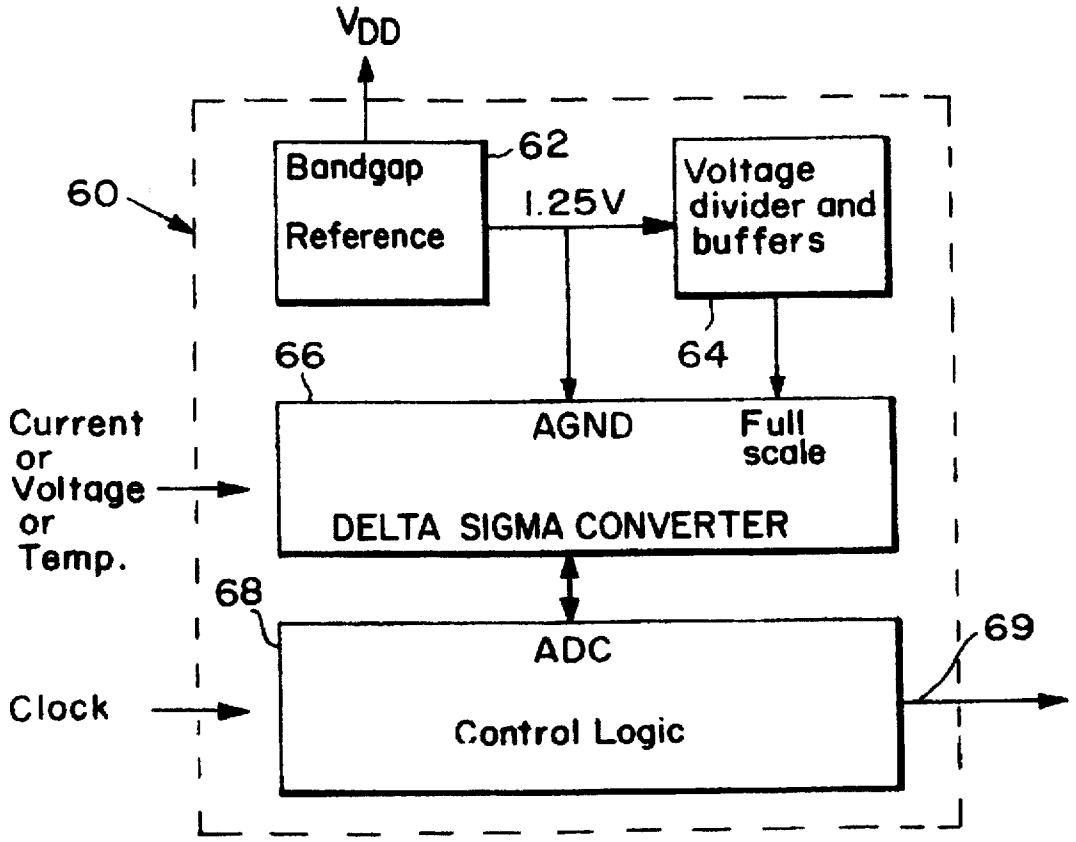


FIG.5A

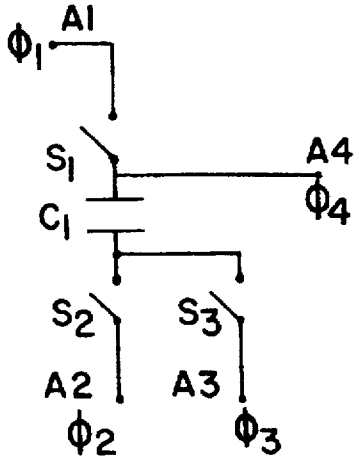


FIG.5B

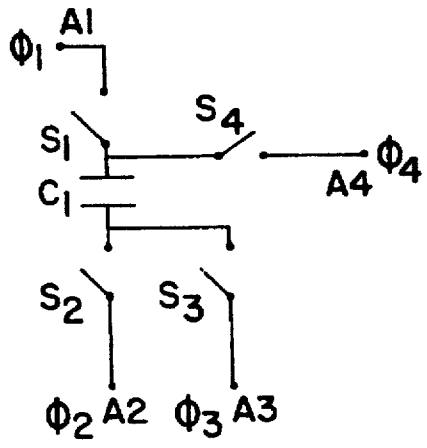


FIG.6

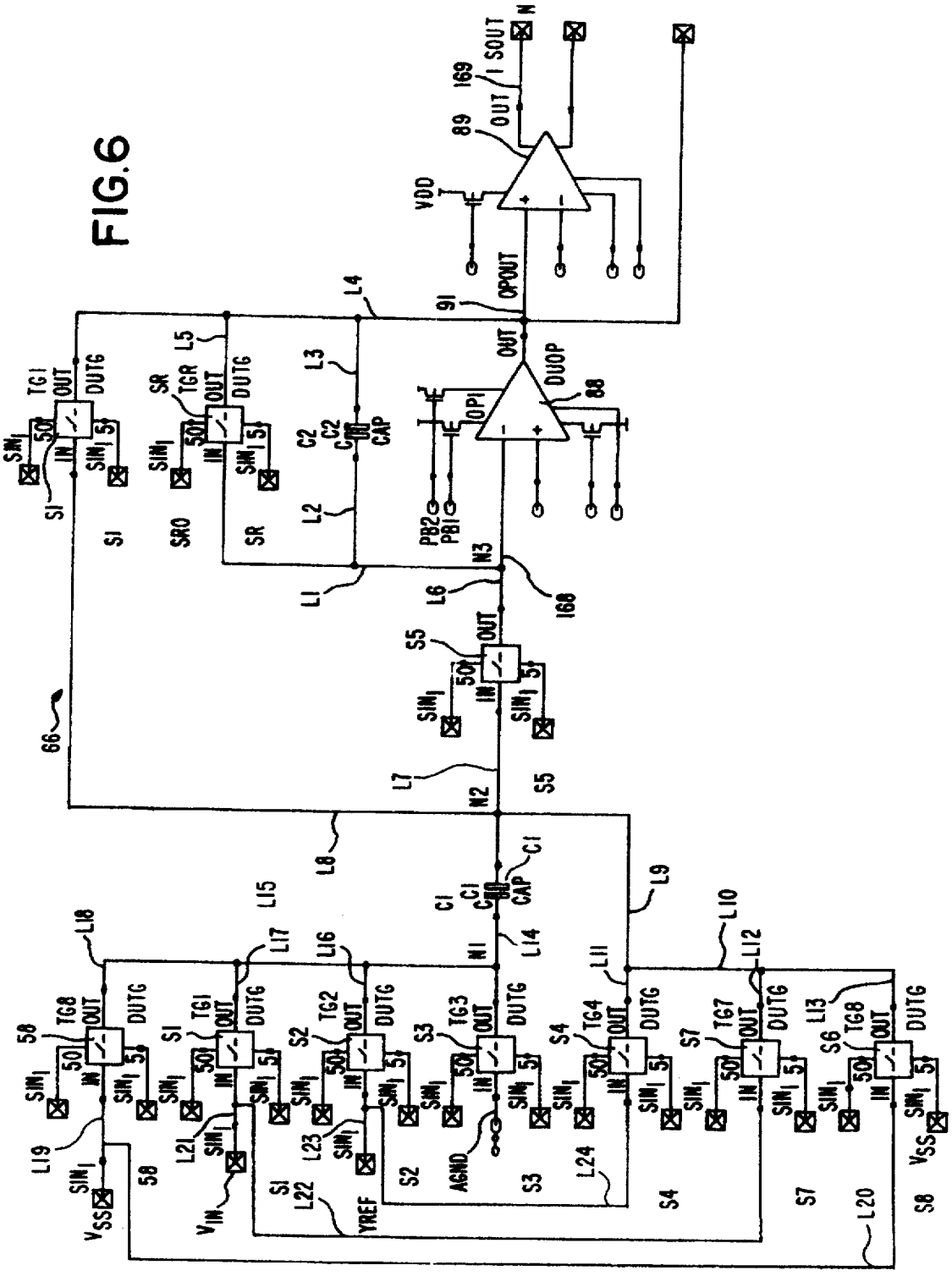

VDD
89
169
I SOUT
N
OUT
OPOUT
91
L4
L5
L3
L2
L1
C2
CAP
SR
SR0
SI
TG1
TG2
TG3
TG4
TG7
TG8
DUTG
IN
OUT
SIN1
50
5Y
OPI
DUOP
88
PB2
PB1
N3
L6
168
S5
66
L7
N2
L8
L9
C1
N1
L14
L10
L11
L12
L13
L15
L16
L17
L18
L19
L21
L22
L23
L24
L20
S1
S2
S3
S4
S6
S7
S8
VSS
VIN
YREF
AGND

FIG. 7

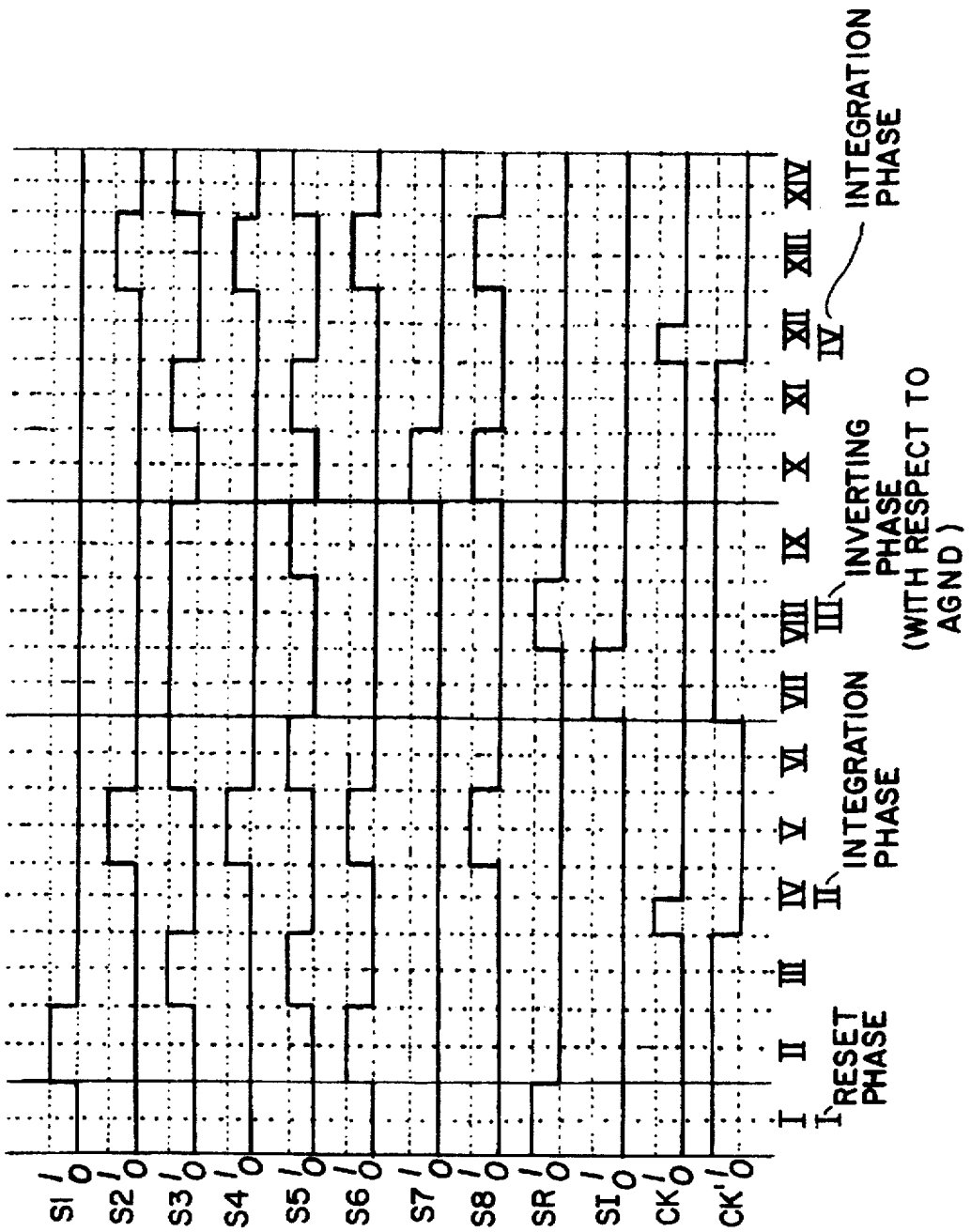

SI
S2
S3
S4
S5
S6
S7
S8
SR
SI
CK
CK'
I
II
III
IV
V
VI
VII
VIII
IX
X
XI
XII
XIII
XIV
RESET PHASE
INTEGRATION PHASE
INVERTING PHASE (WITH RESPECT TO AGND)
INTEGRATION PHASE

FIG.8A

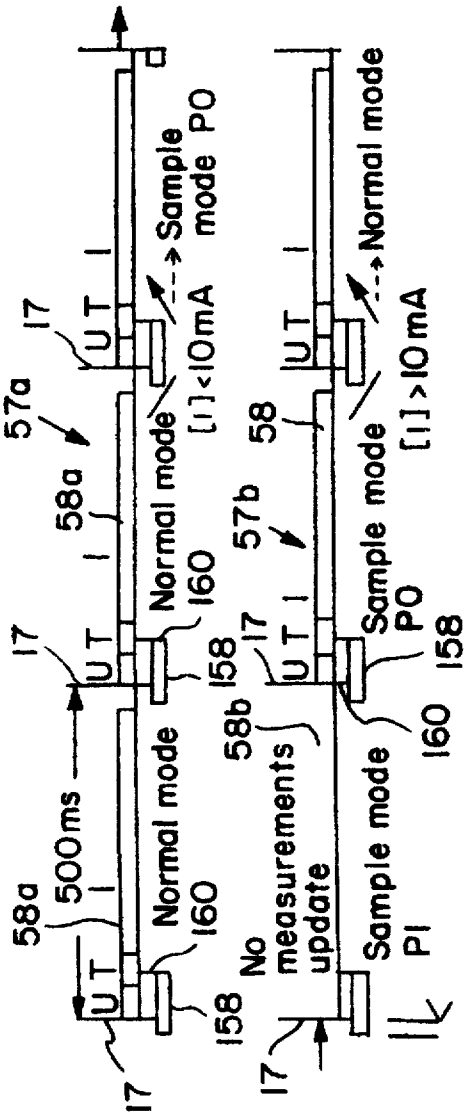
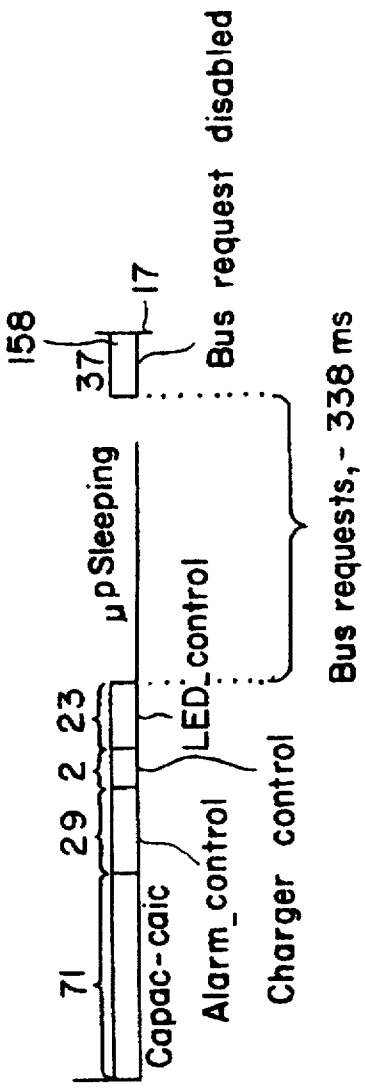

500ms
58a
57a
58a
57b
58
58b
17
158
160
Normal mode
No measurements update
Sample mode
Sample mode P0
Normal mode
[I]<10mA
[I]>10 mA
P0
P1

FIG.8B


158
17
37
Bus request disabled
μp Sleeping
LED_control
Alarm_control
Charger control
Capac-caic
71
29
2
23
Bus requests,- 338 ms

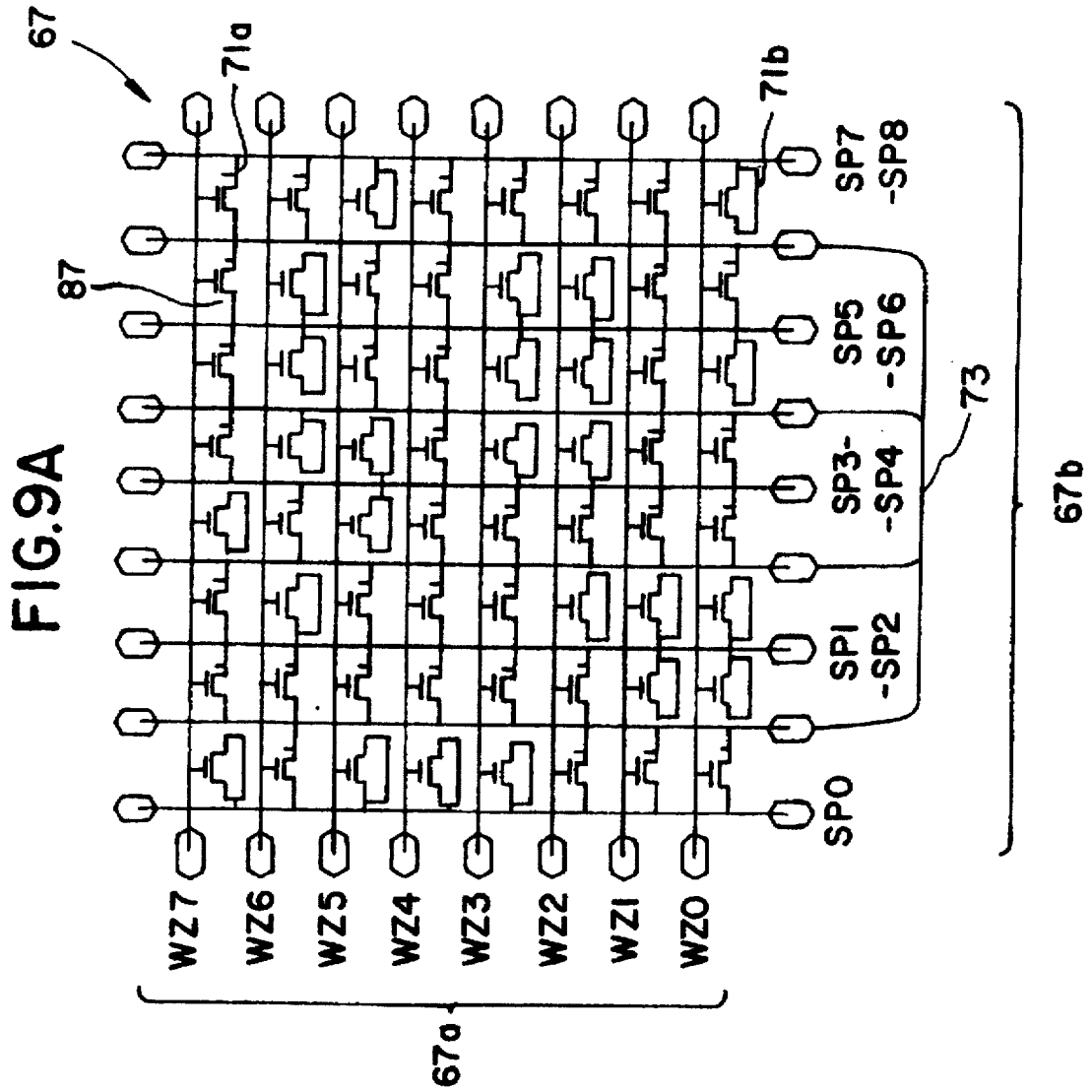

67
71a
71b
87
SP7
-SP8
SP5
-SP6
SP3-
-SP4
SP1
-SP2
SP0
73
67b
WZ7
WZ6
WZ5
WZ4
WZ3
WZ2
WZ1
WZ0
67a

FIG.9A

FIG. 9B
PRIOR ART

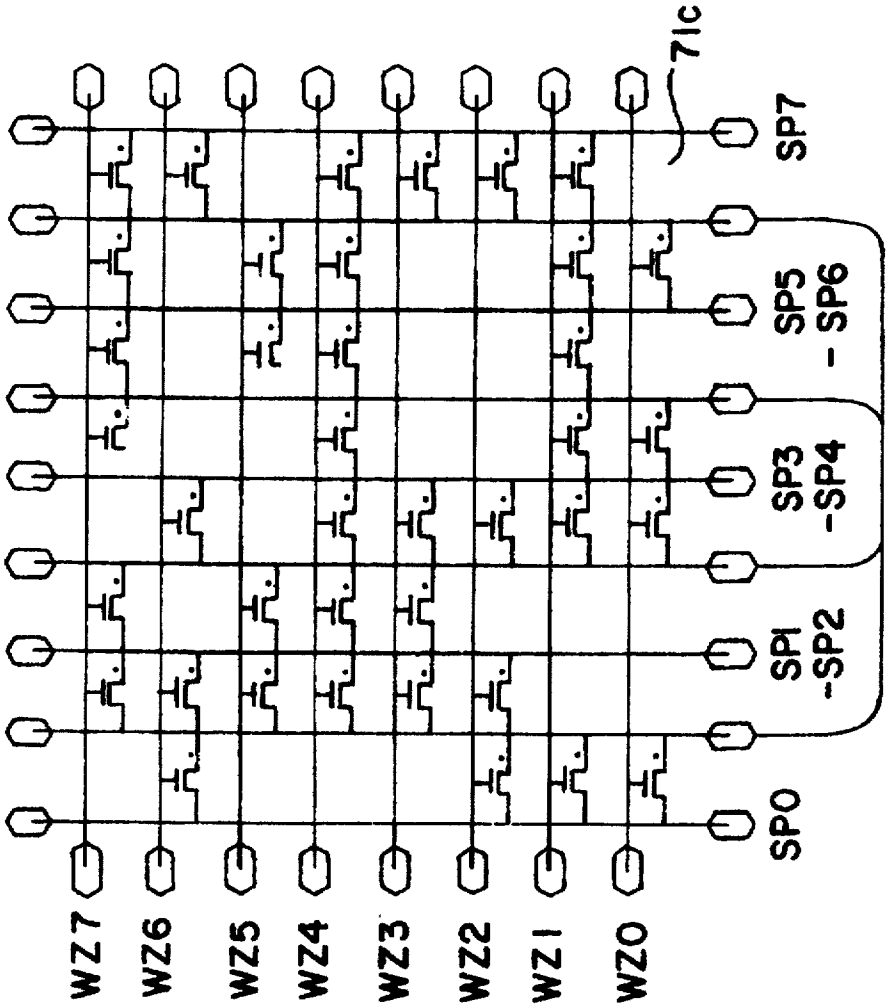


FIG. 10

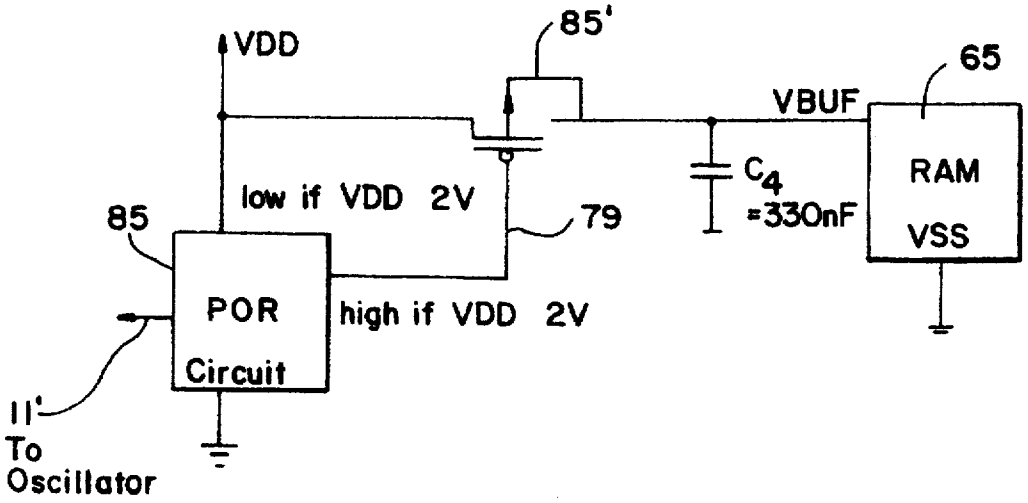

VDD
85'
65
VBUF
low if VDD 2V
79
C_4
=330nF
RAM
VSS
85
POR
Circuit
high if VDD 2V
11'
To
Oscillator

FIG. 11

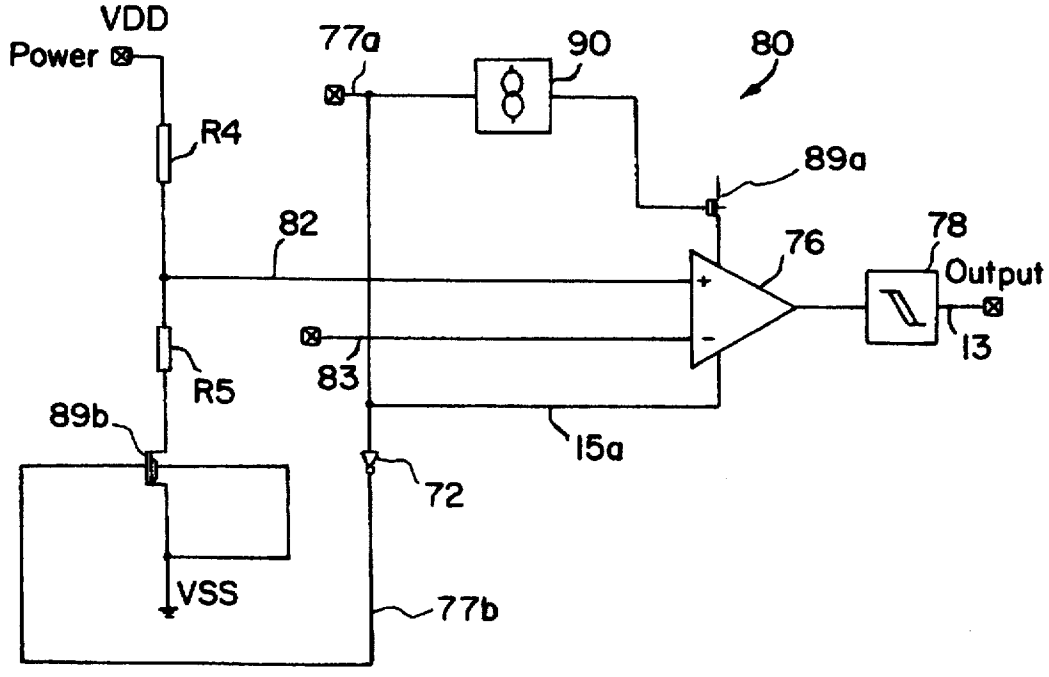

VDD
Power
77a
90
80
R4
89a
82
76
78
Output
13
83
R5
89b
15a
72
VSS
77b

FIG. 12

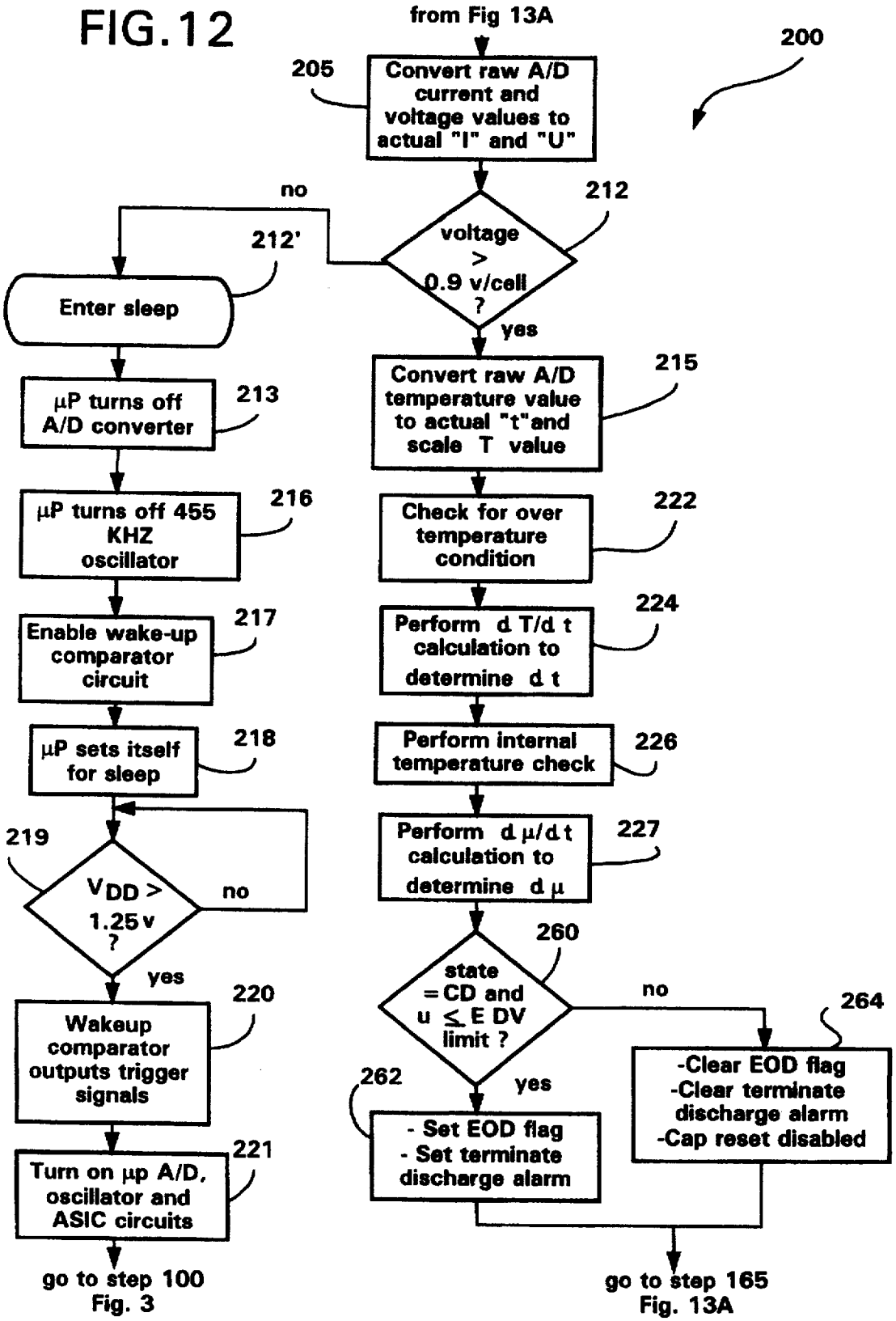

from Fig 13A
200
205
Convert raw A/D current and voltage values to actual "I" and "U"
212
voltage > 0.9 v/cell ?
no
212'
Enter sleep
yes
215
Convert raw A/D temperature value to actual "t" and scale T value
213
μP turns off A/D converter
222
Check for over temperature condition
216
μP turns off 455 KHZ oscillator
224
Perform d T/d t calculation to determine d t
217
Enable wake-up comparator circuit
226
Perform internal temperature check
218
μP sets itself for sleep
227
Perform d μ/d t calculation to determine d μ
219
V_{DD} > 1.25 v ?
no
260
state = CD and u ≤ E DV limit ?
no
264
-Clear EOD flag
-Clear terminate discharge alarm
-Cap reset disabled
yes
262
- Set EOD flag
- Set terminate discharge alarm
yes
220
Wakeup comparator outputs trigger signals
221
Turn on μp A/D, oscillator and ASIC circuits
go to step 100
Fig. 3
go to step 165
Fig. 13A

FIG.13A

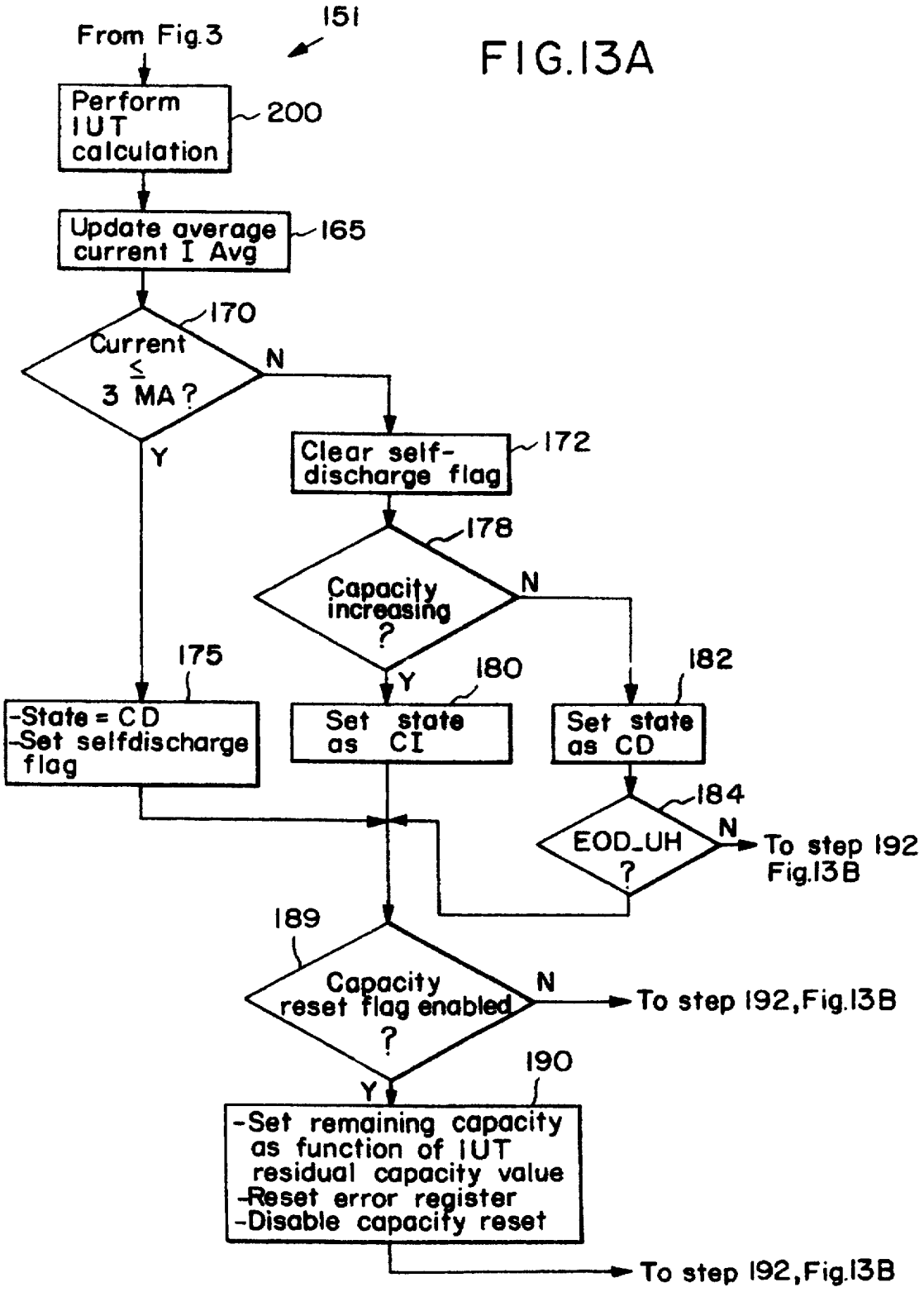

From Fig.3
151
Perform IUT calculation
200
Update average current I Avg
165
Current ≤ 3 MA?
170
N
Y
Clear self-discharge flag
172
Capacity increasing ?
178
N
Y
-State = CD
-Set selfdischarge flag
175
Set state as CI
180
Set state as CD
182
EOD_UH ?
184
N
To step 192 Fig.13B
Capacity reset flag enabled ?
189
N
To step 192,Fig.13B
Y
-Set remaining capacity as function of IUT residual capacity value
-Reset error register
-Disable capacity reset
190
To step 192,Fig.13B

FIG.13B

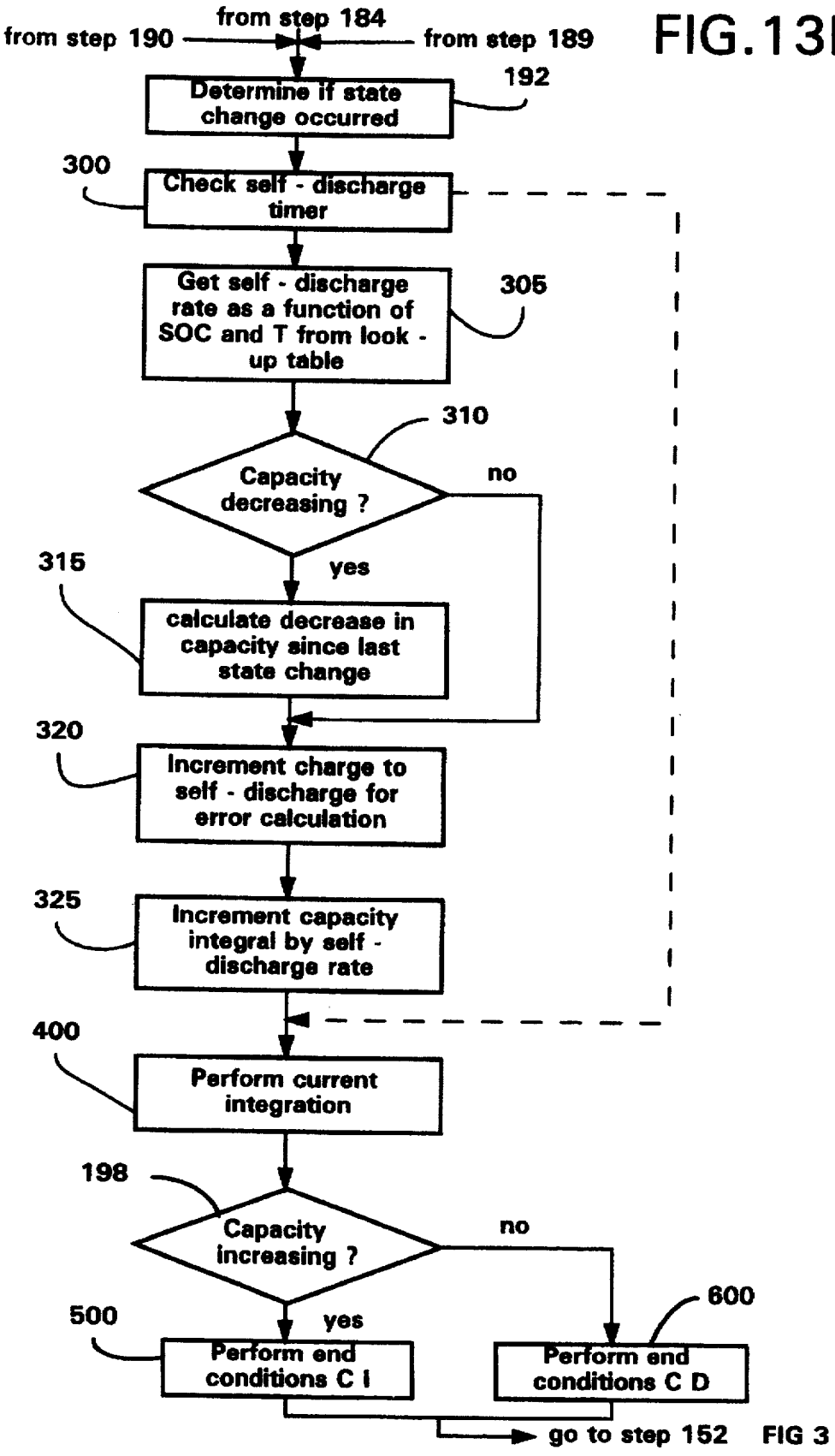

from step 184
from step 190
from step 189
Determine if state change occurred
192
300
Check self - discharge timer
Get self - discharge rate as a function of SOC and T from look - up table
305
310
Capacity decreasing ?
no
yes
315
calculate decrease in capacity since last state change
320
Increment charge to self - discharge for error calculation
325
Increment capacity integral by self - discharge rate
400
Perform current integration
198
Capacity increasing ?
no
yes
500
Perform end conditions C I
600
Perform end conditions C D
go to step 152

FIG 3

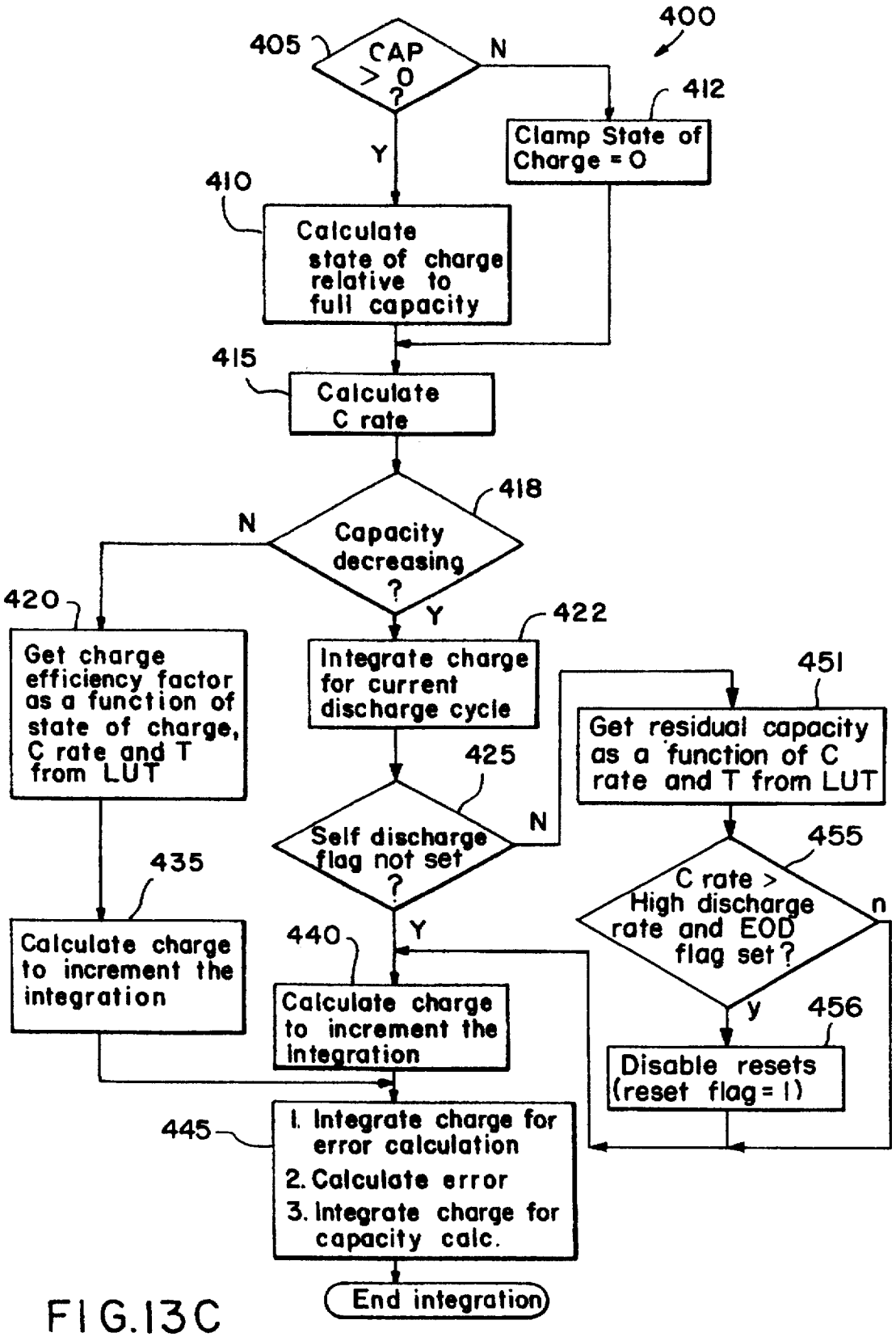

400
405
CAP > 0 ?
N
412
Clamp State of Charge = 0
Y
410
Calculate state of charge relative to full capacity
415
Calculate C rate
418
Capacity decreasing ?
N
Y
420
Get charge efficiency factor as a function of state of charge, C rate and T from LUT
422
Integrate charge for current discharge cycle
425
Self discharge flag not set ?
N
Y
435
Calculate charge to increment the integration
440
Calculate charge to increment the integration
451
Get residual capacity as a function of C rate and T from LUT
455
C rate > High discharge rate and EOD flag set ?
n
y
456
Disable resets (reset flag = 1)
445
1. Integrate charge for error calculation
2. Calculate error
3. Integrate charge for capacity calc.
End integration

FIG.13C

FIG.14A

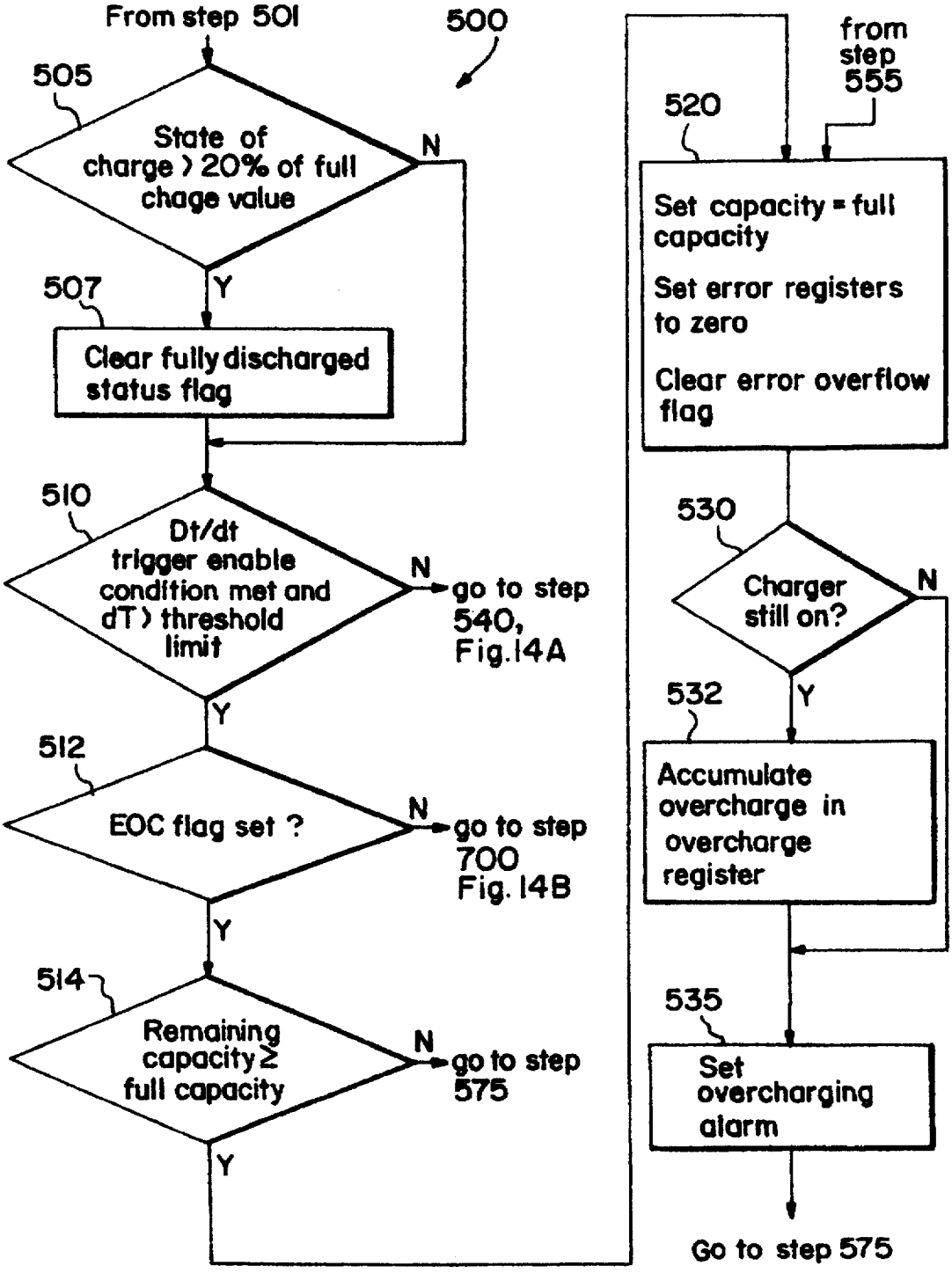

From step 501
500
505
State of charge > 20% of full chage value
N
Y
507
Clear fully discharged status flag
510
Dt/dt trigger enable condition met and dT > threshold limit
N
go to step 540, Fig.14A
Y
512
EOC flag set ?
N
go to step 700 Fig. 14B
Y
514
Remaining capacity ≥ full capacity
N
go to step 575
Y
from step 555
520
Set capacity = full capacity
Set error registers to zero
Clear error overflow flag
530
Charger still on?
N
Y
532
Accumulate overcharge in overcharge register
535
Set overcharging alarm
Go to step 575

FIG.14B

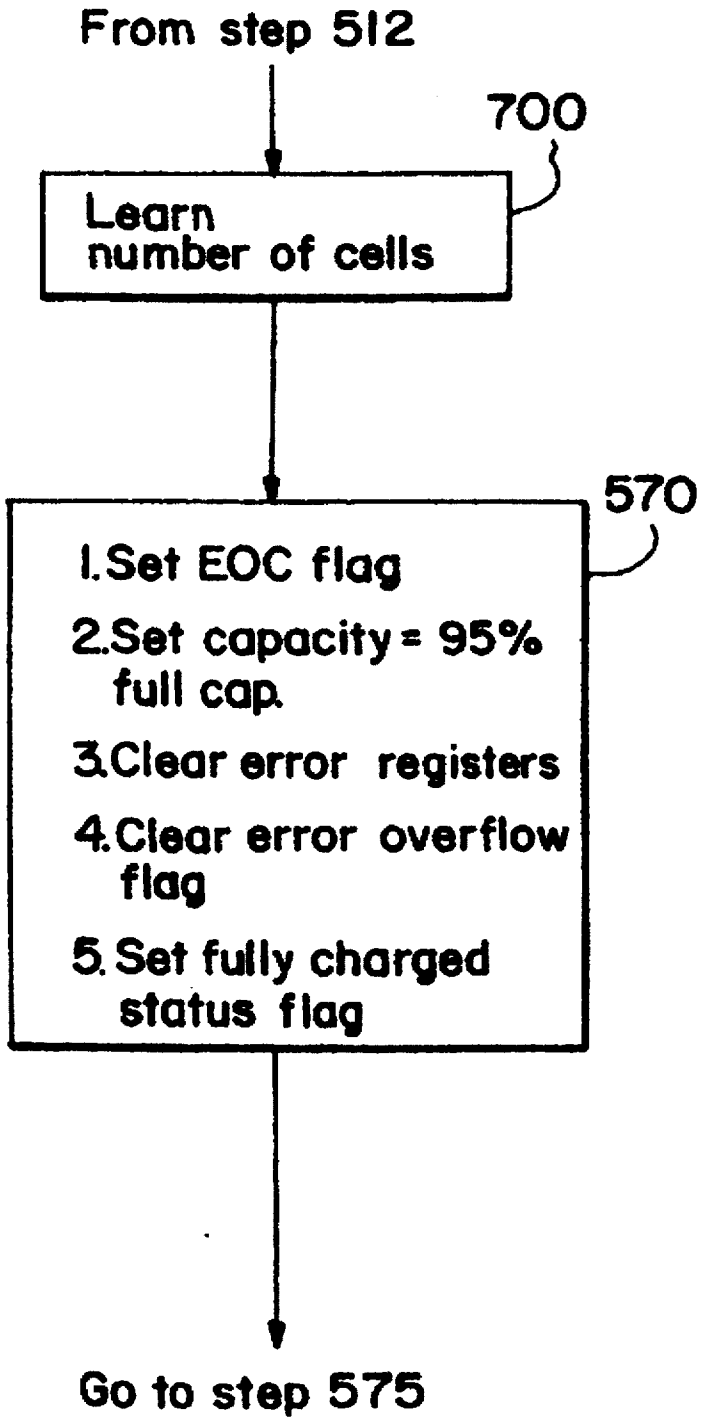

From step 512
700
Learn number of cells
570
1. Set EOC flag
2. Set capacity = 95% full cap.
3. Clear error registers
4. Clear error overflow flag
5. Set fully charged status flag
Go to step 575

FIG.14C

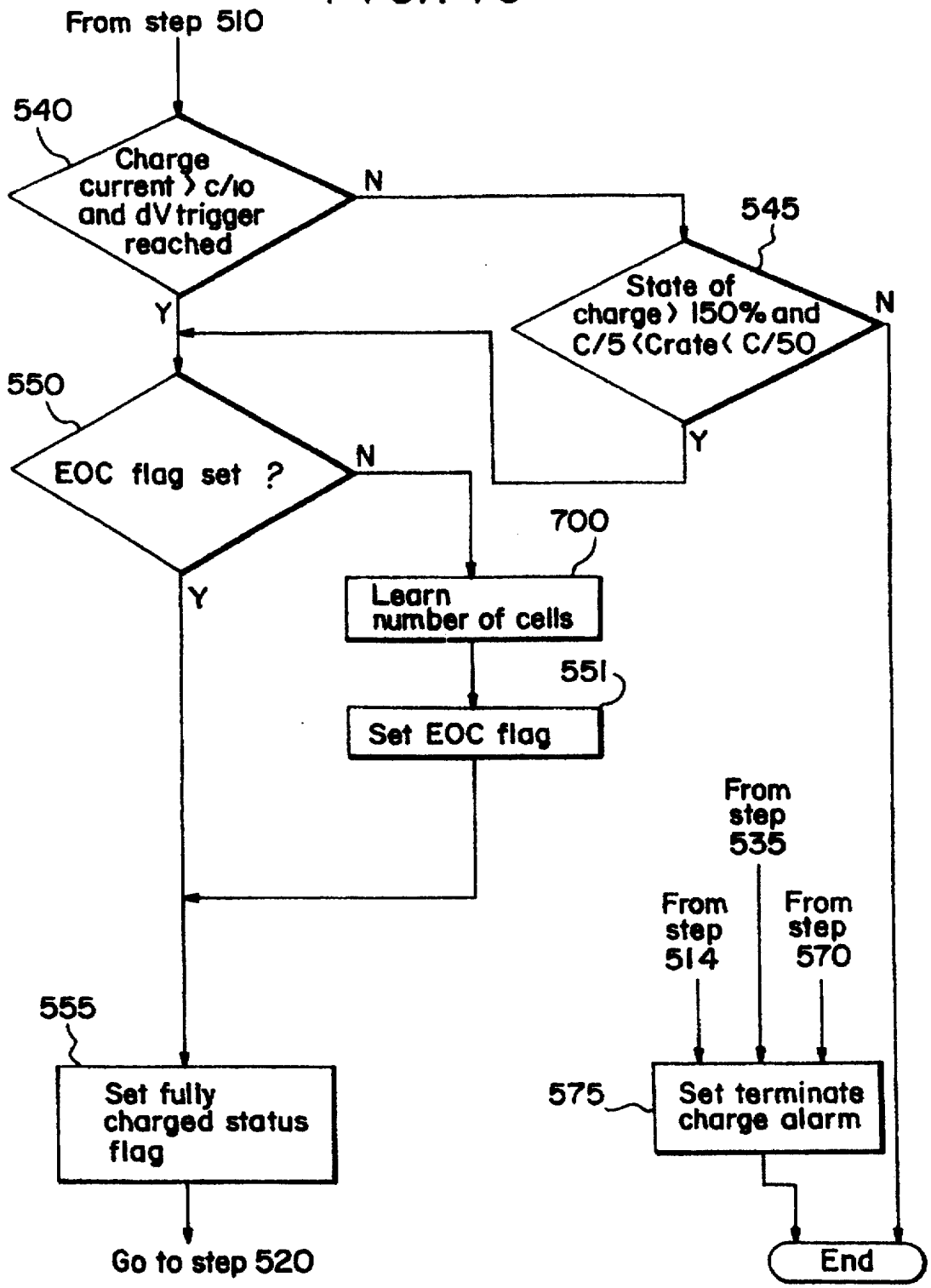

From step 510
540
Charge current > c/10 and dV trigger reached
N
545
State of charge > 150% and C/5 < Crate < C/50
N
Y
Y
550
EOC flag set ?
N
Y
700
Learn number of cells
551
Set EOC flag
From step 535
From step 514
From step 570
555
Set fully charged status flag
575
Set terminate charge alarm
Go to step 520
End

FIG.14D

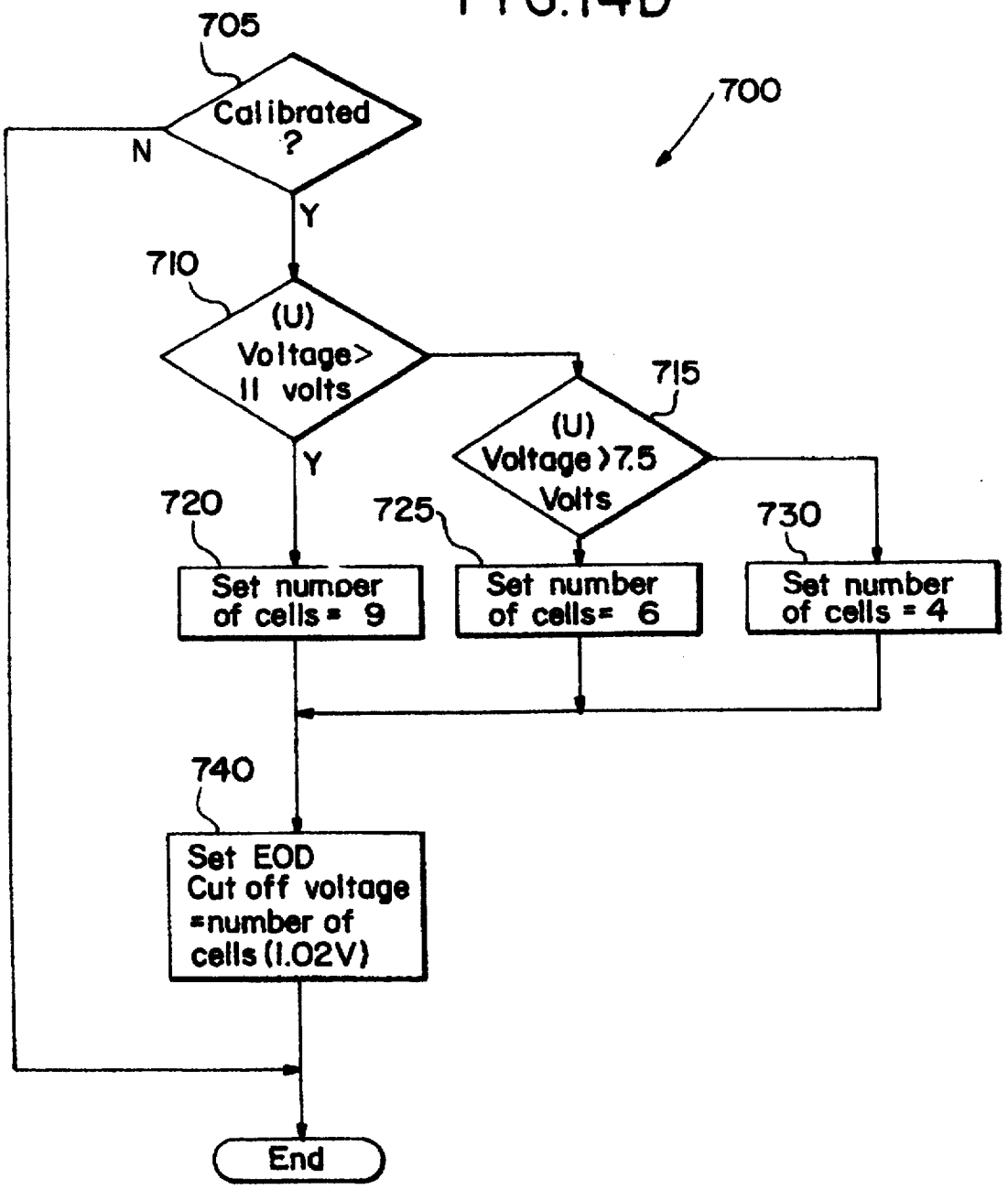

705
Calibrated ?
N
Y
700
710
(U) Voltage> 11 volts
Y
715
(U) Voltage >7.5 Volts
720
Set number of cells = 9
725
Set number of cells= 6
730
Set number of cells = 4
740
Set EOD Cut off voltage =number of cells (1.02V)
End

FIG.15A

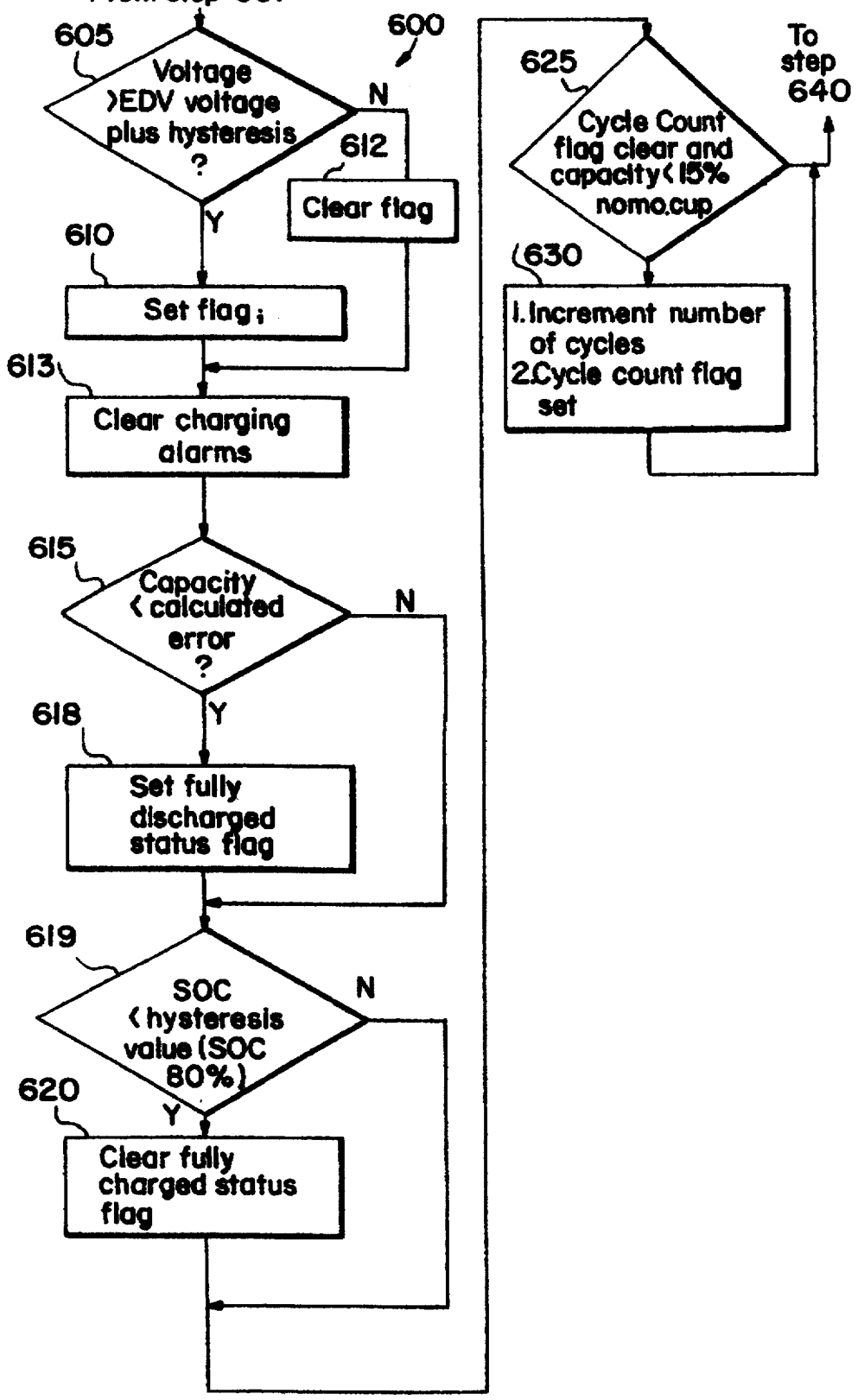

From step 601
600
605
Voltage >EDV voltage plus hysteresis ?
N
612
Clear flag
Y
610
Set flag;
613
Clear charging alarms
615
Capacity < calculated error ?
N
Y
618
Set fully discharged status flag
619
SOC < hysteresis value (SOC 80%)
N
620
Y
Clear fully charged status flag
625
Cycle Count flag clear and capacity < 15% nomo.cup
To step 640
630
1. Increment number of cycles
2. Cycle count flag set

FIG.15B

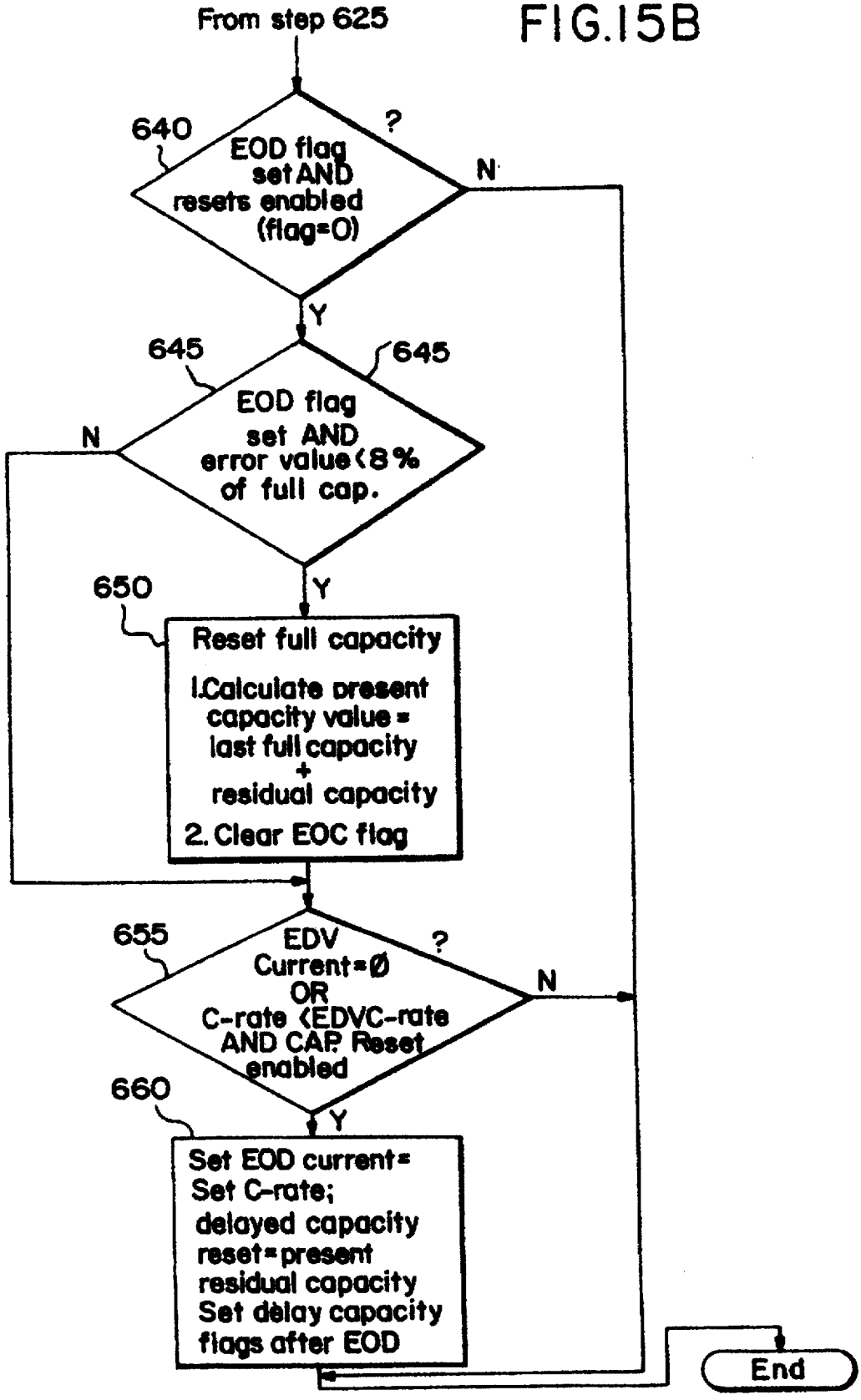
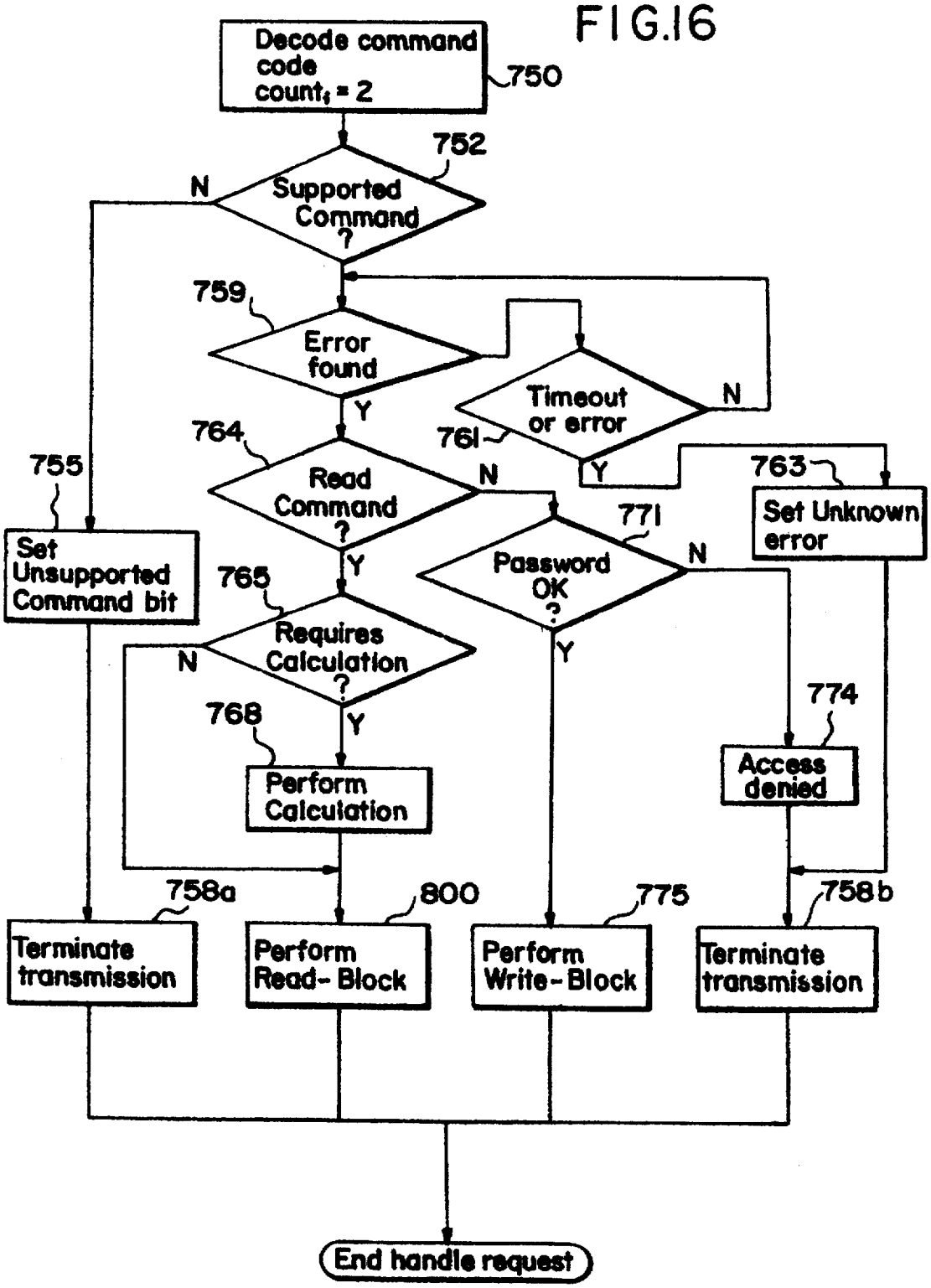

From step 625
640
EOD flag set AND resets enabled (flag=0) ?
N
Y
645
645
EOD flag set AND error value<8% of full cap.
N
Y
650
Reset full capacity
1.Calculate present capacity value = last full capacity + residual capacity
2. Clear EOC flag
655
EDV Current=Ø OR C-rate <EDVC-rate AND CAP Reset enabled ?
N
Y
660
Set EOD current= Set C-rate; delayed capacity reset=present residual capacity Set delay capacity flags after EOD
End

FIG.16


Decode command code count$_i$ = 2
750
752
Supported Command ?
N
Y
759
Error found
Y
764
Read Command ?
N
Y
761
Timeout or error
N
Y
763
Set Unknown error
771
Password OK ?
N
Y
755
Set Unsupported Command bit
765
Requires Calculation ?
N
Y
768
Perform Calculation
774
Access denied
758a
Terminate transmission
800
Perform Read-Block
775
Perform Write-Block
758b
Terminate transmission
End handle request

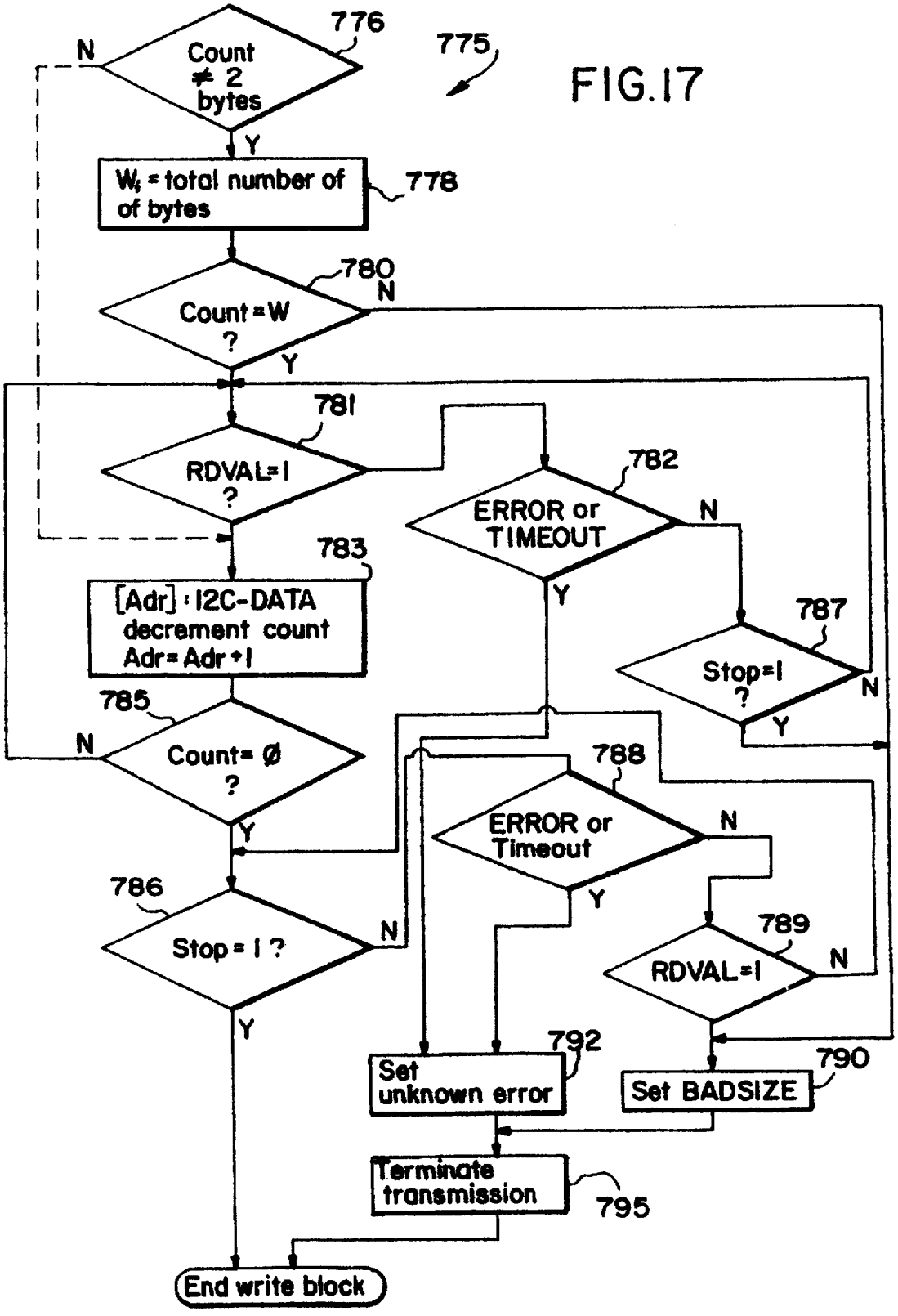
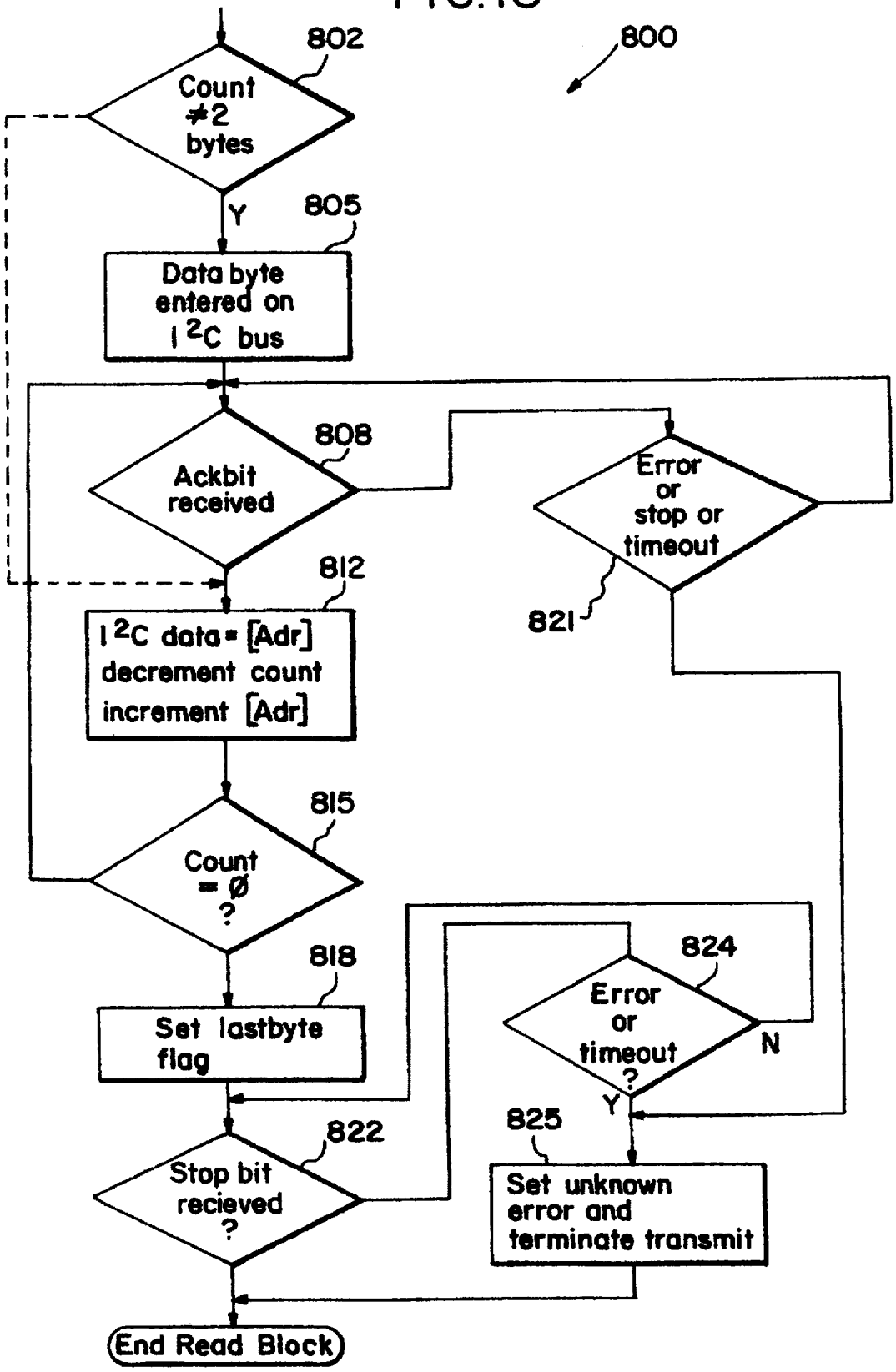

776
775
Count ≠ 2 bytes
N
Y
W_t = total number of of bytes
778
780
Count = W ?
N
Y
781
RDVAL=1 ?
782
ERROR or TIMEOUT
N
Y
783
[Adr] ← I2C-DATA
decrement count
Adr = Adr + 1
787
Stop=1 ?
N
Y
785
Count = Ø ?
N
Y
788
ERROR or Timeout
N
Y
786
Stop = 1 ?
N
Y
789
RDVAL=1
N
792
Set unknown error
790
Set BADSIZE
Terminate transmission
795
End write block

FIG.17

FIG. 18


800
802
Count ≠2 bytes
Y
805
Data byte entered on I²C bus
808
Ackbit received
Error or stop or timeout
821
812
I²C data = [Adr] decrement count increment [Adr]
815
Count = Ø ?
818
Set lastbyte flag
824
Error or timeout ?
N
Y
822
Stop bit recieved ?
825
Set unknown error and terminate transmit
End Read Block

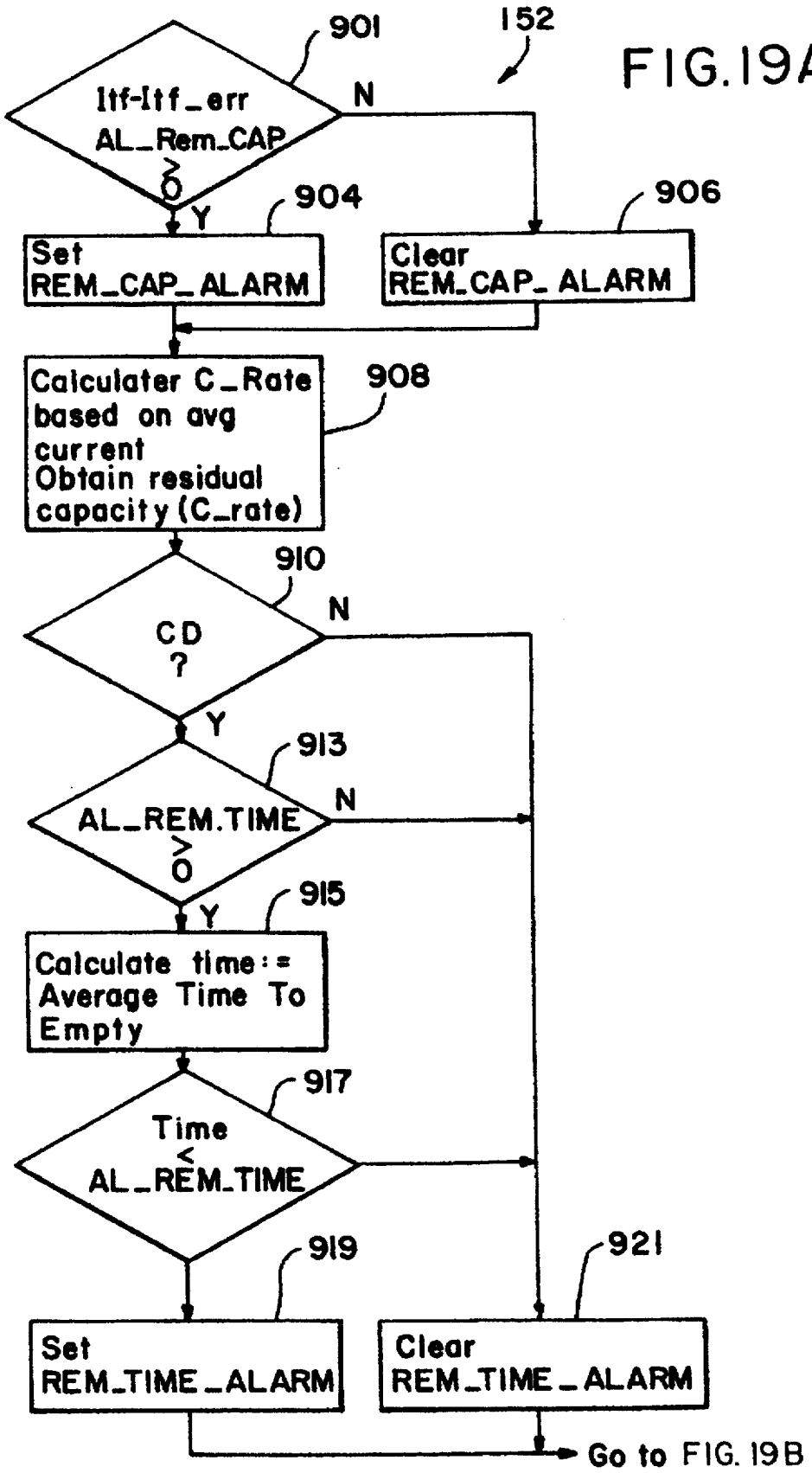
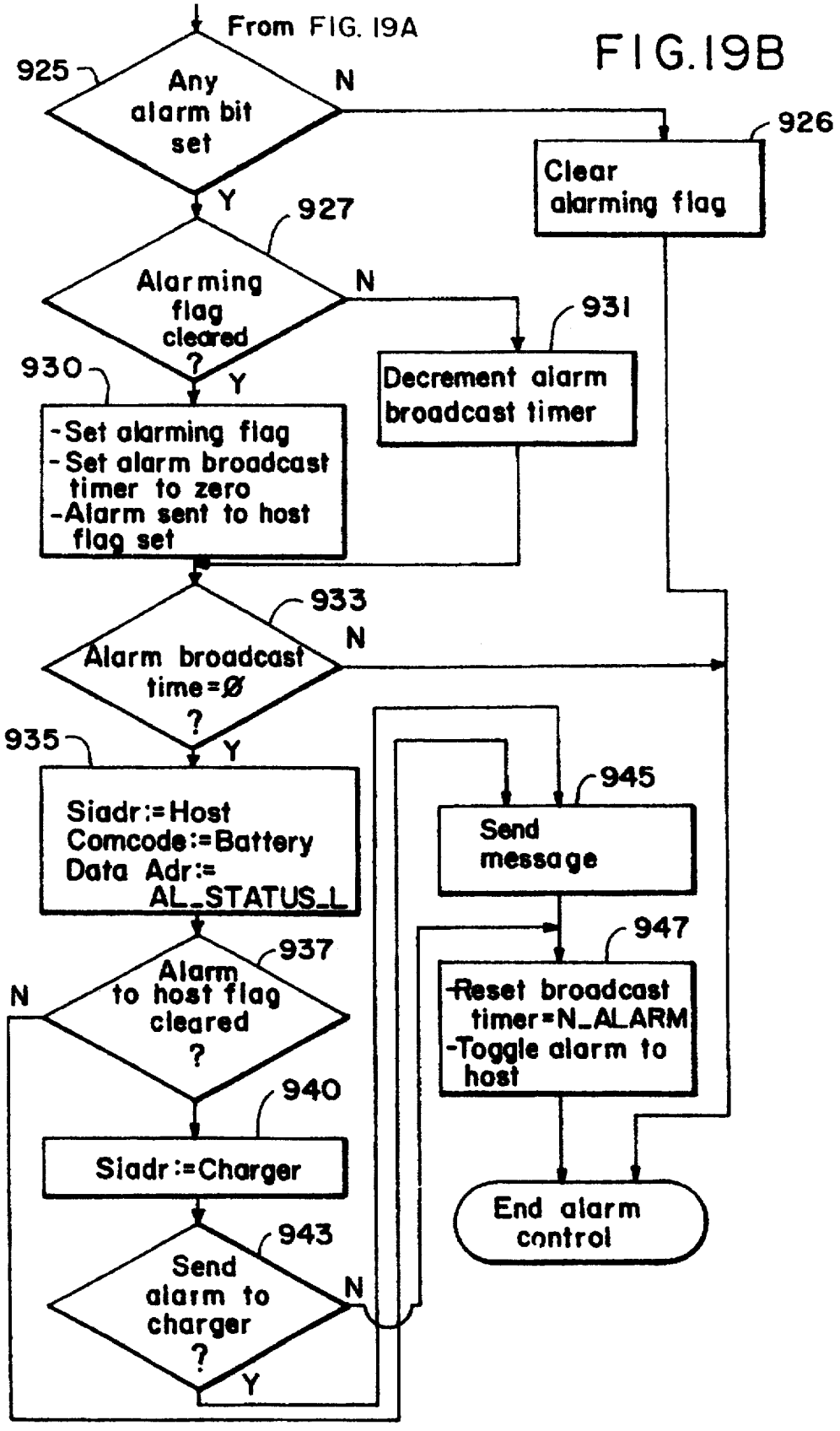

152
901
Itf-Itf_err
AL_Rem_CAP
> 0
N
Y
904
Set
REM_CAP_ALARM
906
Clear
REM_CAP_ALARM
Calculater C_Rate
based on avg
current
Obtain residual
capacity (C_rate)
908
910
CD
?
N
Y
913
AL_REM.TIME
> 0
N
Y
915
Calculate time:=
Average Time To
Empty
917
Time
<
AL_REM_TIME
919
Set
REM_TIME_ALARM
921
Clear
REM_TIME_ALARM
Go to FIG. 19B

FIG.19A

FIG.19B


From FIG. 19A
925
Any alarm bit set
N
Y
926
Clear alarming flag
927
Alarming flag cleared ?
N
Y
931
Decrement alarm broadcast timer
930
-Set alarming flag
-Set alarm broadcast timer to zero
-Alarm sent to host flag set
933
Alarm broadcast time=Ø ?
N
Y
935
Siadr:=Host
Comcode:=Battery
Data Adr:=
AL_STATUS_L
945
Send message
947
-Reset broadcast timer=N_ALARM
-Toggle alarm to host
937
Alarm to host flag cleared ?
N
940
Siadr:=Charger
943
Send alarm to charger ?
N
Y
End alarm control

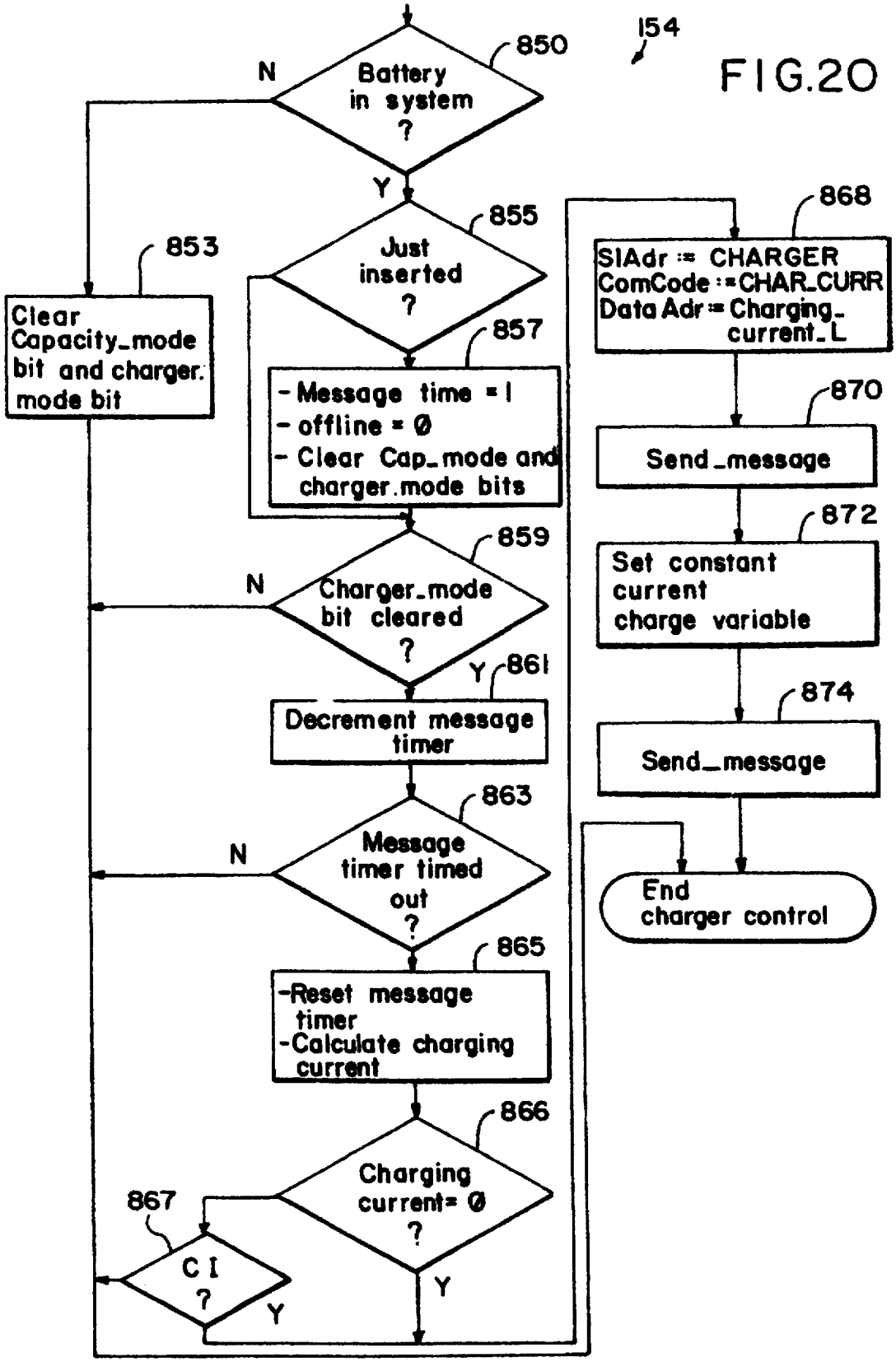

154
850
Battery in system ?
N
Y
853
Clear Capacity_mode bit and charger. mode bit
855
Just inserted ?
857
- Message time = 1
- offline = Ø
- Clear Cap_mode and charger.mode bits
859
Charger_mode bit cleared ?
N
Y
861
Decrement message timer
863
Message timer timed out ?
N
865
-Reset message timer
-Calculate charging current
866
Charging current= Ø ?
867
C I ?
Y
Y
868
SIAdr := CHARGER
ComCode := CHAR_CURR
Data Adr = Charging_ current_L
870
Send_message
872
Set constant current charge variable
874
Send_message
End charger control

FIG.20

FIG. 21A

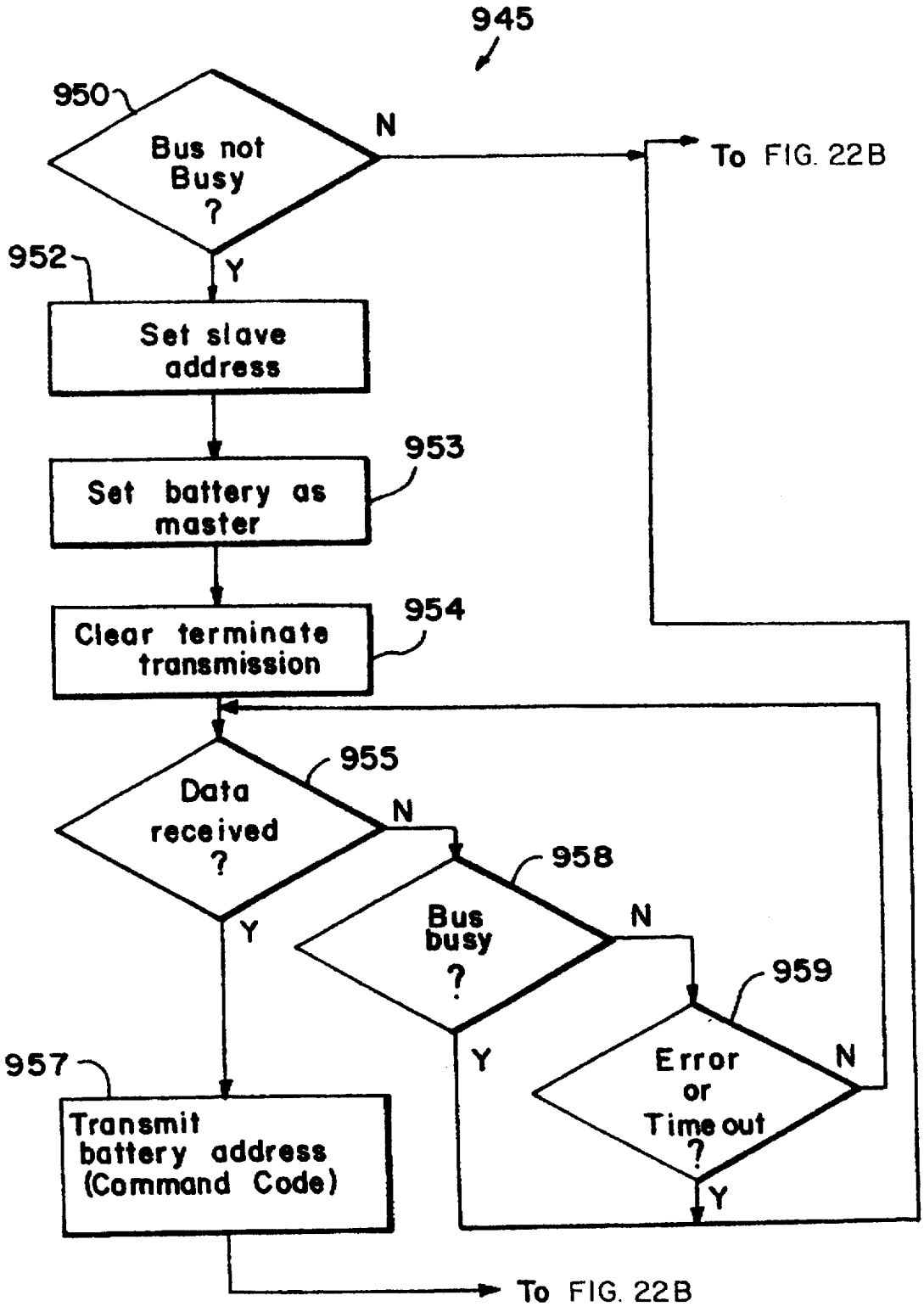

945
950
Bus not Busy ?
N
To FIG. 22B
Y
952
Set slave address
953
Set battery as master
954
Clear terminate transmission
955
Data received ?
N
958
Bus busy ?
N
959
Error or Time out ?
N
Y
Y
Y
957
Transmit battery address (Command Code)
To FIG. 22B

FIG. 21B

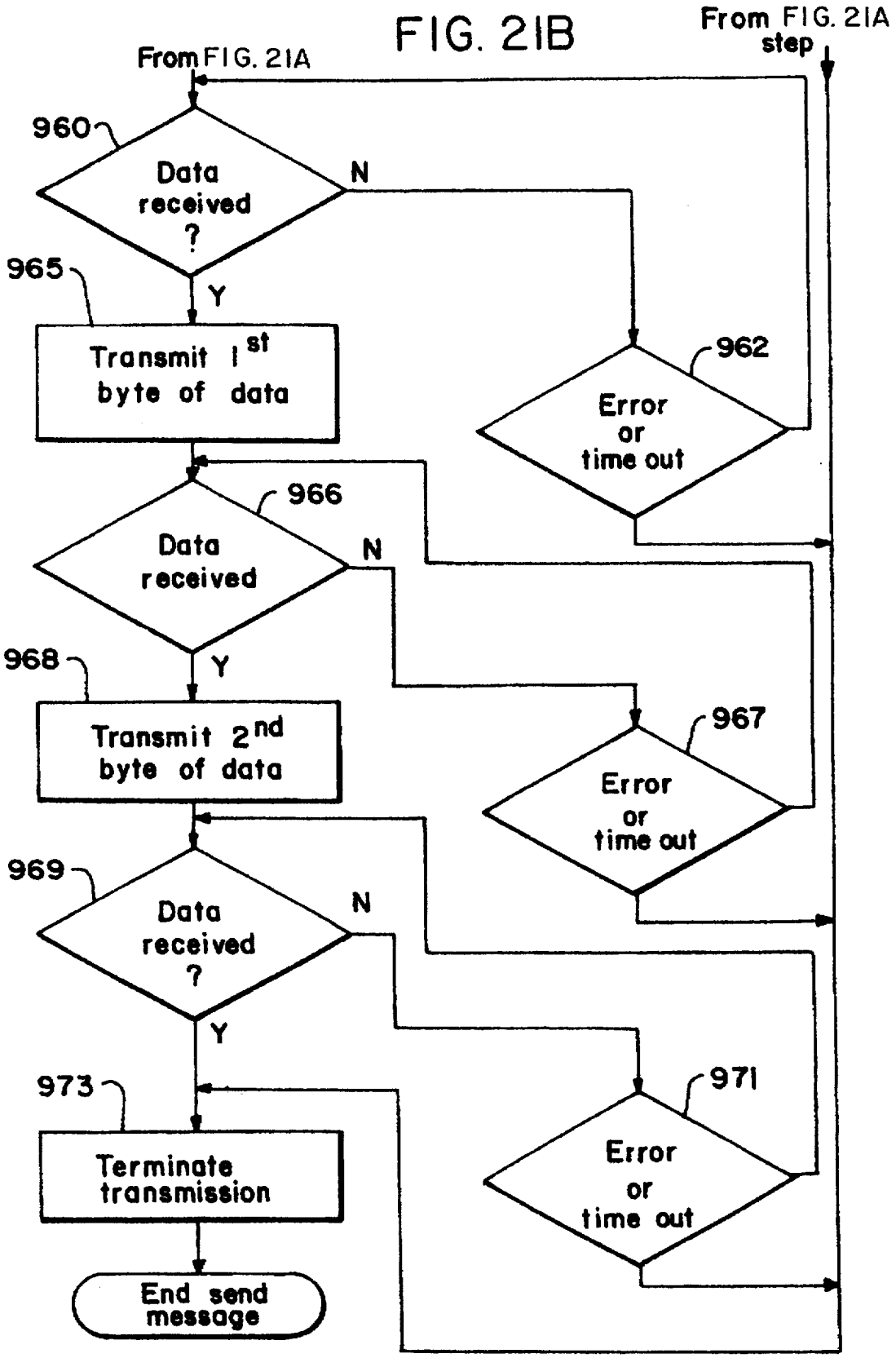

From FIG. 21A
From FIG. 21A step
960
Data received ?
N
Y
965
Transmit 1st byte of data
962
Error or time out
966
Data received
N
Y
968
Transmit 2nd byte of data
967
Error or time out
969
Data received ?
N
Y
973
Terminate transmission
971
Error or time out
End send message

FIG. 22A

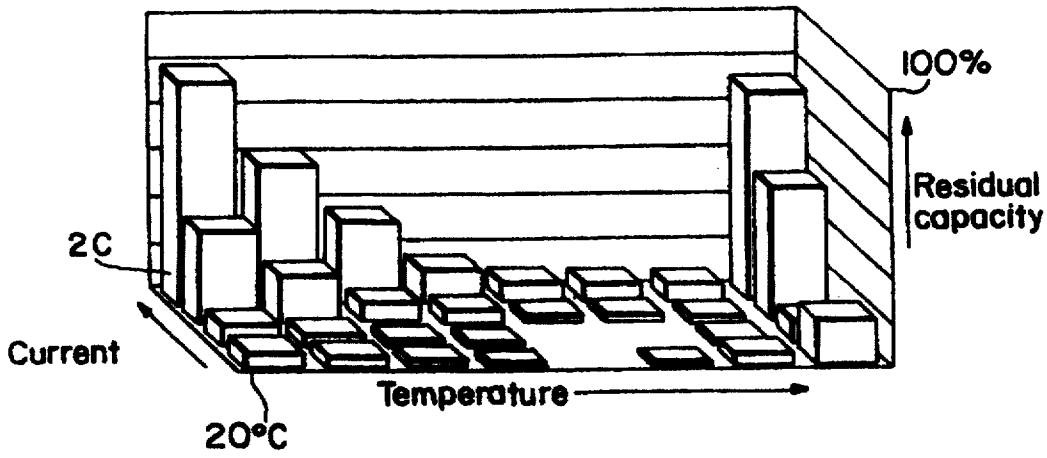


FIG. 22B

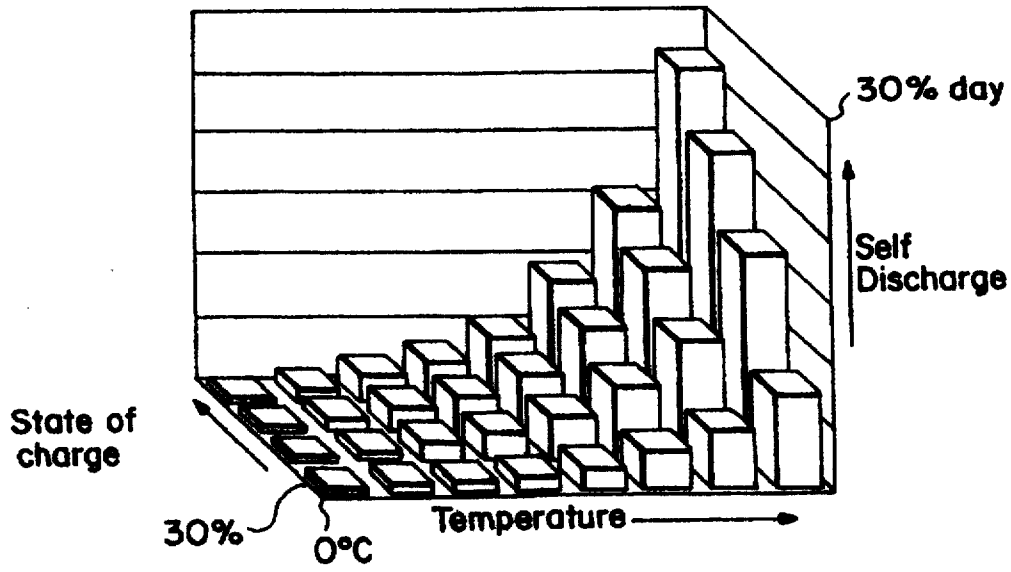


FIG. 22C

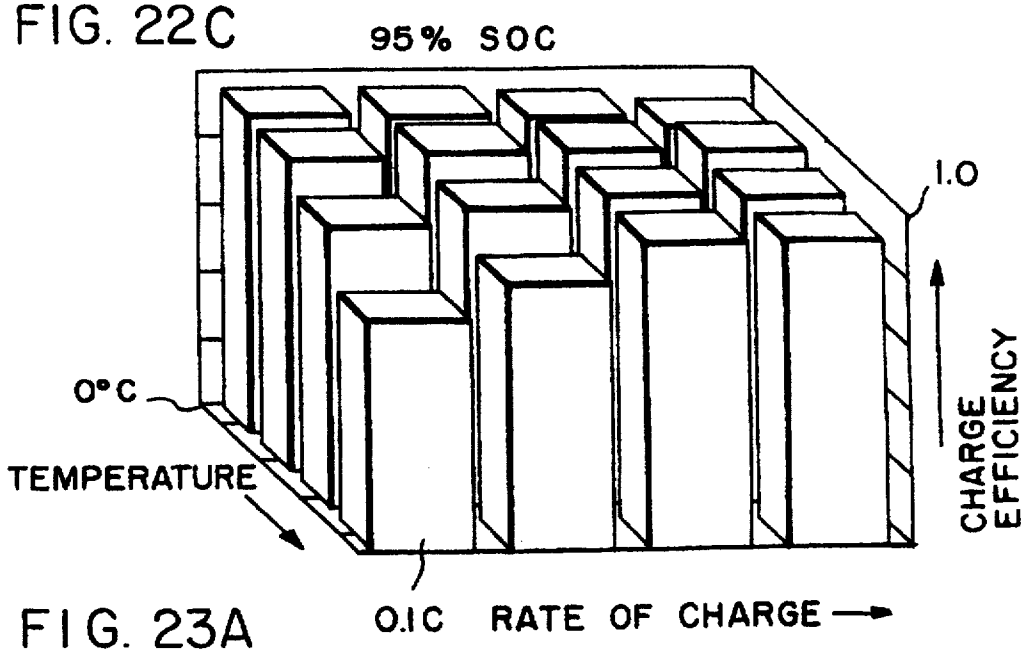


FIG. 23A

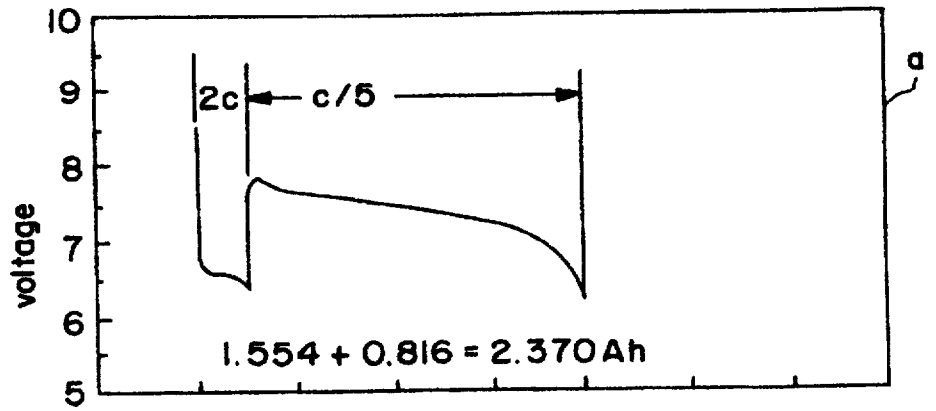
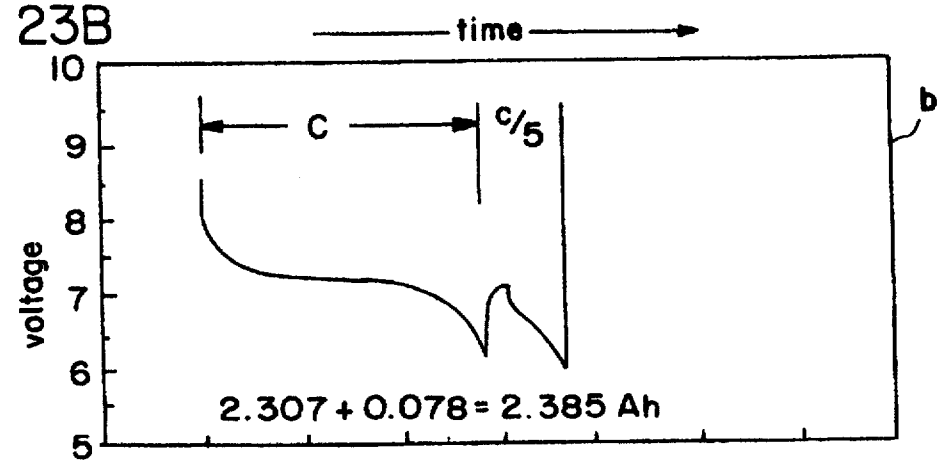


FIG. 23B



BATTERY PACK HAVING A PROCESSOR CONTROLLED BATTERY OPERATING SYSTEM

CROSS-REFERENCE

This application is a divisional of U.S. Ser. No. 08/336,945, filed Nov. 10, 1994.

FIELD OF THE INVENTION

The present invention relates generally to the art of rechargeable batteries and more specifically to a smart battery for use in an intelligent device having power management capabilities. The invention is a smart battery apparatus for controlling the operation of rechargeable Nickel Metal Hydride (NiMH) or Nickel Cadmium (NiCad) batteries, and the like, to enable the reporting of accurate information to the intelligent device for power management and charge control specific to the battery's state of charge and chemistry.

DESCRIPTION OF THE PRIOR ART

The advent of intelligent portable electronic device such as notebook computers, video cameras, and cellular phones has enabled the development of smart rechargeable batteries that can communicate with the intelligent device to provide accurate information on the battery's present state of charge, and how best to recharge the battery to maintain maximum battery life, thus enabling the highest number of charge-discharge cycles. A user of such intelligent portable devices utilizing such smart batteries will not only know how much charge is left in the battery, but battery run time at various rates of power consumption. This enables the user to select a mode of operation that will enable maximum service life on the remaining state of charge and, how long the device will continue to operate.

Prior art rechargeable battery units have been provided with means for generating some desired information to their users, including for instance, a charge monitor and fuel gauge such as that disclosed in U.S. Pat. No. 5,315,228 which discloses a method for calculating state of charge and reporting run time to empty to the host computer system.

However, there is a need for a rechargeable power unit that will accurately maintain its own state of charge information even when nominally fully discharged such that a user will have instantaneous access thereof. Moreover, there is also a need for an intelligent rechargeable battery that can provide the user with an accurate prediction of its remaining operating time at various levels of power consumption. The user of such an intelligent device, such as a portable computer, can thus elect to power down a hard disk drive to extend the operation of the portable computer for a longer period of time than would have been possible at the higher rate of power consumption.

SUMMARY OF THE INVENTION

Accordingly, it is an object of the present invention to provide a smart battery device for use with a rechargeable battery to be installed in a host computer that will optimize the performance of the rechargeable battery throughout its life cycle.

It is another object of the instant invention to provide a smart battery device that includes a microprocessor for controlling a rechargeable battery that performs battery capacity calculations for communication to a host computer device or a smart battery charge device.

It is still another object of the instant invention to provide a smart battery device that includes a microprocessor for controlling a rechargeable battery and that provides intelligence in the form of present state of charge and battery charge parameters to a host device for communication to a smart charger.

It is yet still a further object of the instant invention to provide a smart battery device that includes a microprocessor for controlling a rechargeable battery that monitors battery operating parameters such as voltage, current, and temperature to thereby enable either a rapid charging rate or an optimal charging rate from any charged state.

Still yet another object of the instant invention is to provide a smart battery device that includes a microprocessor for controlling a rechargeable battery that calculates predictive data such as the battery's remaining life at the current rate of drain and at alternate rates of drain.

It is still a further object of the instant invention to provide a smart battery device that is an application specific integrated circuit (ASIC) having analog and digital components.

Furthermore, another object of the present invention is to provide a smart battery device that includes an analog to digital (A/D) converter for measuring battery charge parameters such as voltage, current, and temperature.

Yet still another object of the present invention is to provide a smart battery device having an A/D converter with a single positive power supply that is capable of bipolar operation for converting both positive and negative analog signals representing battery charge and discharge currents, respectively.

Another object of the instant invention is to provide a smart battery device as above wherein the analog and digital components of the ASIC comprise CMOS semiconductor technology designed for improved accuracy, and high A/D converter resolution with minimal power consumption.

Still another object of the present invention is to provide a smart battery device having a microprocessor that, when nominally discharged, will place itself in a sleep mode with virtually no power consumption.

Yet a further object of the present invention is to provide a smart battery device that includes a microprocessor with RAM memory, and comprises means for retaining RAM memory contents when the device is in a sleep mode.

Yet still a further object of the invention is to provide a smart battery device that comprises short circuit protection means for preserving RAM memory contents when battery is temporarily short circuited.

Another object of the instant invention is to provide a smart battery device that includes a ROM memory that is manufactured by a process that facilitates the programming of ROM in an upper or respectively later produced layers.

Yet furthermore, an object of the instant invention is to provide a smart battery device that includes a ROM memory device whereby the programming of ROM is effected in a metal mask.

Furthermore, an object of the instant invention is to provide a smart battery device having incorporated therein an error treatment algorithm, for taking into account measurement errors, interpolation from look-up tables, etc., wherein the errors are considered to be a function of time. It is contemplated that if a total error is larger than a predetermined value, certain operating modes are disabled, and, in particular, variables are substituted by default values to result in a smaller error. In case of displayed information, such as LED battery pack display, the error can be addi-

tionally taken into account, for e.g., a quantity of: capacity—total error in capacity, may be displayed. If an error that is too big is produced, the end criterion for determining end of charge condition may be changed, for e.g., using a change in battery voltage instead of the error influenced criterion.

These and other objects of the present invention are attained with a smart battery device which provides electrical power and which reports predefined battery parameters to an external device having a power management system, wherein the battery includes:

(a) at least one rechargeable cell connected to a pair of terminals to provide electrical power to an external device during a discharge mode and to receive electrical power during a charge mode, as provided or determined by said remote device,

(b) a data bus for reporting predefined battery identification and charge parameters to the external device,

(c) an analog means for generating analog signals representative of battery voltage and current at said terminals, and an analog signal representative of battery temperature at said cell,

(d) a hybrid integrated circuit (IC) having a microprocessor for receiving the analog signals and converting them to digital signals representative of battery voltage, current and temperature, and calculating actual charge parameters over time from said digital signals, said calculations including one calculation according to the following algorithm:

$$CAP_{new}=CAP_{FC}-\Sigma I_d\Delta t_d-\Sigma I_s\Delta t_s+\Sigma\epsilon_c I_c\Delta t_c$$

wherein ϵ_c is a function of battery current and temperature; and I_s is a function of battery temperature and CAP_{FC},

(e) a data memory defined within said hybrid IC for storing said predefined battery identification and actual charge parameters, even when nominally fully discharged, said charge parameters including at least full charge capacity and remaining capacity,

(f) a bus controller defined within said hybrid IC for sending battery messages to said remote device over said data bus, said messages including said predefined battery identification and said actual charge parameters.

Superimposed on this equation is reset logic, to be explained below, that self corrects the value of CAP_{FC} with a capacity calculation at each end of full charge (EOC) and each end of full discharge.

Further benefits and advantages of the invention will become apparent from a consideration of the following detailed description given with reference to the accompanying drawings, which specify and illustrate preferred embodiments of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a diagrammatic block diagram of a smart battery device connected to a host computer and battery charging device.

FIG. 2(*a*) is a simplified block diagram of the smart battery device and connector, including a pinout diagram of an Application Specific Integrated Circuit (hybrid IC) used in the present invention.

FIG. 2(*b*) illustrates a simplified block diagram of the hybrid IC **32** that includes the microcontroller of the smart battery device of the instant invention.

FIG. 3 is a general flow diagram illustrating the primary functional features of an algorithm and method for controlling the smart battery device of a the instant invention.

FIG. 4 illustrates a general schematic diagram of the A/D converter **60**.

FIG. 5(*a*) illustrates a schematic sketch of dc voltage shifting circuit arrangement.

FIG. 5(*b*) illustrates a second embodiment of the dc voltage shifting circuit arrangement.

FIG. 6 is a schematic sketch of the circuit arrangement in the A/D converter **60**.

FIG. 7 is a phase diagram in the operation of the A/D converter pursuant to FIG. **6**.

FIG. 8(*a*) illustrates the timing of the operating cycles under normal and sample mode operating conditions.

FIG. 8(*b*) illustrates the approximate time durations for the various measurements per operating cycle.

FIG. 9(*a*) illustrates a schematic sketch of a sample transition arrangement for the ROM included in the smart battery device; and

FIG. 9(*b*) is a schematic sketch of the transistor arrangement of a ROM programmed pursuant to the prior art.

FIG. **10** is a detailed schematic of the power-on reset **85** and RAM de-latching circuit **85'**.

FIG. **11** illustrates a detailed schematic diagram of the comparator wake-up circuit **80**.

FIG. **12** is a flow diagram illustrating the IUT (current, voltage, and temperature) calculation program **200**.

FIGS. 13(*a*) and 13(*b*) are flow diagrams illustrating the sequential processes **151** programmed in the microprocessor for calculating the current capacity and the amount of battery self discharge for the smart battery of the instant invention.

FIG. 13(*c*) illustrates the integration program **400** for calculating the amount of battery charge or discharge flowing into or out of its terminals.

FIGS. 14(*a*) through 14(*c*) are flow diagrams illustrating the sequential processes **500** programmed in the microprocessor for determining battery charging end conditions when the battery is in a capacity increasing state.

FIG. 14(*d*) illustrates a flow diagram of the learn number of cells program **700**.

FIGS. 15(*a*) and 15(*b*) are logic flow diagrams illustrating the sequential processes **600** programmed in the microprocessor for determining battery end conditions when the battery is in a capacity decreasing state.

FIG. **16** illustrates a logic flow diagram of the handle request routine that is invoked when there is communication between the smart battery and the host computer or battery charger.

FIG. **17** illustrates a detailed logic flow diagram of the write block routine for writing data to the smart battery.

FIG. **18** illustrates a detailed logic flow diagram of the read block routine for reading data from the smart battery.

FIGS. **19** illustrates a flow diagram describing the logic steps invoked by the smart battery system when broadcasting an alarm condition to an external device.

FIG. **20** illustrates a logic flow diagram describing the steps invoked by the smart battery system when broadcasting a charge condition to a battery charger.

FIG. **21** illustrates a logic flow diagram describing the steps invoked by the smart battery system when broadcasting a message.

FIG. 22(*a*) is a three-dimensional graphic representation of look up tables that depict predicted residual capacity values as a function of discharging current and temperature.

FIG. 22(*b*) is a three-dimensional graphic representation of look up tables that depict the amount of self-discharge current (vertical axis) as a function of relative battery state of charge and temperature.

FIG. 22(*c*) is a three-dimensional graphic representation of charge efficiency look-up tables showing charge efficiency factors as a function of relative state of charge, charging current, and temperature.

FIG. 23 illustrates two voltage versus time graphs, a and b, comparing calculated battery capacity characteristics at various discharging current rates for a six (6) cell battery pack.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The smart battery device of the present invention is intended for use with an intelligent host device such as a portable computer, portable video camera or cellular telephone having a system management bus and a smart charger, or an intelligent host device having a system power manager that can receive and send data over a system management bus.

A representative example of such a system is illustrated in FIG. 1, wherein the smart battery **10** is connected to a power plane **12** to supply and receive electrical energy over the power plane, and a system management bus **14**, which is a bi-directional modified I2C data bus (communication interface) that communicates with a host device **16** which may be a portable computer. The host device **16** may be powered by the smart battery **10**, or by the system power supply **18** and a conventional AC source **20**. A system power supply or power management system also communicates with a smart charger **22** which may be used to determine the rate and duration of charge sent to the smart battery by the power supply. Smart charger **22** also communicates with the system management bus **14**, and may receive a temperature signal representative of battery cell temperature on a separate line **24**. A detailed functional description of the system management bus **14** (bi-directional modified I2C data bus) can be found in the Intel\Duracell System Management Bus Specification, Rev 0.95, (April 1994).

The power management system **18** may supply or draw power to/from the smart battery **10** over power plane **12**, depending upon the state of charge in smart battery **10**, and depending upon the presence or absence of power at AC source **20**.

The smart charger **22** may periodically poll the smart battery **10** for charge characteristics, and adjust output to match a smart battery charge request. Optionally, and if selected by the user of the host device, the smart charger **22** can override the smart battery's charge rate request and charge the smart battery at a higher or quick charge rate. The user of the host device does not necessarily need to override the smart battery's request. As will be explained in greater detail below, the smart battery may periodically broadcast the desired charging current, or the smart charger **22** polls the smart battery for a charging current. The host or the charger need not comply with the smart battery's request and can provide a greater or lesser amount of power than requested.

The host device **16** may communicate with the smart battery over the system management bus **14** and request information from the battery for use in the system power management scheme, thereby providing the user of the host device with information about the battery's present state and capabilities. The host device **16** will also receive notice of critical events, including alarm conditions, remaining capacity below a user set threshold value, a remaining run time below a user set threshold value, or an end of discharge signal. The alarm conditions include but are not limited to overcharging, overtemperature, a remaining charge capacity below a predetermined or user set capacity, or a run time below a predetermined or user set run time remaining.

As will be hereinafter explained in greater detail, the smart battery can report out an instantaneous current value being drawn from the battery, current values averaged over predetermined time intervals, present temperature and present voltage.

The smart battery may also report out a number of battery status indicators, indicating whether or not the battery is charging or discharging, that charging is complete, or that the battery is fully discharged.

In addition, the smart battery can provide calculated values including run time remaining at a present current usage, a run time remaining at an average current use, a run time remaining at optimal current use, and a predicted run time remaining at a host device selected current level (discharge rate).

The smart battery device **10** is also provided with a read-only memory (ROM) that is manufactured to contain a set of predefined battery identification parameters which may include manufacturer data, cell chemistry, design capacity, design voltage, and a unique device identification number. The predefined battery identification parameters are available, for either the host device or the smart charger, to assist them in the selection of optimal usage and charge parameters for the smart battery.

The smart battery is also capable of recommending a desired charge current, reporting a time remaining to full charge, a battery capacity available at full charge, and the number of times the battery has been charged or discharged.

The smart battery of the present invention utilizes a hybrid integrated chip (IC) containing an embedded microprocessor and a novel analog to digital converter which receives analog signals from the battery and converts them to digital signals representative of battery voltage, current and temperature. The smart battery microprocessor then calculates actual charge parameters over time from these digital signals according to a predetermined algorithm in which CAP_{rem} is the remaining capacity of the battery which is continuously assigned a new value to reflect adjustments for effective charge, discharge, and self discharge.

The charge delivered to the battery is measured, and adjusted by an efficiency factor which is a function of current, temperature, and relative state of charge. It should be mentioned that the remaining capacity, CAP_{rem}, and the relative state of charge, SOC, represent the same thing (remaining battery capacity) and differ in that relative state of charge is indicated as a percentage of the last full charge capacity. The charge efficiency is a value determined as a function of the above variables and may be derived from a look up table, hereinafter described with respect to FIG. 2(*c*), or calculated from a formula which provides a stepwise approximation of charge efficiency behavior, depending upon current, temperature and state of charge. It is understood that the charge efficiency factor can be obtained from a response equation or interpolation between several different values stored in memory.

Likewise, the remaining battery capacity CAP_{rem} is decremented by the measured discharge rate over time. A predictive model of residual capacities determines expected CAP_{rem} for a present current and temperature. This predic-

tive model may also estimate when the battery voltage will drop to a predetermined cut-off voltage for the present rate of discharge. This residual capacity model may be calculated from a formula or obtained from a look up table, which includes values of residual capacities as a function of discharge current and temperature.

Finally, CAP_{rem} is also adjusted by subtracting self discharge. Self discharge is calculated as a function of temperature and state of charge, and is always subtracted from CAP_{rem}, regardless of whether the battery is discharging or being charged. Self discharge may be derived from a look up table of empirical models of identical cell chemistry that predict self discharge as a function of temperature and state of charge, or may be calculated by the microprocessor.

As will be hereinafter explained in greater detail, CAP_{FC} is a learned value which is self correcting because of reset logic incorporated in the capacity algorithm. The capacity algorithm takes actions on four types of end of charge (EOC) signals, including a negative voltage slope at a full charge voltage, a temperature rise that exceeds a predetermined rate, or a calculated state of charge that is equivalent to a value of 100% to 150% of the previous CAP_{FC} value, if an optimal charging current has been used, or a high temperature limit value. When one of the first three of the above four types of conditions is encountered, the reset logic resets CAP_{rem} to the previous CAP_{FC} value, sets a fully charged status flag, and, signals the host device and charger to terminate charge. If the high temperature limit is reached, only a signal to terminate charge is invoked.

The charge algorithm terminates its integration of the present discharge state when it reacts to an end of discharge (EOD) signal between 0.9 volts/cell and 1.1 volts/cell and preferably 1.02 volts per cell. At that point the algorithm resets CAP_{rem} to a new learned value of residual capacity, as determined from the integration of the discharge current, as a function of discharge current and temperature.

As will be hereinafter explained in greater detail, the reset logic will reset CAP_{FC} as a function of which EOD signal was acted on. Thus a new CAP_{FC} value for the smart battery's actual capacity is learned after each full discharge cycle, as a function of the last fully integrated battery discharge cycle. The smart battery **10** of the present invention is thus able to self correct CAP_{FC} within one full cycle to readjust its capacity at each EOC and EOD, and effectively relearn full battery capacity within a single cycle, even if all prior battery history has been extinguished by virtue of a catastrophic memory failure. The smart battery of the present invention is therefore able to accurately predict actual capacity, and typically is able to correctly predict the remaining run time to empty within a few minutes for a 2400 maH battery.

Smart battery **10** of the present invention is more fully illustrated in FIG. **2**(*a*) which is a simplified block diagram of the smart battery, an advanced design multi-pin connector, and a battery module **28** which includes a pinout diagram of the hybrid ASIC **32** used in the present invention. As illustrated in FIG. **2**(*a*), the smart battery device **10** includes a plurality of rechargeable cells generally indicated at **26** which may be Nickel Metal Hydride (NiMH) or Nickel Cadmium (NiCad) cells.

For the purposes of an illustrative but not limiting example, in the following specification, 6 NiMH cells having a nominal 2400 maH capacity, will be assumed. Such an arrangement of cells is particularly appropriate for powering a portable computer.

A suitable advanced design multi-pin battery connector **30** is used to connect the smart battery to a host device **16** or power supply **18**, as previously described with respect to FIG. **1**. The multi-pin connector **30** includes a positive power supply terminal **31** which is connected to the positive terminal of the first cell, and a negative power supply terminal **33** which is connected to the negative terminal of the last cell. A plurality of rechargeable cells may be connected in series therebetween as illustrated in FIG. **2**(*a*).

The smart battery module **28** includes a hybrid IC **32** containing a microprocessor **50** (FIG. **2**(*b*)) and a plurality of sensor means for generating analog signals representative of battery voltage, current and temperature. The module also includes a series of four (4) LEDS **34** driven by an LED drive circuit **53** and a switch **35** which may be manually actuated by an end user to determine the state of charge in the battery even when the battery module has been removed from the host device **16**. The LEDS **34** may be used to represent a relative state of charge (SOC) in a logic scheme as follows: if the state of charge is greater than 75% (or less than 100%) then all 4 LEDS are illuminated; if the SOC is from 50% to 75% then 3 LEDS are illuminated; if SOC is from 25% to 50%, then 2 LEDS are illuminated; if SOC is from 10% to 25%, then 1 LED is illuminated, and if SOC is less than 10%, a single LED is flashing. As mentioned above, relative SOC is remaining capacity relative to last full capacity.

As shown in FIGS. **2**(*a*) and **2**(*b*), the hybrid ASIC **32** also includes an external crystal **36** operating at a fixed frequency which is used as a time base for integration of battery current over time, and to ensure stable start up after a prolonged standby period when power is reapplied to the smart battery **10**. The smart battery of the present invention utilizes two separate oscillators, a low power RC oscillator **48** formed within the hybrid IC **32** and used as an operating clock for the hybrid IC and the A/D converter **60** therein, and the external crystal **36**. As will be hereinafter described in greater detail, the external crystal **36** is used to restart the measurement period after each predetermined interval to provide for accurate measurements and integration of battery conditions, regardless of battery temperature, which can adversely affect the accuracy of the internal oscillator. The frequency value of external crystal **36** may range from 10 kHz to 66 kHz, preferably at 32 kHz and the frequency value of oscillator **48** may range from 450 kHz to 460 kHz.

The hybrid IC **32** includes a MIKRON GmbH low cost, high performance, CMOS 8 bit microcontroller (μP) **50** with an advanced RISC architecture. A reduced set of **32** instructions that are all single cycle instructions (except for program branches which are two cycles), and a Harvard architecture scheme achieves a high level of performance with minimal power drain. The microprocessor operates at a clock input anywhere from DC to 10 MHz with 12 bit wide instructions and 8 bit wide data path. A free programmable Counter/Timer circuitry is provided as well as a free programmable Watchdogtimer. Additionally, the microprocessor is addressable in direct, indirect, and relative addressing modes. The microprocessor **50** is commercially available from Mikron Gmbh, located at Breslauer Straβe 1-3, D85386, Eching, Germany, and is available in the U.S.A. through MICROCHIP Technology, Inc., Chandler, U.S.A.

The hybrid IC **32** also includes a plurality of analog circuits which are used, in combination with external analog sensors, to generate digital signals representative of battery voltage, current and temperature as will be hereinafter explained.

For example, as shown in FIG. **2**(*a*) battery voltage is obtained from a voltage divider circuit which resistors **R1**

and R2 which are internally switched by a NMOS transistor within the hybrid IC **32** to provide voltage measurement during a small portion of each measurement interval, thereby minimizing current drain on the battery cells **26**.

The measurement of battery temperature is accomplished with an NTC-thermistor, illustrated as R_{NTC1} in FIG. **2**(*a*), which varies resistance as its temperature varies. A resistor R3 is connected in series to form a voltage divider circuit between V_{ASS}, (negative analog power supply voltage) V_{TEMP}, (the temperature voltage input) and V_{REFT}, which is a reference voltage applied to the thermistor/resistor string by the hybrid ASIC **32** at pin V_{REFT}. The temperature voltage input is measured at V_{TEMP} according to the following formula:

$$V_{TEMP} = \frac{R3}{R3 + R_{NTC1}} \times V_{REFT}$$

wherein the NTC1 value may be 10 kohms at 25° C. and varies with temperature. If desired, a look-up table with a plurality of temperature values and a plurality of V_{TEMP} values may be defined to calculate the battery temperature, and between these values, the temperature is linearly interpolated by the microprocessor within IC **32**.

The measurement of battery current is measured through a shunt resistor, illustrated in FIG. **2**(*a*) as R_{shunt}, that is connected in series with the battery cells and negative terminal **33** of cell pack **26**. The shunt resistor is of small value, but may range anywhere from 1 mohm to 200 mohms depending on the number of cells and expected usage of the battery. The voltage drop across the shunt is sensed between V_{SHUNT+}, the shunt resistor positive input pin of ASIC **32**, and V_{ASS}, the negative analog power supply voltage.

As shown in FIG. **2**(*b*), whenever the analog signals representing battery voltage, current, and temperature are obtained, they are input into an ASIC multiplexor or switching network **55** which enables only one analog signal at a time to be input to the A/D converter **60** for digital conversion. The switching network acts in conjunction with digital logic circuitry for informing the A/D converter, via line **55'**, shown in FIG. **2**(*b*), of the amount of integration cycles to perform depending upon the type of measurement to be converted. For instance, more integration cycles are needed when making a current measurement conversion to ensure a higher bit resolution as compared to when a voltage or temperature measurement is being converted, as will be explained in further detail below with respect to FIG. **8**(*a*).

A general schematic diagram of the A/D converter **60** is shown in FIG. **4**. In the preferred embodiment, the A/D converter **60** is a bipolar, high resolution, incremental sigma-delta converter and consists of three parts: a bandgap reference circuit **62** which provides a preset analog voltage which is used as an analog ground for the A/D; a voltage divider network **64** which divides the present voltage to the analog voltages which are used as the full-scale voltage for the A/D; and a sigma delta circuit **66** for converting the analog signal to a digital word output at line **69**. A/D control circuit **68** having a clock input from the IC oscillator, provides the control for the sigma delta converter which has a different degree of resolution depending on the type of measurement. For instance, in one embodiment of the invention, the A/D converter was configured as having a resolution of 13 bits and a conversion time ranging from 300 to 400 msec for current measurements, and was configured as having a resolution of 10 bits and a conversion time ranging from 30 to 60 msec for voltage and temperature measurements. The timing diagram for the voltage, current, and temperature measurements in each operating cycle is illustrated as **58***a* in the timing of operating cycles diagram of FIG. **8**(*a*), as explained below.

In one embodiment of the invention, the voltage divider circuit **64** of the A/D converter divides the preset bandgap reference voltage into the following full scale voltages: a 150 mV signal used as the full scale voltage for the battery current measurement; 150 mV, 250 mV, or 350 mV signals used as the full-scale voltage for the battery pack voltage measurement and dependent upon the number of battery cells; and 150 mV used as the full-scale voltage for the battery temperature measurement. These values are illustrative and may vary as battery design varies.

The A/D converter of the smart battery device utilizes a sigma-delta converter circuit **66** as explained above in view of FIGS. **4** and **6**. Details of the sigma-delta converter circuit **66** capable of bipolar conversion are explained hereinbelow in view of FIGS. **5**(*a*),**5**(*b*) and FIGS. **6** and **7**. FIG. **6** particularly illustrates a switching capacitor network for receiving positive and negative voltage values, indicated as V_{IN} in FIG. **6** for input into an integrator circuit **88** and comparator circuit **89** for output into control and logic circuit **68**. In the reference, Jacques Robert et al., (1987) "A 16-bit Low-Voltage CMOS A/D Converter", *IEEE Journal of Solid-State Circuits*, Vol. sc-22, No. 2, 157–159, an incremental (integrating) sigma-delta converter implementing 4-μm CMOS, switched capacitor technology similar to that implemented in the A/D converter of the smart battery device is disclosed. What is described in the reference is a simplified, unipolar A/D converter that is largely insensitive to variations in clock frequency and clock waveforms due to the fact that all signals are represented by charges, rather than currents, as in the switched capacitor integrator that forms the core of the converter.

In the prior art, to measure positive and negative input voltages, a negative power supply is necessary in addition to the positive voltage supply. Thus, where it is desired to measure negative voltages (or currents) such as smart battery discharging current, external components (such as inverters) and circuitry that consume extra power are required, and the prospect of utilizing such circuitry for the low power application such as needed in the smart battery device of the instant invention, is diminished. Instead, to overcome this drawback, the A/D converter **60** of the instant invention does not utilize a negative voltage power supply, but makes use of an available on-chip A/D bandgap reference voltage "AGND" to be used as a virtual ground. The concept of utilizing a "virtual ground" is based on the fact that a voltage stored on a capacitor can be transferred to another d.c. voltage reference point using analog switches with virtually no loss of charge.

In FIG. **5**(*a*) there is represented a first embodiment of the dc voltage shifting circuit arrangement, consisting of three switches S1 through S3, and four connectors A1 through A4 and a capacitor C1 (with the capacitance C1). The connectors A1 through respectively A4 are at the potentials ϕ_1 through respectively ϕ_4. As shown in FIG. **5**(*a*), the switch S1, and the combination of parallel-connected switches S2 and S3 are connected to opposite terminals of the capacitor C1.

In the following there is described the operation of the inventive circuit arrangement. At the beginning, the switches S1 and S2 are closed and the switch S3 is open. The capacitor charges itself up due to the voltage differential $\phi_1-\phi_2$ and stores a charge $C1\times(\phi_1-\phi_2)$.

In the next step of the inventive process, the switches S1 and S2 are opened and one pole of the capacitor is connected through switch S3 with a potential ϕ_3. Present at the capaci-

tor C1 is now a voltage $\phi_3+(\phi_1-\phi_2)$ which can be tapped off through connection with the connectors A3 and A4 which lie on the potentials ϕ_3 and ϕ_4.

In FIG. 5(*b*) there is now represented a further embodiment of the dc voltage shifting circuit whereby an additional switch S4 is provided which, when open, prevents the presence of a potential ϕ_1 at the tapping off of the voltage $\phi_3+(\phi_1-\phi_2)$ present at the connectors A3 and A4, when switch S1 is closed.

In FIG. 6 there is illustrated the schematic circuit diagram of the inventive circuit arrangement in a switched capacitor A/D converter. The A/D converter **66** possesses an operational amplifier **88** which is utilized as an integrator, and an operational amplifier **89** which is utilized as a comparator. The non-inverted input of the comparator **89** by means of the line **91** stands in connection with the output of the integrator **88**. The inverted input of the comparator **89** and the non-inverted input of the integrator **88**, are connected with a reference potential AGND, (analog ground=1.25 volt). The output of the comparator **89** is "high", in the event that the output voltage of the integrator **88** is higher than the reference voltage AGND and "low" in the event that the output voltage of the integrator **88** is lower than the reference voltage AGND. By means of the lines L1, L2, L3 and L4, the integrator **88** or, in essence, the inverted input and the output of integrator **88** have connected in parallel therewith a capacitor C2 with a capacitance C2. The capacitor C2 has a switch SR connected in parallel therewith through lines L1 and L5, which can effectuate a discharge of the capacitor C2. Through a line L6, the inverted input of the integrator **88** stands in connection, by means of a switch S5 and a line L7, with a capacitor C1 having the capacitance C1. A line L8 connects the line L7 through a switch S1 and the line L4 with the output of the integrator **88**. The line L9 connects the pole of the capacitor C1 facing towards the integrator **88** in FIG. **6** with a line L10, which stands in connection through the lines L11, L12 and respectively L13, with the switches S4, S7 and, respectively S6. Connected to the other pole of the capacitor C1 is a line L14, which is connected through the switch S3 with the reference voltage AGND=1.25 volt. A line L15 stands in connection with line L14 and connects through the lines L16, L17, and respectively L18, the pole of the capacitor C1, which faces away from the integrator **88** in FIG. **6**, with the switches S2, S1, and respectively, S8. The internal mass of the chips V_{SS}=0 volt stands through the lines L19 and, respectively, L20, in connection with the switches S8, respectively, S6. In this manner, through suitable opening and closing of the switches S8 and S6, the voltage V_{SS} can be applied to both poles of the capacitor C1. The input voltage V_{IN} which is to be digitized stands in connection with the switches S1 and, respectively, S7, through lines L21 and, respectively, L22. In this manner, through suitable opening and closing of the switches S1 and S7, the input voltage V_{IN} can be applied to either of the two poles of the capacitor C1. The reference voltage V_{REF} which determines the resolution of the A/D converter is connected through lines L23 and, respectively, L24 with the switch S2 and, respectively, S4. In this manner, the reference voltage V_{REF}, which, for example, consists of 150 milli-volt, can be applied to one of the two poles of the capacitor C1. The switches S1, ... S8, SR and SI are preferably CMOS switches, especially CMOS transmission gates. The connection of the input voltage V_{IN}, the reference voltage V_{REF} and the mass V_{SS} with the input capacitor C1 of the A/D converter is known in the technology. Inventively there is connected through the switch S3 a reference voltage AGND=1.25 volt ($\neq V_{SS}$=0 volt) to the input capacitor C1. Similarly, through the inventive circuit, V_{IN}, R_{REF} and AGND can be applied to both sides of the input capacitor C1, which presently causes a charging up at different polarity of the capacitor C1.

In FIG. 7, there is illustrated the operation of the A/D converter in a phase diagram. Thereby, S1 through S8, SR and S1 designate the switches of the A/D converter **66** pursuant to FIG. 6, and CK is the pulse signal of the comparator **89** in FIG. 7. CK' represents a further tapped-off pulse signal.

In the diagram, the switch conditions fluctuate between 0 and 1, whereby 1 signifies that the switch is closed, whereas 0 stands for the opened switch. The operation of the A/D converter can be divided into four phases which are designated with I, II, III and IV whereby I designates a RESET or resetting phase; II an integration phase, III and inverting phase and IV an integration phase of the input voltage of reverse polarity or sign. The cycle is more finely subdivided into steps i, - - - xiv. As shown as step i in FIG. 7, during the reset phase I, only the switch SR is closed, whereas all other switches are opened. This causes a discharge of the capacitor C2. At the beginning of phase II, as indicated as step ii, in FIG. 7 the switches S1 and S6 are closed, whereas all remaining switches remain further open. This causes a charging up of the capacitor to a charge $\Delta Q=C1\times(V_{IN}-V_{SS})=C1\times V_{IN}$. In step iii, the switches S3 and S5 are closed, whereas all other switches remain open. One pole of the capacitor is now set to the potential AGND, whereas the other pole of the capacitor C1, through closing of the switch S5, stands in connection with the capacitor C2. There now takes place a charge transfer from the capacitor C1 to the capacitor C2. Inasmuch as the integrator **88** resultingly causes the two input potentials to be equalized, there is present at the output **91** of the integrator **88** the output voltage V_{OUT} equal $-(C1/C2)\times V_{IN}+AGND$. In step iv all switches are opened and the comparator pulse CK is 1, meaning, the comparator **89** carries out a comparison between V_{OUT} and AGND. Upon the result of this comparison there now depends the further cycle. The representation of the switch conditions in step v must be understood in the following manner: In step v the switches S2 through S8 are not closed, but the switches S2 and S6 are closed, and S1, S3, S4, S5, S7, SR and SI are open, in the event that the output of the comparator is 0, in effect "low", while the switches S4 and S8 are closed and S1, S2, S3, S5, S6, S7, SR and SI are open when the output of the comparator is 1, meaning, "high", and in other instances remain open. When the output of the comparator is 0, meaning the output voltage V_{OUT} is lower than AGND, then the switches S2 and S6 are closed. At the capacitor C1 there are now present V_{REF} and V_{SS}. In the instance in which the output of the comparator is 1, meaning, V_{OUT} is higher than AGND, then the switches S4 and S8 are closed, whereby similarly V_{SS} and V_{REF} are present at the two poles of the capacitor C1, but with the reverse sign or polarity than in the instance in which the output of the comparator is 0. In step v, the switches S1, SR and SI are opened, and in step vi, the switches S3 and S5 are closed (compare step iii) which causes the capacitors C1 and C2 to be interconnected. As in step iii, voltage AGND is applied to one pole of the capacitor C1. There again, in turn takes place a charge transfer between the capacitors C1 and C2, as result of which a voltage $-(C1/C2)\times V_{REF}+AGND$ is added to or, respectively, subtracted from that of the output voltage of the integrator **88**, in accordance with the result of the comparison by the comparator in step iv. During the steps i through vi of phase II there is processed an input voltage which is phase shifted with respect to AGND, with

a reference voltage which is shifted relative to AGND. Similarly, at the non-inverted input of the integrator **88** and the inverted input of the comparator **89** there lies AGND, which causes that the output voltage is referenced to AGND and causes a comparison by the comparator **89** not with V_{SS}=0 voltage, but with AGND=1.25 volt.

In the following there is now discussed phase III consisting of steps vii to ix. In this phase, a sign or polarity reversal is implemented for the output voltage V_{OUT} of the integrator **88** with reference to AGND. During the entire phase III the switch S3 is closed. The closure of the switch S3 during the phase III causes the voltage AGND to be applied to one pole of the capacitor C1, as a result of which the voltage V_{OUT} is also inverted with regard to AGND and not with regard to V_{SS}=0, as in the known A/D converters. In step vii there is now closed the switch SI, whereas all remaining switches are open, except switch S3. This causes that the voltage V_{OUT} is temporarily in the capacitor C1, such that in step viii all switches are opened except switch SR. The switch SR is in effect closed, which causes a discharge of the capacitor C2. In the step ix the switch S5 is closed additionally to switch S3, while all remaining switches are opened. This causes that the negative voltage which is phase shifted at AGND is present at the output of the integrator **88**. The negative sign is obtained, as previously through the charge transfer from the capacitor C1 to the capacitor C2. In step x of Phase IV, the switches S7 and S8 are closed, whereas all remaining switches are opened. Compared with the step ii the input voltage V_{IN} is present with a reverse polarity at the capacitor C1. This causes a change in the sign of the integration of the input voltage, which is also well recognizable in FIG. **6** of the above mentioned publication of Jacques Robert et al. The steps xi through xiv correspond with the steps iii through vi, meaning, there is implemented an integration of the input voltage (only due to step x with a reverse sign of V_{IN}), and in accordance with the result from the comparator **89** in step xii V_{REF} is added or, respectively, subtracted after the integration (in case C1=C2). For a 14-bit A/D-converter, after implementing step i there is carried out phase II ($[2^{14}-2$ (for the phases I, and III)]:2=8191 times), as well as phase IV. The output of the comparator is connected to a up/down counter, which each time, in accordance as to whether V_{REF} is added or subtracted, increases or lowers its count condition by 1. The result of the counter is then a 14-bit representation of the ratio of V_{IN} to V_{REF}. The phases III and IV are necessary since through the integration with reverse signs of V_{IN} offset errors encountered in, for example the operational amplifiers, are reported or, respectively eliminated.

The multi pin connector **30** includes two pins for the system management bus interface **75**, which include a serial clock I/O line **38** and a bidirectional serial data I/O line **40**. These lines are connected to the SMBCLK and SMBD data pins, respectively, of the hybrid IC **32**. As explained generally above, and, in greater detail below, the smart battery module **28** communicates with the host device **16** and the smart charger **22** over the system management bus and data line **40** to communicate both stored battery parameters and calculated battery parameters.

The smart battery **10** also includes a separate thermistor R_{NTC2} which is connected across the negative terminal of multi-pin connector **30** and a temperature or thermistor line **42**. Thermistor R_{NTC2} may be used independently by the smart charger **22** to determine battery temperature, in a manner similar to that previously described with respect to R_{NTC1}.

A positive digital power supply voltage is obtained from the plurality of rechargeable battery cells **44**, and supplied to the hybrid IC through pin V_{DD} as the positive power supply voltage for the chip. It should be understood that the supply voltage for the hybrid IC does not necessarily have to be obtained at the battery midpoint **46**, but should be obtained at a point from the battery cells in order to receive a voltage of approximately 3 to 4.8 volts, i.e., the equivalent voltage of three (3) cells. As will be hereinafter explained in greater detail, the use of a battery midpoint for the positive voltage supply enables the hybrid IC to remain powered even when the battery is accidently shorted and removed from terminals **31–33**, and enables the A/D converter **60** to determine whether the battery is discharging or being charged as will hereinafter be explained in greater detail. Suitable fuse elements (one of which is shown in FIG. **2**(*a*)), and a positive temperature coefficient (PTC) elements (one of which is shown in FIG. **2**(*a*), are provided in series with the battery pack cells to protect the battery from very high current and excessive temperatures caused by a temporary short circuit across the battery terminals or other thermal event.

As shown in FIG. **2**(*b*), the hybrid IC **32** further includes RAM memory **65** which can store up to 128 8-bit registers for communication of calculated battery parameters, and a ROM memory **67** for storing look-up table values utilized in the battery capacity calculation algorithm (explained in detail below). The exact amount of RAM, ROM, and program ROM memory is a design choice, and these values change as the ratio between calculated and preset parameters vary.

As shown in FIG. **2**(*a*), the addition of capacitor C4 acts as a buffer to maintain the integrity of the RAM memory contents in the case of a battery short-circuit or temporary power loss. Preferably, the capacitor C4 is connected to the negative analog voltage supply terminal, and its value is chosen to ensure that a source of supply voltage is supplied to the embedded memory (RAM) for a time dependent upon the RAM leakage current. In the preferred embodiment, the power to RAM memory is unlatched if a temporary short circuit condition exists, However, capacitor C4 preferably of capacitance 330 nF, provides a source voltage to the RAM for a period of time necessary for the PTC element to ramp to a high resistance value. The PTC element will create a high impedance between battery terminals when a short circuit across the battery pack terminals creates a high circuit drain.

The hybrid IC **32** further includes up to 4 kbytes of additional ROM memory IC for addressing and storing the various algorithms, subroutines, manufacturer data, and data constants utilized by the smart battery module for calculating the battery capacity, sending messages such as alarms and battery charger control commands etc., and handling message requests from external devices.

The programmable ROM generator is implemented by means of a metal mask (not shown) as opposed to conventional ROM generation by means of diffusion masking. In accordance with the information which was to be permanently stored, transistors were generated in a matrix arrangement through diffusion, whereby the information was coded in the plane through the distribution of the transistors in the diffusion step. Thus, the ROM generator generates in effect, a ROM matrix, whereby the presence or respective absence of an MOS transistor stands for a logic "0" respectively "1." A disadvantage of a ROM matrix with the programmable level of diffusion is that the diffusion process, which is incorporated as one of the first steps of a CMOS process, can not be changed when there is a change in ROM contents, thus, rendering impossible the production of wafer stock for a particular type of ROM.

By contrast, the advantage of a ROM matrix programmable in a metal layer is that wafer stock with the same basic layers up to the metal may be fabricated. Thus, a microprocessor family with different ROM contents can be realized with low cost and fast turn around time. Additionally, the pre-manufacture of a portion of the ROM with the flexibility of programming in application specific information in the upper or respectively later produced layers, is possible.

The hybrid IC chip itself may comprise thirteen or fourteen layers, with the 9^{th} or 10^{th} layer (i.e. one of the upper layers) being a layer of metal, wherein the distribution of the metal is characteristic for the storing contents of the ROM. Thus, in the hybrid IC ROM manufacturing process, nine (9) layers are grown and the next four ROM programming layers are grown dependent upon the customer's particular needs (i.e., special properties of the battery pack).

FIG. **9**(*a*) shows a ROM matrix with the metal layer as a programmable layer. A MOS transistor, e.g. **71**(*a*) for the matrix is always present on the matrix and will either serve as a logical "0" or "1". Specifically, FIG. **9**(*a*) schematically illustrates the ROM **67** of the smart battery device that is programmed according to the unique process as follows: The represented ROM matrix consists of eight word lines **67***a* and indicated as WZO, . . . , WZ7 and 8 spaces **67***b* and indicated as SPO, . . . , SP8, whereby the spaces SP1, SP3, SP5, SP7 connect with a virtual ground line **73**. At each location of the matrix, there is produced a transistor in the diffusion step, three transistors **71***a*, **71***b*, and **87** of the matrix are shown in FIG. **9**(*a*). For the programming of a logic "0," in a respective word line, the drain or respective source electrodes of a transistor are connected to a metal mask with the corresponding source or respectively drain electrodes of the joining transistors or the joining transistor. The drain or respective source electrodes of such a transistor are connected with the gap lines or, respectively, the virtual ground lines **73**. Transistor **71***a* in word WZ7, as shown in FIG. **9**(*a*), is programmed for a logic "0" as its drain terminal is connected with the source terminal of connecting MOS Transistor **87** which is tied to virtual ground line SP7.

Logic "1" in contrast therewith is probed in, in that the drain or respectively source electrodes are connected to a common line, preferably, as can be ascertained from FIG. **9**(*a*), to a gap line SP**0**, SP**2**, SP**4**, SP**6**, SP**8**. Thereby, the transistors, such as the transistor **71***b* of word WZ**0** as shown in FIG. **9**(*a*), are short circuited.

The connections of the transistors are thus initially determined with the application of the metal mask. In the usual manner two (through contacting) metal masks are applied on the ROM. In should be understood that in this instance preferably the lower of the two metal masks, meaning the mask which is located closer to the transistors, is employed for the short circuiting and the connection of the applicable transistors. Inasmuch as the transistors are short circuited, this does not influence the operation of the metal mask which is employed for the contacting. Since this metal mask is usually one of the uppermost layers, for example the tenth of about 14 layers, the inventive ROM can be pre-manufactured up to the ninth layer and then programmed and manufactured in accordance with the application.

In FIG. **9**(*b*) there is illustrated a usual programmed ROM. It can be ascertained from FIG. **9**(*b*) that the transistors, which are short circuited in FIG. **9**(*a*), are in any event not produced in the diffusion mask. As shown in FIG. **9**(*b*), the transistor **71***c* which is not present corresponds to a short circuited transistor **71***b* in the metal mask pursuant to the process described above.

Each of the algorithms, subroutines, manufacturer data, and data constants stored in ROM and utilized by the smart battery module for calculating the battery capacity, etc. as mentioned above, will now be explained in further detail below. Further details of the smart battery algorithm for reporting battery parameters to an external device is found in applicant's co-pending patent application U.S. Ser. No. 08/318,004 assigned to the assignee of the instant invention and the disclosure of which is incorporated by reference herein.

As shown in FIG. **3**, the battery operating system **10'** will first perform an initialization routine **100** that is initiated upon system power up, enabled by a power ON signal/reset impulse signal **11**, or, enabled by a wakeup from STANDBY signal **13** which is generated after the microprocessor has determined that it should exit the standby mode. As shown in FIGS. **2**(*b*) and FIG. **10**, the hybrid IC **32** is provided with a power-on reset circuit **85** which generates a reset impulse signal **11** to activate the external crystal oscillator **36** and reset the system every time the power supply voltage is applied to the ASIC. Specifically, this reset impulse initiates the start of the external crystal oscillator **36** to provide the precise triggering of the internal 450 kHz oscillator for providing the time base for the hybrid IC components. The threshold of this circuit is between 1.2V and 1.6V depending upon the type of transistors used in the circuit of FIG. **10**.

More specifically, as illustrated in FIG. **10**, the power-on reset circuit **85** is provided with a transistor network Comprising n- and p- channel transistors that are tied to hybrid IC voltage supply V_{DD}. When V_{DD} is sensed as dropping between 1.6 V to 2.0 V, or, in the case of battery short circuit 0.0V, the transistors of circuit **85** generate a RAM memory de-latching signal **79** which turns off PMOS- transistor **85'** and effectively de-latches RAM memory **65**. As mentioned above, the voltage on buffer capacitor C**4** will keep RAM memory contents alive for period dependant upon RAM leakage current.

After a power on/reset signal **11** is received, or, after the sleep mode is exited, the system is placed in a standby mode **23** (FIG. **3**) until it is triggered by trigger signal **17** generated by the external oscillator **36** which provides the trigger for the system operations (capacity calculation) every 500 msec, or, is awakened by a bus request signal **15** as will be explained in further detail below. In the battery "standby" mode, the microprocessor is in an idle state until the operating cycle trigger **17** or external bus request signal **15** is received.

Initialization of Algorithm Variables

The initialization routine, which is described and shown (in FIG. **4**) of the above-mentioned, copending patent application (U.S. Ser. No. 08/318,004), is conducted at the virginal start of the system. The initialization routine functions to clear all values to be stored in the system RAM and to assign all system default values. Preferably, many of the default values are constant values and are available in case of an emergency situation wherein all RAM memory has been lost while the system was in the STANDBY mode.

On power-on-reset as well as on a wakeup from the STANDBY mode of the chip (explained below), the program is started at an initial memory address. A "checksum" test is conducted for checking whether the RAM memory is valid whereby the capacity calculation is continued, or, whether the emergency mode (which uses ROM defaults) will be activated. Such an instance occurs when the chip switches into the STANDBY mode at low battery voltage and then back into the ON mode when the battery is to be recharged.

If the "checksum" test fails, the μP will first clear all RAM banks completely, and, as consequence an internally gener-

ated CALIBRATED flag will be cleared and the number of cells of the battery pack has to be learned, a process to be explained in greater detail below. Next, the default values (described below) are transferred from ROM to RAM. To prevent exceptions in the capacity calculations to be described hereinbelow, it is imperative that variables do not have undefined values. This enables the algorithm to work in a catastrophic emergency mode in the event that all RAM memory has been lost. The default values of critical variables may then be substituted by correct values when the battery system is reformatted at a battery service station using the original manufacturer's data.

Included in the initialization routine will be an initialization of FullChargeCapacity "full_cap", RelativeStateOfCharge "SOC" and the RemainingCapacity "Itf" values, as well as state and other variables to ensure a proper start of the capacity calculation. Then, the program resets all system timers such as the calculation of voltage, temperature and selfdischarge timers before passing out of the initialization routine. The capacity calculation will then initiated at each trigger signal **17** which is delivered every 500 msec by the external 32 kHz crystal **36**.

As explained above, the default values are necessary to ensure that upon a power-on/reset, the rechargeable battery capacity calculation (explained below) may be executed. The preferable nominal default values for the critical parameters used for the capacity calculation algorithm **151** and explained in detail in copending patent application (U.S. Ser. No. 08/318,004), are set forth as follows:

The DesignCapacity (theoretical or nominal capacity, hereinafter "nom_cap") may range between 1700 maH to 2400 mAH, but, after a memory loss, the capacity calculation algorithm defaults to a preferred value of 2000 mAh and the new capacity is relearned from that level; the default value of the number of battery cells in the rechargeable battery pack is 6 cells, however, this value may be changed depending upon the actual configuration of the battery pack; The AL_REM_CAP value represents the remaining capacity alarm triggering value and may range from 50 mAh to 500 mAh. Preferably, AL_REM_CAP has a default value (AL_REM_CAP_DEF) of 200 mAh. An alarm condition exists when the remaining capacity is below this value (without taking into account the remaining capacity after EDV due to current and temperature (i.e., the residual capacity correction)). The AL_REM_TIME value represents the estimated remaining time at the present discharge rate and may range from 1.0 min. to 20 min. Preferably, AL_REM_TIME has a default value (AL_REM_TIME_DEF) of 10 minutes. This alarm condition exists while the calculated remaining time to voltage breakdown (EDV), based on the minute average current (discussed below), is below the value of AL_REM_TIME and will automatically be disabled when the battery is in the charging mode. The AL_DTEMP value represents the dT/dt alarm trigger condition and may range from 1° K./min. to 5° K./min. Preferably, AL_DTEMP has a default value (AL_DTEMP_DEF) of 2° K./minute. This alarm condition will exist when the battery detects that the rate of its internal thermal rise (dT/dt) is greater than the AL_DTEMP value. The AL_HI_TEMP value represents the high temperature alarm trigger and may range from 310° K. to 345° K. Preferably, AL_HI_TEMP has a default value (AL_HI_TEMP_DEF) of 328° K. Additionally, when the capacity calculation is started by power-on-reset, the FullChargeCapacity, ("full_cap" represents the learned full charge capacity of the battery), will be initialized to the DesignCapacity (nom_cap); the RemainingCapacity ("Itf") to ⅛ of the full_cap; and, the RelativeStateOfCharge ("soc") to 12.5% and the battery state to capacity decreasing, and, specifically, to selfdischarging mode. The alarm timer N_ALARM is set at 10 seconds and this is the amount of time that an alarm condition will be broadcast between a host device and/or a battery charger as will be explained in further detail below. It should be understood that these values are typical values for a NiMH battery intended for use in a portable computer. Other types of battery chemistry, or portable devices, may call for a different set of default values.

As shown in FIG. **3**, after the system is initialized at step **100**, the battery will enter into a standby or maintenance mode **23** where it will either awake upon a bus-request signal **15** or awake upon the external crystal trigger signal **17** every 500 msec. If the battery is awaked by a bus request signal **15** as determined at step **21**, then the battery will handle the request by the handle request routine indicated at step **25** where it will thereafter exit into the standby mode. The routine for handling the requests **25** will be explained in further detail below.

If the system is triggered by the normal external crystal trigger signal **17**, and there are no bus requests, then the program disables the bus requests (approximately 37 msec before the trigger signal) and enables the A/D converter to begin the current, voltage, and temperature measurements for the current operating cycle as shown at step **130** in FIG. **3**. A "getvalues" status flag is then checked at step **139** to determine whether A/D conversions of the raw current, voltage, and temperature measurement values are to be performed. When this flag is set high (logic level =1), the raw current, voltage, and temperature values of the rechargeable battery are obtained for the current trigger cycle as shown at step **140**. These raw A/D current, voltage and temperature values are built into a special function register **61**, as shown in FIG. **2**(*b*), which is one of sixteen such registers provided in the hybrid IC for subsequent storage in RAM as I, U, or T. If the "getvalues" flag is low (logic level=0), then no raw current, voltage, and temperature measurements will be obtained for the present cycle, and the getvalues flag will toggle high (logic 1) at step **148** and the process will continue as shown in FIG. **3**.

After new current, voltage, and temperature values are obtained (step **140**), the A/D measurements ready flag is set high (logic level=1) at step **141**, and a check is made at step **142** to determine whether the system is in a sample mode. Thus, at step **142**, if the absolute value of the raw current, |I|, is determined to be below a threshold value of 10 mA, then the battery system will operate at half the sample rate depending upon the status of the sample mode flag. Thus, at step **143** in FIG. **3**, a determination is made as to whether the sample mode flag is low (i.e., logic 0) or high (logic 1). If the sample mode flag is low, then the sample mode flag will toggle to a high level at step **144**, and the system is placed in a sample mode and the process proceeds at step **149** to initiate the A/D conversion. If the sample mode flag is already high (from the previous cycle), then the "getvalues" flag is set equal to zero at step **146**, and the A/D converter is disabled at step **147**. The A/D conversion will not occur (to save power) and the algorithm proceeds to the capacity calculation (step **151**). The "getvalues" flag is always set low in the sample mode. The status of this flag ensures that an A/D conversion will be skipped, and, as a consequence, no new valid data will be available for the capacity calculation at step **150**.

If the raw current, |I|, is determined at step **142** to be above the 10 mA threshold, then the battery system will exit the

sample mode (and the sample mode flag is set at logic 0) at step **145**, and the A/D conversion of the raw current, voltage, and temperature values will be performed at step **149**. At step **150**, a determination is made as to whether the A/D measurement ready flag is high (logic 1) indicating that valid raw battery parameter data has been received. If it is set high, then the capacity calculation and attendant battery characteristic conversions (voltage, current, and temperature) will be performed. If the A/D measurement ready flag is low (logic 0), then the capacity calculation is not performed in the current cycle, and the process proceeds to step **158** where the bus request line for message transfer is enabled and the hybrid IC is placed in the sleep mode at step **23**. The oscillator trigger **17** continues to wake up the microprocessor every 500 msec, however, when the current is less than 10 mA, the A/D conversions and the capacity calculations may be performed at an arbitrarily determined rate that is less frequent, for e.g., once every two or once every five seconds, to conserve power.

FIG. **8**(*a*) illustrates the timing of the operating cycles under normal mode operating conditions **57***a* as compared when the system operates under sample mode conditions **57***b* explained below. As shown in FIG. **8**(*a*) and, as mentioned above, the 32 kHz external crystal delivers the trigger signal **17** every 500 msec to initiate the raw voltage, current, and temperature measurements, indicated as **158**. Also initiated is the capacity calculation **160** which utilizes the current, voltage, and temperature measurements of the previous operating cycle. When the raw current value obtained is determined to be below a threshold value of 10 mA, the battery system will operate at half power, and no measurements will be taken during the next 500 msec operating cycle as indicated as **58***b* in FIG. **8**(*a*). However, measurements are taken one second later at the next operating cycle as indicated as **58***c*. When the raw current value obtained is determined to be above a threshold value of 10 mA, the battery system will resume normal mode operation and during the next and subsequent operating cycles, the capacity calculation and attendant battery characteristic measurements (voltage, current, and temperature) will be taken.

FIG. **8**(*b*) illustrates the approximate time durations for the various measurements. As a matter of design choice, the capacity calculation **160** is performed in approximately 71 msec for each operating cycle. Thereafter, the alarm control subroutine **152** will be performed for a duration of approximately 29 msec and the charger control subroutine **154** will be performed for a duration of approximately 2 msec if the smart battery determines these operations are to be performed (see FIG. **3**). The LED display routine **156** may be performed if it is requested by a user and the LED display control functions will take place for approximately 23 msec as shown in FIG. **8**(*b*). It should be understood that the aforementioned performance times for the various routines may vary due to the accuracy of the internal 455 kHz oscillator, which may vary with temperature. Each of the alarm control subroutine **152**, charger control subroutine **154** and LED display subroutine **156** will be explained in further detail below.

Since the system management bus request line is inactive during the capacity calculation, alarm control, charger control, and LED display routines, the microprocessor will be unable to receive requests from a host device or battery charger as indicated for the time duration **158** for each operating cycle shown in FIG. **8**(*a*). Therefore, in each operating cycle, after the capacity calculation has been performed, the System management bus request line is enabled for the remaining time of the 500 ms cycle, as indicated in FIG. **8**(*b*), so that it may respond to a request from a host device or charger. Concurrently, the battery places itself in the standby mode **23** whereupon it will be awaked for the next cycle upon receipt of the system trigger signal **17**, or, be awakened by a bus request signal **15** as shown in FIG. **3**. For a remaining 37 msec of each operating cycle, the bus request is again disabled as shown for the time duration **158** prior to the next trigger signal **17**. As mentioned above, each system trigger signal **17** initiates the start of the internal clock **48** generating the 455 kHz signal for controlling the hybrid IC, microprocessor, A/D converter, etc.

Algorithm for Calculating Battery Capacity

The purpose of the capacity calculation is to continuously monitor the capacity of the rechargeable battery in accordance to the formula indicated by equation (1) as follows:

$$CAP_{rem} := CAP_{rem} + \Sigma \epsilon_c I_c \Delta t_c - \Sigma I_d \Delta t_d - \Sigma I_s \Delta t_s \quad (1)$$

where CAP_{rem}, also referred to hereinbelow as Itf, and indicates the remaining capacity in the battery at any given time expressed as mAh (milliamperehours); the $\Sigma \epsilon_c I_c \Delta t_c$ term represents the sum of the incremental increases in capacity as the battery is being charged and takes into account a charge efficiency factor ϵ_c accessed preferably from look-up table values to be explained in further detail below with respect to FIG. **22**(*c*), or, alternatively, may be obtained from a response equation or by interpolating between several points stored in memory; a $\Sigma I_d \Delta t_d$ term which represents the sum of the continuous decrease in battery capacity due to discharge associated with the battery's usage; and a $\Sigma I_s \Delta t_s$ term which represents the predicted and measurable amount of self-discharge based upon self-discharging effects associated with the battery's chemistry and is a function of the battery state of charge and temperature. By knowing the RemainingCapacity, Itf, at all times, it is possible to provide battery parameter information useable by a host computer (PC) or smart battery charger to ensure safe and reliable battery use and to ensure prolonged battery life.

FIGS. **13**(*a*) through **13**(*b*) illustrate the capacity calculation routine performed for the rechargeable battery pack at each trigger cycle. In parallel, the current, voltage and temperature measurements are running except when in the "sample" mode where these measurements are taken once every second. The sample mode is designed to save power consumption (i.e., the A/D conversions occur at half-frequency) and is switched on and off depending upon the amount of detected current. For example, when the current falls below 10 mA, the "sample" mode is enabled and less frequent measurements are made.

Normally the temperature, voltage and current are measured and updated once per cycle. The current is measured with an integrating method (explained in detail below), which recognizes its changes during the conversion time. All output values taken from SMBus requests and capacity calculation are one period delayed. The A/D measurements are controlled by an on-chip oscillator at nominal 455 kHz and the operating cycles—responsible for the integration time—by the precise 32 kHz oscillator. The lower accuracy of the absolute frequency value of the on-chip oscillator has no influence on the accuracy of the measurement.

As shown in FIG. **13**(*a*), at step **200**, the first step of the capacity calculation, the IUT Calculation routine **200** is performed to first convert the raw analog/digital converter output data from register **61** (FIG. **2**(*b*)) into values having appropriate units useful for the capacity calculation algo-

rithm. Details of the IUT Calculation routine can be found in the above-mentioned, co-pending patent application (U.S. Ser. No. 08/318,004). Briefly, as illustrated in FIG. **12**, at step **205**, the raw A/D Current measurement, I_raw, is scaled and converted to the actual current value "I" in units of milliamps. Similarly, the raw A/D pack voltage measurement, U_raw, is scaled and converted to the actual battery pack voltage value "U" in units of millivolts. Next, as indicated at step **212**, the μP checks the battery pack voltage "U" to determine whether or not the individual cells of the battery pack have an output voltage less than 0.9 V. If a cell is detected as outputting a voltage less than 0.9 volts, then the battery pack is placed in a Sleep mode, as indicated at step **212'**. As shown in FIG. **12**, the following actions take place when the battery state changes between an ON and SLEEP mode:

To save battery power and minimize current drain, the μP proceeds to switch off: the A/D converter **60** at step **213** and 455 kHz on-chip oscillator at step **216**. While in the sleep mode, the RAM memory contents are kept alive by voltage from the battery with only memory leakage current drain (which is dependent upon the amount of RAM). Additionally, the wake-up comparator circuit **80** (FIG. **11**) is activated at step **217** and then the μP sets a bit flag to tell the hardware to start a special voltage control logic to set itself for sleep, as indicated at step **218**.

As shown at step **219** in FIG. **12**, and, as illustrated in FIG. **11** the wake-up comparator circuit **80** is periodically activated by a trigger signal **77***a* derived from the external 32 KHz oscillator. At each period, the comparator is turned on to compare the ratio of pack voltage signal **82** with the predetermined bandgap reference voltage signal **83** that is supplied from the bandgap reference circuit **62** (FIG. **4**) and input to the inverting input of comparator **76**. For a three cell battery pack, the bandgap reference voltage **83** is approximately 1.239 volts, but, this value may be changed in accordance with the battery pack design. When the ratio of pack voltage signal **82** V_{DD} of the ASIC has increased above reference voltage signal **83**, then the comparator circuit will toggle, as shown at step **220**, to awake the μP and enable the A/D converter again to take measurements, as indicated at step **221**. The capacity calculation will then continue with an initialization at step **100**.

A detailed schematic of the wake-up comparator circuit **80** is shown in FIG. **11**. As shown in FIG. **11**, the wake-up comparator circuit **80** comprises a voltage divider comprising resistors R4 and R5 which are tied to the V_{DD} ASIC power supply to supply a ratio of V_{DD} pack voltage (signal **82**) to a first non-inverting input of a comparator **76**. As will be explained in further detail below, an NMOS (n channel MOSFET) transistor switch **89***b* connected between resistor R5 and ground is nominally turned off in sleep mode to prevent battery current drain to ground, but, is periodically turned on once every 500 milliseconds (30 microseconds) by trigger signal **77***a* to enable the divided V_{DD} voltage to appear at the non-inverting input of the comparator **76**. Simultaneously, the external oscillator trigger signal **77***a*, triggers the wake-up comparator circuit **80** by simultaneously turning on the transistors **89***a,b* to enable comparator **76** operation. As shown in FIG. **11**, a low power current source **90** which is derived from the battery by external circuitry, turns on transistor switch **89***a*, to provide a reference current to comparator **76**. From this current source **90**, the working point of the comparator is fixed. Additionally, enable line **15***a* is tied to signal **77***a* to simultaneously enable the comparator to take a measurement. Transistor switch **89***b* is turned on by signal **77***b*, which is output from inverter **72**, to create a path to ground to enable V_{DD} voltage divider signal **82** to appear at the comparator input so that the comparison may be made.

When the V_{DD} ratio is low (<0.9 V/cell) and the ratio of pack voltage signal **82** is less than the A/D converter bandgap reference signal **83**, then the comparator output signal **13** is low. When V_{DD} rises above the reference voltage **83**, i.e., 3.33 Volts (1.11 volts per cell for a three-cell battery pack) the wake-up (comparator output) signal **13** goes high, thus, allowing normal sample mode operation to resume. As shown in FIG. **11**, element **78** is a Schmitt trigger device which is a bistable device that is provided at the output of the comparator **76** to prevent spurious oscillations appearing at the output of the comparator **76** that might be due to comparator switching characteristics and/or amplifier noise.

Due to the low power consumption of the MOS circuitry implemented in the hybrid IC, the total current consumption of all operating components while in the sleep mode is no greater than approximately 2.0 μamp (microamps).

Referring back to FIG. **12**, as long as each cell is detected as outputting a voltage greater than 0.9 volts, the capacity calculation continues, and, at step **215**, the raw A/D pack current temperature measurement, T_raw, is converted to the actual battery pack temperature in units of degrees Kelvin. This temperature value is additionally scaled to take into account thermistor scaling values, (not shown), and a final current temperature value of "T" is obtained. At step **222**, the condition of the battery is checked to determine if an over temperature condition exists, where a temperature of 328° K. or greater is detected. When detected, a temperature alarm condition flag, HI_TEMP_ALARM, is set. If capacity is increasing and the over temperature condition exists then a TERMINATE_CHARGE_ALARM flag will be set indicating that one or more of the battery's charging parameters are out of range.

At this point, it should be mentioned that an end of charge condition may exist (if the capacity is increasing). This end of charge condition may be detected when the rate change in voltage or temperature taken between successive measurements is at a certain gradient. Thus, as shown in FIG. **12** at step **224**, and described in detail (steps **240** through **249** of FIG. **5**(*b*)) in co-pending patent application (U.S. Ser. No. 08/318,004), the change in temperature dT/dt calculation is performed. Additionally, as shown in FIG. **12**, a change in voltage dU/dt calculation is performed at step **227**.

The change in temperature (dT/dt) calculation is performed to evaluate the difference dT between the current temperature value T and a previous temperature value determined at a time 20 seconds previously, but may range anywhere from 10 to 120 seconds previous. After the dT calculation is performed, a determination is made as to whether the amount of internal temperature change exceeds the allowable rate, i.e., whether the AL_DTEMP alarm condition exists, as shown at step **226** in FIG. **12**. A temperature change of approximately 2° K./min or greater indicates an AL_DTEMP alarm condition and, when detected, an alarm condition flag, DTEMP_ALARM, is set.

The change in voltage (dU/dt) calculation is performed to evaluate the difference dU between the current voltage value U and a previous voltage value determined at a time preferably 255 seconds previous.

After the dU calculation is performed, a determination is made at step **260** as to whether the capacity is decreasing, and, as to whether the present voltage U is less than the end of discharge voltage (EDV) limit (typically 0.9 V/cell), indicating that an end of discharge condition EOD_U exists.

Thus, the present voltage value U is compared to the preset end of discharge voltage (Uempty) to determine if it is less than this voltage. If an End of Discharge condition for voltage exists, then an EOD_U flag is set at step **262** and a Terminate_Discharge_Alarm flag is set indicating that the battery has supplied all the charge, and is now nominally fully discharged. If an End of Discharge condition does not exist, then the EOD_U flag and the Terminate_Discharge_Alarm flag are cleared at step **264**. Additionally, at step **264**, the capacity reset flag is disabled. The IUT_Calculation procedure **200** is then exited and the capacity calculation continues at step **165** in FIG. **13**(*a*).

At step **165** of the capacity calculation routine **151** of FIG. **13**(*a*), a calculation of the rolling minute average current is performed utilizing the recent previous current (I) measurements. Rolling minute average current calculations are important for calculating battery conditions such as "average time to empty" which is based on the average current drain, and which might be requested by a host device, as will be explained in greater detail below. Then, at step **170** of FIG. **13**(*a*), a determination is made as to whether the present current (I) value is less than or equal to the selfdischarge current I_SELFD, which, in the preferred embodiment, is 3.0 milliamps but may range anywhere from 2.0 ma to 10.0 ma and represents the limit for a mode and battery state recognition. If the present current (I) value is less than or equal to the selfdischarge current then the state of the battery is determined to be capacity decreasing without any external drain. Consequently, a selfdischarge flag bit is set at step **175**. If the present current (I) value is greater than the selfdischarge current (3.0 mA), then the battery selfdischarge flag bit is cleared at step **172**. The battery selfdischarge current is always calculated regardless as to whether the battery is in a capacity increasing or capacity decreasing state. The direction of current is established at step **178** in FIG. **13**(*a*) to determine the present state of the battery. If the current (I) is determined to be a positive value, then the state of the battery is capacity increasing (hereinafter CI) and a capacity increasing flag is set at step **180**. If the current is determined to be a negative value, then the state of the battery is capacity decreasing (hereinafter CD) and a capacity decreasing flag is set at step **182**. If it is determined that the capacity is decreasing, then a determination is made at step **184** as to whether the end of discharge voltage (plus hysteresis) EOD_UH flag has been set.

For accurate battery parameter presentation and battery life predictions, it is important that the full battery capacity be reset after an end of discharge voltage condition (battery nominally fully discharged) has been detected. Even at a nominally discharged condition, some residual battery capacity remains and this is taken into account into the battery calculation, as will be explained below. Thus, a determination is made at step **189** as to whether the capacity reset flag has been set as a result of the EOD_UH flag having been set indicating that the battery pack end of discharge voltage has been reached has determined at step **184**), or, as a result of the battery self discharge flag having been set (as determined at step **175**), or, if capacity is increasing. If the capacity reset flag has been set, then, at step **190**, the remaining capacity (Itf) at the EOD voltage condition is reset to a predicted Residual Capacity "pd" value obtained from look up table depicted in FIG. **22**(*a*). Additionally, at step **190**, the error register is reset to zero and the capacity reset flag is cleared. The program then proceeds to the selfdischarge calculation and current integration procedures. If, at step **184**, the EOD_UH flag has been determined not to have been set, or, if the capacity reset flag had not been set as determined at step **189**, then the algorithm proceeds at step **192** in FIG. **13**(*b*).

As described in further detail (with reference to FIG. **6**(*b*) of co-pending patent application (U.S. Ser. No. 08/318,004), and in view of step **192** of FIG. **13**(*b*), a state change determination is made for determining whether the state of the battery has changed, i.e., whether the battery has changed from a capacity increasing (CI) state to a capacity decreasing (CD) state, or vice versa. This step is necessary to avoid the instance of false battery cycle counting or the inaccurate learning of the full charge capacity due to current pulse sign changes or breaks of the current flow.

As indicated from steps **300** to **325** of FIG. **13**(*b*), the selfdischarge calculation procedure is performed. Specifically, as described in further detail (with reference to FIG. **6**(*b*) of co-pending patent application (U.S. Ser. No. 08/318,004), a 128 second timer for the selfdischarge calculation is first decremented. Preferably, steps **305–325** of the selfdischarge calculation are performed once every 128 seconds. If the self-discharge timer has not timed out, the program proceeds to step **400** (indicated by broken lines) to perform the current integration procedure **400**, as shown in detail in FIG. **13**(*b*) and explained in further detail below.

Selfdischarge Calculation Routine

Due to the electrochemical nature of batteries the selfdischarging correction of the remaining capacity has to be calculated all the time, independent from the existence of any charging or discharging currents. This is because there will always be a self-discharge current drain regardless of whether the battery is being charged or discharged and the amount current drain is a function of the battery charge and temperature. Thus, as indicated as step **305** in FIG. **13**(*b*), the selfdischarge rate "s" as a function of the relative state of charge "soc" and current temperature T is accessed via a look-up table, shown in FIG. **22**(*b*) which shows a three-dimensional graphic representation of self-discharge current (vertical axis) as a function of relative battery state of charge and temperature. These look up factors "s" for selfdischarge give the predicted selfdischarge rate scaled by the design (nominal) capacity, and, as is shown in FIG. **22**(*b*), the amount of selfdischarge current, I_s, generally increases with increasing temperature and increased battery state of charge levels. For instance, at approximately 65° C. and a 95% relative state of charge, battery selfdischarge current might total an amount of up to 30% of the full battery capacity per day. The selfdischarge values depicted in FIG. **22**(*b*) were empirically derived and will vary, depending upon the battery chemistry and battery architecture.

At step **310**, a determination is made as to whether the state of the battery is capacity increasing or capacity decreasing. If the battery is in a discharging state, as shown at step **315**, the total amount of capacity decrease (current drained) since the last state change is calculated and stored in a separate register. If the capacity is increasing, then the program is directed to step **320**, where the effects of the selfdischarge rate are taken into account for the error calculation. Step **320** is also performed after the total amount of capacity decrease (current drained) since the last state change is calculated at step **315**. Then, at step **325**, the actual capacity integral "Itf" is decremented by the selfdischarge rate "s", thus, providing the $\Sigma I_s \Delta t_s$ in equation (1) described above. Afterwards, the self-discharge procedure ends and the current integration routine **400** is performed.

Battery Charge Integration Routine

When the battery is being charged, it is said to be in the Capacity Increasing state (CI), else it is in the Capacity Decreasing state (CD). CD includes the standby mode of the

battery, when no current flows through the battery terminals. In the standby mode, only the selfdischarging rate reduces the capacity.

The battery current will be precisely integrated during both charge and discharging states. The capacity integration itself is independent from the battery state, but, as will be hereinafter explained, look up tables (LUT) provide adjustment factors to enable more precise capacity adjustment. For instance, a first LUT (described below with respect to FIG. **22**(*c*)) comprises current efficiency factors dependent upon the battery relative state of charge, the C_rate (current), and the temperature; a second LUT comprising selfdischarging rates dependent upon relative state of charge and temperature; and, a third LUT with residual capacity corrections dependent upon the discharging current rate and temperature which give the fraction of the full capacity which can be extracted from the battery under relaxed conditions after the battery has reached an end of discharge voltage condition at a given current rate.

The flow diagram for the current integration process **400** is shown in FIG. **13**(*c*). As shown in FIG. **13**(*c*) the first step of the current integration process is to determine the magnitude of the relative state of charge (soc). The soc is defined as the actual capacity expressed as a percentage of the full charge capacity (i.e., the capacity of the battery when fully charged) and is used to estimate the amount of charge remaining in the battery. Thus, as indicated at step **405**, a determination is made as to whether the remaining capacity is greater than zero (0). If the remaining capacity Itf is a negative number, the full capacity is incorrect and must be learned and the soc value is clamped to zero (as indicated at step **412** in FIG. **13**(*c*). Otherwise, the soc calculation will take place at step **410**. As previously described, until the full charge capacity of the battery is learned, the full charge capacity is initialized as the design (nominal) capacity.

Next, as indicated at step **415** in FIG. **13**(*c*), the C_rate is calculated. The C_rate is defined as the rate at which it would take the energy source to drain in one hour and is measured in units of reciprocal hours. The C_rate calculation in step **415** is based on the actual current value (I) and the present full charge capacity value and is additionally scaled. A determination is then made at step **418** as to whether the battery is in a capacity increasing or capacity decreasing (discharging) state. If the capacity is increasing, then the battery is being charged and the charge calculation must take into account a charge efficiency factor, made available in a LUT for charge efficiency, accessible by the microprocessor, as graphically represented in FIG. **22**(*c*). Thus, at step **420** the charge efficiency factor dependent upon the charge current, relative state of charge (soc), and the temperature, is accessed. For instance, as shown in FIG. **22**(*c*), when the battery is charged to approximately 95% of full capacity, and the current is being charged at a 0.1 C_rate at a temperature of 45° C., the charge efficiency factor ϵ_c is found to be about 0.8. The charge efficiency factors are empirically derived and will vary depending upon the battery chemistry and battery architecture. The representations shown in FIG. **22**(*c*) are for a battery state of charge 95% and it is understood that charge efficiency values will vary considerably depending upon (remaining capacity) state of charge.

Finally, the increase in charge for the current time interval taking into account the actual current and the charge efficiency factor is calculated at step **435** to form the term $\epsilon_c I_c \Delta t_c$ in equation (1). This value will be used to increment the integration at step **445** as will be explained below.

If at step **418** it is determined that the capacity is decreasing, the amount of discharge will be integrated for the current discharge cycle as indicated at step **422** in FIG. **13**(*c*). It is next determined at step **425** whether the self-discharge flag had been previously set (see step **175**, FIG. **13**(*a*)) indicating that the battery discharge current is less than 3 mA, and that only the self-discharging processes need to be considered. If the self-discharge flag bit has not been set, a charge calculation is made at step **440** to increment the integration. The final integration is accomplished at step **445** wherein the charge increment calculated at either step **435** or step **440** is added to the remaining capacity Itf, and, as indicated in equation (1). Additionally, at step **445**, the charge is integrated for an error calculation and the running total of the error is also calculated as will hereinafter be discussed in detail.

If it is determined at step **425** that the self-discharge flag has been set (step **175**), then the battery is selfdischarging without any external correct drain (step **175**, FIG. **13**(*a*)) and the residual capacity is calculated at steps **451** through **456**. The first step of this routine is to determine the residual battery capacity value. This value, which is dependent upon the current C_rate and the temperature, is accessed at step **451** by the microprocessor from the look-up table depicted in FIG. **22**(*a*). For instance, as shown in FIG. **22**(*a*), at a temperature of −20° C. and a current drain of twice the C_rate, (2C), it has been empirically derived that approximately 92% of the full battery capacity will remain when the end of discharge voltage is reached. When applying a light load (e.g., C/10 discharge rate) at a temperature of about 23° C., virtually no residual capacity will remain when end of discharge voltage is reached.

At step **455**, a determination is made as to whether the C_rate is greater than a high discharge threshold rate (preferably of _ mAh) and whether the End of Discharge flag (see step **262**, FIG. **12**) had been set. If not, then the capacity calculation at steps **440** and **445** is performed as described above. If the current discharge rate is higher than the high discharge threshold rate, then all of the capacity resets are disabled, as indicated at step **456**, and the integration procedure continues at step **440**.

During the operational state of the battery, whether the battery capacity is increasing (CI) or decreasing (CD), the end of charge conditions (EOC) and end of discharge (EOD) conditions, respectively, have to be observed. Therefore, the capacity calculation routine illustrated in FIGS. **13**(*a*) and **13**(*b*) continues by making a determination as to whether the battery is in a capacity increasing or capacity decreasing (resting or discharging) state, as indicated at step **198** in FIG. **13**(*b*). If the capacity is increasing, then the routine for determining whether an End_Condition CI has been met as indicated at step **500**. If the capacity is decreasing, then the routine for determining whether an End_Condition CD has been met as indicated at step **600**.

Observation Routine for Capacity Increasing End Conditions

The microprocessor of the hybrid IC calculates a charge termination by one of three methods: a negative voltage slope greater than 10 mV/cell/min+/−5 m V/cell/min at a full charge voltage; a $^{\Delta T}/_{\Delta t}$ that exceeds 0.9°/min+/−0.2°/min, or a preferred calculated charge of 120% of full charge capacity (but may range from 100% to 150% of CAP_{FC}. The routine for determining if one of the EOC trigger conditions has been met is illustrated in the flow diagrams of FIGS. **14**(*a*)–**14**(*d*).

If it is determined that the capacity is increasing, then the first step **505** of the EOC (CI state) observation process **500** illustrated in FIG. **14**(*a*), is a determination of whether the battery's relative state of charge (soc) value is greater than

20% of the battery's full charge capacity value. If the battery has attained that level of capacity, then the fully discharged status flag is cleared at step **507**. As will be explained below, the fully discharged status flag is set when it is determined that the battery has supplied all the charge it can without being damaged. Until the battery reaches that capacity level, the FULLY_DISCHARGED status flag will remain set. Next, as indicated at step **510**, the first EOC trigger detection method is performed. This first method is a determination as to whether the dT/dt trigger enable condition has been met, and, whether the slope of the temperature increase dT is greater than or equal to a threshold limit indicating an EOC condition. In the preferred embodiment, the dT/dt trigger enable condition is satisfied whenever the relative state of charge (soc) is above a 50% threshold limit, and, an end of charge condition is detected when the slope of the temperature increase becomes greater than a threshold of about 0.9° C./min. It should be mentioned that the slope of the temperature may trigger EOC when it is detected within the range from 0.5° C./min to 12° C./min. If either of these conditions are not satisfied, then a second method of detecting an EOC condition, namely, a detection of whether the slope of the voltage change, dU/dt, becomes negative wherein the value of dU/dt must have a minimum amount and the charging current rate (C_rate) must be greater than a certain value, is performed at step **540** as will be explained in further detail below. If the dT/dt trigger enable condition has been met and the slope of the temperature increase dT is greater than or equal to the EOC threshold limit, then a determination as to whether the EOC flag has been set is made at step **512**. When the EOC flag has not been set, then the number of cells in the battery pack will have to be learned—a process indicated as element **700** in FIG. **14**(*b*) to be described below. Whether or not the number of cells in the battery pack is learned (as will be explained below), at step **700**, then step **570** is performed wherein: a) the EOC status flag is set; b) the remaining capacity is set equal to 95% of the full charge capacity; c) the error registers are cleared; d) the overflow flag for the uncertainty calculation is cleared; and, e) the fully charged status flag is set indicating that the battery has reached a charge termination point. Finally, the algorithm proceeds to step **575**, shown in FIG. **14**(*c*), where the terminate charge alarm flag is set.

If the dT/dt trigger enable condition has been met, the slope of the temperature increase dT is greater than or equal to the EOC threshold limit, and the EOC flag has been set (step **512**), then a determination is made at step **514** as to whether the remaining capacity (Itf) is greater than or equal to the full charge capacity. If this condition is satisfied, then the remaining capacity is set to the full charge capacity as indicated at step **520**. Additionally, at step **520**, the error registers are cleared and the overflow flag for the uncertainty calculation is cleared. If the remaining capacity (Itf) is not greater than or equal to the full charge capacity (step **514**) then the algorithm proceeds to step **575**, shown in FIG. **14**(*c*), where the terminate charge alarm flag is set. In the preferred embodiment, the terminate charge alarm flag must be set when the battery detects EOC on any of the EOC trigger conditions or when an over temperature condition exists, i.e., if T≧AL_HI_TEMP (step **222**, FIG. **12**). As explained above, the terminate charge alarm flag may already be set by the 95% full-trigger, which is initiated when the first temperature slope trigger condition is satisfied at step **510**.

After the remaining capacity is set to the full charge capacity at step **520**, the algorithm proceeds at step **530** to determine whether the battery charger is still on. This is accomplished by checking for a positive charge increase obtained during the charge integration process (see step **435**, FIG. **13**(*c*)). If the charger is still on, then it is known that the charger is continuing to overcharge the battery, and the algorithm must keep track of the amount of battery overcharge. Thus, at step **532** in FIG. **14**(*a*), the total amount of overcharge is calculated by adding the charge increase to the overcharge registers (not shown). It should be mentioned that the overcharge register is never reset, so that the total amount of overcharging since the system start-up is retained. Whether or not the battery charger is still on, the algorithm proceeds to step **535** where the overcharging alarm status flag is set indicating that the battery is being charged beyond an EOC indication. Finally, the algorithm proceeds to step **575**, shown in FIG. **14**(*c*), where the terminate charge alarm flag is set.

As mentioned above with respect to step **510**, if either the dT/dt trigger enable condition has not been met, or, the slope of the temperature increase dT is not greater than or equal to the EOC threshold limit, then a second method of detecting an EOC condition is performed at step **540** shown in FIG. **14**(*c*). At step **540**, a determination is made as to whether: a) the charge is constant current, i.e., whether the difference between the current value and the average current value for one (1) minute is preferably less than 50 milliamps; b) whether the dU/dt voltage change is negative and is greater than a threshold amount of preferably 12 mV/m; and, c) whether the charge current is greater than a predetermined rate, preferably, a rate of C/10. If either of the second method EOC trigger conditions are not satisfied, then a third method of detecting an EOC condition, namely, a detection of whether the relative state of charge (soc) is above 120% and the current rate is between C/50 and C/5 is performed at step **545**. It should be mentioned that the EOC condition may be triggered when the relative state of charge (soc) is detected within the range of 100% to 160%. If all of the second method EOC trigger conditions are satisfied, or, if all of the third method EOC trigger conditions are satisfied, then a determination as to whether the EOC flag has been set, is made at step **550** in FIG. **14**(*c*). If either the second method EOC trigger conditions or third method EOC trigger conditions are satisfied, and the EOC flag has been set (step **550**), then the fully charged status flag is set at step **555** indicating that the battery has reached a charge termination point. Afterwards, the process proceeds at step **520**, FIG. **14**(*a*), by clamping the remaining capacity value to the full charge capacity value as described above. If the EOC flag has not been set, then the number of cells might have to be learned—a process indicated as element **700** to be described below. When the process of learning the amount of cells in the battery is complete, then the EOC status flag will be set at step **551**, and the fully charged status flag is set at step **555** indicating that the battery has reached a charge termination point and the algorithm continues at step **520** described above. If all three EOC trigger conditions are not satisfied, then the EOC detection procedure **500** is exited and the capacity calculation (FIG. **6**(*b*)) continues.

Alternately, a −dU trigger condition will be reached when it is determined that the battery capacity is increasing, dU>DU_MIN, where DU_MIN is a predetermined value equal to the number of battery pack cells multiplied by 10 mV, and the current is determined to be constant and the charge rate is higher than 0.3 C. The charge current is considered constant if $|I-I_{avg}|<50$ mA and $|I-I^{-1}|<50$ mA where I^{-1} was the previous value of the current measurement. The constancy of the battery charging may be calculated in addition to, or, in place of steps **250** et seq. of the

IUT calculation routine FIG. **5**(*b*), where the method of calculating –dU may be accomplished without time dependency.

Learn Number of Cells Routine

As described above, an emergency power-down condition may occur wherein all RAM contents are lost. In such a situation, it may be necessary to relearn the number of cells in the battery pack. Rather than burning in the number of cells for a particular battery module in the ASIC ROM, the number of cells may be learned to enable the ASIC to be configured with other battery packs having a different number of cells. The relearning of the number of cells is indicated by a bit (CALIBRATED bit) in the AL_STATUS register, which will indicate whether the number of battery cells has to be relearned. In the preferred embodiment, it is easily accomplished by utilizing the voltage measured at the battery pack terminals after an EOC condition, described above, is met.

The first step **705** in the learn number of cells procedure **700** shown in FIG. **14**(*d*), is to determine whether the battery pack is uncalibrated, i.e., whether the CALIBRATED bit in the AL_STATUS register indicates that the number of cells should be learned. If so, it is determined at step **710** whether the converted voltage value, U (mV), measured at step **210**, FIG. **5**(*a*) during the IUT calculation procedure, is greater than 11 volts. If so, then it is concluded that the battery pack has nine (9) cells and the number of cells is set at nine in step **720**. If the measured voltage value, U, is not greater than 11 volts, then a determination is made at step **715** as to whether the voltage is greater than 7.5 volts. If so, then it is concluded that the battery pack has six (6) cells and the number of cells is set at six in step **725**. If the measured voltage value, U, is not greater than 7.5 volts, then it is concluded that the battery pack has four (4) cells and the number of cells is set at four in step **730**. After the number of cells is determined, the EOD cutoff voltage, Uempty, is set equal to the number of cells multiplied by the operating battery voltage of 1.02 Volts in the preferred embodiment as indicated at step **740** in FIG. **14**(*d*).

Observation Routine for Capacity Decreasing End Conditions

As previously mentioned, the capacity calculation routine **151** at step **198** makes a determination as to whether the battery is in a capacity increasing or capacity decreasing (resting or discharging) state. If it is determined that the capacity is decreasing, then the first step **605** of the EOD (CD state) observation process **600** illustrated in FIGS. **15**(*a*) and **15**(*b*), is a determination of whether the present voltage measurement (U) is greater than the end of discharge voltage (EDV) and any hysteresis. When the EDV voltage is reached, it is an indication that discharging should be stopped to save the battery from damage. Typically, the EDV is 1.02 V/cell. If the voltage obtained is greater than the EDV voltage, then a flag indicating that the voltage is greater than the EDV voltage plus hysteresis is set at step **610**. If the voltage is not greater than the EDV voltage plus hysteresis, then the flag is cleared at step **612**. Additionally, as indicated at step **613**, since the capacity is decreasing, the Terminate Charge Alarm and Over Charging Alarm flags are cleared.

A determination as to the value of the remaining capacity (Itf) is made at step **615**, where it is determined whether the remaining capacity is less than the calculated error (i.e., the uncertainty capacity). If the remaining capacity is less than the calculated error, then this is an indication that the battery pack has no more capacity and is fully discharged. Consequently, the FULLY_DISCHARGED status flag is set at step **618** and the process continues at step **619**. If there is remaining capacity, then the FULLY_DISCHARGED flag is not set, and the process continues at step **619** where a determination of the relative state of charge is made. If the relative state of charge (soc) has dropped below some hysteresis value, preferably, about 80% of the full charge capacity, then the FULLY_CHARGED status flag is cleared, as indicated at step **620**. Whether the FULLY_CHARGED status flag is cleared or not, the process continues at steps **625** and **630**, where the cycle count number is updated. At step **625**, a determination is made as to whether a cycle count flag is cleared, and, whether the capacity has decreased by 15% of nominal capacity. If these two events of step **625** have occurred, then the cycle count register, containing a value of the number of times the battery has been charged or discharged (not shown), will be incremented at step **630** and the cycle count flag will be set. It should be understood that in the preferred embodiment, the cycle count will be incremented whether or not the battery has been fully or partially charged. Whether the cycle count flag is incremented or not, the process continues at step **640**, where a check is made as to whether the EOD flag is set, and, whether the reset flag is clear. If either the EOD flag is not set, or, the reset flag is not clear, then the end condition observation routine **600** is exited. If the EOD flag is set, and, the reset flag is clear, then a determination is made at step **645** as to whether the EOC (end of charge) flag has been set and whether the error value (uncertainty capacity) is less than 8% of nominal capacity. If these conditions are satisfied then the full charge capacity value is learned at step **650**. Specifically, whenever the battery has performed a full cycle reaching an EOC trigger point and the EOD point and the uncertainty capacity is below 8% of the nominal capacity, the full charge capacity is reset at step **650** with the formula:

$$full_cap = full_cap + full_cap * pd/256 - Itf$$

where "pd" is the predicted residual capacity correction value accessed from the look-up table of FIG. **22**(*a*) and is dependent upon the discharging current rate and temperature. The divisor 256 provides for an integer scaling of pd. The meaning of the formula is to exchange the remaining capacity (Itf) by the residual capacity from the LUT table, which contains fractions of the full charge capacity (Note: the residual capacity obtained is calculated from step **451** of the charge integration process of FIG. **13**(*c*)). If the EOD point is reached with less capacity output as in the former cycle, the amount of Itf (remaining capacity) will be higher at EDV (less discharged capacity compared with the accumulated charged capacity). The full charge capacity will be reduced by the difference of Itf compared with the former cycle so that the ageing of the battery is taken into account by this learning step. If the battery is used in several partial charge/discharge cycles without reaching an EOC or EOD point, the error of the calculation can accumulate to a heavy difference between the real capacity and the calculated remaining capacity (Itf). The algorithm (MaxError( )), to be explained in detail below, calculates the maximum possible error (uncertainty) during its operation as precise as the capacity integration itself on the base of a percentile error for each operating mode. The uncertainty is reset to zero at each EOC and EOD point. An uncertainty of above 8% disables the full capacity reset. Additionally, when the conditions at step **650** are satisfied, the EOC flag is cleared indicating that the full charge capacity has been reset. After the full charge capacity is reset (step **650**), or, if it is determined that the uncertainty error is greater than the prespecified value of 8%, or, the EOC flag is not set, then the algorithm continues at step **655**.

At step **655**, a determination is made as to whether the C_rate at the EDV (end of discharge voltage) trigger is equal to zero, or, whether the present C_rate is less than the C_rate at the EDV trigger, and, whether the capacity reset is not disabled. If either of these conditions are satisfied, the present current at the EOD trigger is set equal to the present C_rate, the delayed capacity reset value is set equal to the present residual capacity value, and, the flags to delay capacity reset after EOD are set at step **660**. Else, if both of the conditions of step **655** are not met, then the end conditions observation routine **600** is exited. As indicated in FIG. **13**(*b*) of the capacity calculation routine **151**, if the EOC and EOD triggering has not occurred, then the capacity calculation is exited.

System Management Bus and Bus Interface

As described above, and as shown in FIGS. **2**(*a*) and **2**(*b*), a modified Phillips I^2C bus interface is used by the battery module **28** to communicate within a configuration comprising the ASIC **32** and the battery **10**, a host computer **16**, and a smart charger **22**. As mentioned previously, requests are either from the host computer to the battery, from the charger to the battery, or, from the battery to either the host or charger. An example of a typical communication between the battery and the charger may be to switch the charger on and off, or, to demand a certain charging rate. The host computer may request information of the battery such as the battery state, or, the battery alarm conditions such as minimal capacity, or, overtemperature. The bus interface control circuit **75** controls all requests and alarm conditions via two serial ports SMBCLK and SMBDATA over the system management bus.

When the battery **10** needs to inform the host of an alarm condition or to inform the battery charger about its desired charging voltage or current, the battery acts as a bus master with write function capabilities. The battery will function to: evaluate the request from the µP **50**; check if the system management bus is free; generates a start bit and sends the address of the battery charger or host; checks whether the ACK-bit has been sent from the charger or host and gives a message to the µP; sends the data supplied from the µP on the bus and checks for ACK bit; generates a stop-bit at the end of the transfer.

When the battery **10** is requested by the host to provide it with information to be explained below, the battery acts as a bus slave with read and write capabilities. For instance, during the steady-state operation, the host might request some information from the battery and will formulate a request. FIG. **16** illustrates the software algorithm compatible with the system management bus interface protocol for providing communication between an external device (host PC or battery charger), and the battery, which acts as a slave thereto.

Specifically, the first step **750** in FIG. **16**, is to decode the command code that has been sent by the external device. Illustrative command codes are discussed hereinbelow, and each typically requires two bytes of data to be transmitted which is indicated as the variable "count". The next step, indicated as step **752**, is to determine whether the command code sent is a valid, recognizable command word. If not, a unsupported command bit is set at step **755** and the transmission will be terminated as indicated at step **758***a* in FIG. **16**. If the command is supported, the battery will perform an internal check to determine if an error has occurred at step **759**. If an internal error is found, then the algorithm will enter a timer loop which will keep checking the internal flag until an error is confirmed or the timer (not shown) times out. This is indicated at step **761**. If a correct value is found at step **759**, then the algorithm will continue at step **764** to determine if the decoded command code calls for a read or write function. If the timer has timed out, or, an error is confirmed at step **761**, then an unknown error flag is set at step **763** and the software transmission is terminated at step **758***b*.

When functioning as a slave, the battery will perform either read or write functions. At step **764**, a determination is made as to whether the command code input (step **750**) is a read or write command. If it is a read command, a determination is made at step **765** as to whether the battery is to perform a calculation as requested by the external device and return a value to be read by the external device. Examples of calculations made by the battery in response to a query (for e.g., AvgTimeToEmpty( )) from a host device are described in greater detail below. The battery µP will proceed to perform the calculations at step **768** and will return a data value to a specified address location as indicated by the read block routine at step **800** and explained in detail below. If it is determined at step **765** that a calculation is not to be performed, (for e.g., only a voltage value is requested) then the algorithm will proceed directly to the read block routine **800** as shown in FIG. **16**.

If, at step **764**, it is determined that a write function is to be performed wherein a data value is to be written to the battery address location from an external device, (for e.g., the AL_REM_TIME threshold value), then a write block authorization check must be performed to determine if the external device may perform the write function. This is indicated at step **771** where a password is checked for validity. If the password checked is not an authorized password, then access will be denied as indicated at step **774**, and the external device will not be able to perform the write function and will terminate the software transmission at step **758***b*. If the external device is authorized to write data to a battery address, then the device will write a data value to pre-specified address locations, as indicated by the write block routine at step **775** to be explained in detail below.

Host to Smart Battery Communication

A host to smart battery communication transfers data from the battery to either a user (of a host PC, for e.g.), or, the power management system of an external device. A user can get either factual data, such as battery characteristic data, (Voltage ( ), Temperature( ), charge/discharge Current ( ), AverageCurrent ( ) etc.), or, predictive (calculated) data such as the battery's remaining life at the present rate of drain, or, how long it will take to charge the battery. It should be mentioned that a real load, e.g., a host PC monitor, has a constant power consumption. When remaining time values described below are calculated (using the assumption that the currents are constant), errors and inaccuracies may occur. Thus, it should be considered to assume a constant power consumption of the load when calculating the remaining time and other variables. Thus, in the following calculations such as RemainingCapacityAlarm ( ), AtRate ( ), RemainingCapacity ( ), FullChargeCapacity ( ), and DesignCapacity ( ) . . . , average power values may be utilized as an alternative to average current values.

The following control commands are representative of battery supplied information when queried by a host device or host PC:

The RemainingCapacity ( ) function returns the battery's remaining capacity and is a numeric indication of remaining charge. Depending upon the capacity mode bit, the RemainingCapacity ( ) function will return a value in mAh or 10 mWh. The value returned is calculated as follows:

$$Itf[mAh] - Itf_err[mAh]$$

where the uncertainty error Itf_err is the subtracted value and the output value is set at 0 if (|Itf|<|Itf_err|).

The RemainingCapacityAlarm ( ) function sets or retrieves the low capacity threshold value AL_REM_CAP (described above) for the low capacity alarm value stored in RAM. When the RemainingCapacity ( ) falls below the AL_REM_CAP value, the battery sends Alarm Warning ( ) messages to the host with the REMAINING_CAPACITY_ALARM bit set. At manufacture, the AL_REM_CAP value is set to 10% of design capacity and will remain unchanged until altered by the RemainingCapacityAlarm ( ) function. This function is used by any host system that desires to know how much power it will require to save its operating state. It enables the host system to more finely control the point at which the host will transfer to a low power mode.

The RemainingTimeAlarm ( ) function sets or retrieves the AL_REM_TIME alarm value. When the estimated remaining time at the present discharge rate as calculated by the AverageTimeToEmpty ( ) function falls below the AL_REM_TIME value, the battery sends Alarm Warning ( ) messages to the host with the REMAINING_TIME_ALARM bit set. An AL_REM_TIME value of zero (0) effectively disables this alarm and the value is initialized to 10 minutes at time of manufacture. The FullChargeCapacity ( ) function returns the predicted or learned battery pack capacity when it is fully charged and is expressed either in current (mAh or 10 mWh) depending upon the setting of the CAPACITY_MODE bit (discussed below). The DesignCapacity ( ) returns the theoretical capacity of a new battery pack which when compared with the value returned by the FullChargeCapacity ( ), will provide an indication of the battery wear. This information is useful by a host device or host PC to adjust its power management policy.

The AtRate ( ) function is the first half of a two-function call-set used to set the AtRate value used in calculations based on capacity made by the AtRateTimeToFull ( ), AtRateTimeToEmpty ( ), and, AtRateOK ( ) functions.

When the AtRate value is positive, the AtRateTimeToFull ( ) function returns the predicted time, preferably in minutes, to fully charge the battery at the AtRate value of charge (value is in mA or 10 mW). The calculation formula is governed by equation:

$$\text{time:} = 60 * \frac{(\text{full cap[mAh]} - Itf\text{[mAh]})}{|\text{AT_RATE}|}$$

where "time" is the returned value in minutes.

The AverageTimeToFull ( ) function returns the predicted remaining time in minutes until the battery is full if a current like the last minute rolling average, I_avg, value is continued. The calculation formula is governed by equation:

$$\text{time:} = 60 * \frac{(\text{full cap[mAh]} - Itf\text{[mAh]})}{I_avg}$$

where "time" is the returned value in minutes.

When the AtRate value is negative, the AtRateTimeToEmpty ( ) function returns the predicted operating time, preferably in minutes, at the AtRate value of battery discharge, until the battery will be exhausted (EDV condition). The calculation formula is governed by equation:

$$\text{time:} = 60 * \frac{(Itf\text{[mAh]} - \text{full_cap[mAh]} * pd_at_rate/256 - Itf\text{err[mAh]})}{|\text{AT_RATE}|}$$

where "time" is the returned value in minutes, |AT_RATE| and pd_at_rate values are calculated by the AtRate ( ) function where pd_at_rate represents the remaining capacity (fraction of full_capacity) and is divided by the value of 256 to scale that value to a fraction. Itf_err is the uncertainty error as explained below.

When the AtRate value is negative, the AtRateOK ( ) function returns a Boolean value that predicts the battery's ability to supply the AtRatevalue of additional discharge energy for 10 seconds, i.e., if the battery can safely supply enough energy for an additional load after the host PC sets the AtRate value.

The RunTimeToEmpty ( ) function returns the predicted remaining battery life at the present rate of discharge (minutes) and is calculated based on either current or power depending upon the setting of the CAPACITY_MODE bit (discussed below). The value returned by this function can used by the host PC or device power management system to get information about the relative gain or loss in remaining battery life in response to a change in power policy. The calculation formula is governed by equation:

$$\text{time:} = 60 * \frac{(Itf\text{[mAh]} - \text{full_cap[mAh]} * pd/256 - Itf\text{err[mAh]})}{|I|\text{[mA]}}$$

where "time" is the returned value in minutes and takes into account the remaining capacity in the battery after EDV which can be get out only by reduction of the load; |I| is the current, pd :=pd(C_rate(|I|, T) and is calculated in the capacity calculation algorithm pd represents the remaining capacity (fraction of full_capacity). This value is divided by 256 to obtain a fraction. Itf_err is the uncertainty error as explained below.

The AverageTimeToEmpty ( ) function returns a one-minute rolling average of the predicted remaining battery life (in minutes) and is calculated based on either current or power. This function provides an averaging of the instantaneous estimations, thereby ensuring a more stable display of state-of-charge information. The calculation formula is governed by equation:

$$\text{time:} = 60 * \frac{(Itf\text{[mAh]} - \text{full_cap[mAh]} * pd_avg/256 - Itf\text{err[mAh]})}{I_avg\text{[mA]}}$$

where "time" is the returned value in minutes, I_avg is updated every 0.5 sec, pd_avg :=pd(C_rate(I_avg), T) and is calculated in the alarm_control routine one cycle before and represents the predicted residual capacity (fraction of full_capacity). This value is divided by 256 to obtain a scale fraction. Itf_err is the uncertainty error as explained below.

FIG. 23 illustrates two voltage versus time graphs, a and b, comparing calculated battery capacity characteristics at various discharging current rates for a six (6) cell battery pack. As shown in FIG. 23, graph a, the voltage will rapidly decrease to an end of discharge condition in a short amount of time when a load amounting to a discharge rate of 2C and yielding approximately 1.554 Ah (amperehours) is applied to the battery. When the load is significantly decreased to a C/5 discharge rate, the battery pack voltage will rise to extend the life of the battery for an amount of time to yield

another 0.816 Ah. Graph b, which is of a different time scale than graph a, shows that discharge at the C_rate will yield approximately 2.307 Ah. When that load is lightened to one half the C_rate, the battery voltage will increase slightly and the battery life can be predicted to extend for an amount of time to yield another 0.078 Ah until end of discharge voltage is reached.

As discussed above, certain calculations are dependent upon the value of the uncertainty capacity, i.e., the maximum possible error obtained during the capacity calculations. The MaxError ( ) function returns the actual uncertainty in the capacity calculation in percentage. A MaxError ( ) output of 20% means that the real value may be between 10% below and 10% above the internally calculated capacity. Most of the calculations in the system management bus interface already subtracts the uncertainty error, so that the error will be –0/+MaxError ( )%. The uncertainty is set to zero on EOC and EOD conditions by the capacity algorithm as explained above. The calculations performed are as follows:

$$Itf_err := \frac{Itf_err_C_D * EPS/256 + Itf_err_S * EPS_S}{256}$$

max_error := 2 * 100 * Itf_err[mAh]/full_cap[mAh]

where Itf_err_C_D is the always positive accumulated charge during the charging and discharging mode; Itf_err_S is the accumulated charge of the self_discharging process. Because of the permanent presence of selfdischarging, even while charging, this accumulation is done all the time using the LUT dependency from relative state of charge (soc) and temperature. Both accumulators are reset to zero at EOC and EOD condition. EPS is the error fraction of the capacity calculation—especially from the LUT and from A/D measurement—while charging or discharging, with the scaling factor 256 applied. EPS_S is the error for selfdischarge-charge integration as fraction. The uncertainty will grow undesirable if the battery will not be fully or discharged over several cycles and the learn mode of the full capacity will be disabled.

The CycleCount ( ) function returns the number of charge/discharge cycles the battery has experienced. The cycles count on each charge decrease with the amount of 15% of the design capacity after the last recharging, which needs not to be a full charging.

Other registers contained in the DBOS memory scheme is the BatteryMode ( ) register which is used to select the battery's various operational modes. For instance, the BatteryMode ( ) register is defined as containing a CAPACITY_MODE bit which is set to specify whether capacity information is to be broadcast in units of mAh or mWh (milliwatthours). This bit allows power management systems to best match their electrical characteristics with those reported by the battery. For example, a switching power supply is best represented by a constant power model, whereas a linear supply is better represented by a constant current model. Additionally, the BatteryMode ( ) register contains a CHARGER_MODE bit which is set to specify whether charging voltage and charging current values are to be broadcast to the smart battery charger **22** (FIG. 1) when the smart battery requires charging. This bit allows a host PC or battery charger to override the smart battery's desired charging parameters by disabling the smart battery's broadcast of the charging current and charging voltage.

Another function calculated on the basis of capacity is the BatteryStatus ( ) function which is used by the power management system of a host device or PC to get alarm and status bits, as well as error codes from the battery status register. This function returns the battery's status word flags including alarm warning bits such as OVER_CHARGED_ALARM, TERMINATE_CHARGE_ALARM, DTEMP_ALARM, OVER_TEMP_ALARM, TERMINATE_DISCHARGE_ALARM, REMAINING_CAPACITY_ALARM, and, REMAINING_TIME_ALARM and status bits including INITIALIZED, DISCHARGING, FULLY_CHARGED, and, FULLY_DISCHARGED.

Ancillary functions that the battery **10** is capable of performing include: the SpecificationInfo ( ) for providing the version number of the smart battery specification the battery pack supports; the ManufactureDate ( ) for providing a system with information that can be used to uniquely identify a particular battery; the Serial Number ( ), which provides information for identifying a particular battery; the ManufacturerName ( ) function returns the name of the smart battery's manufacturer; the DeviceName ( ) function returns a character string that contains the battery's name; the DeviceChemistry ( ) returns a character string that contains the battery's chemistry; the ManufacturerData ( ) function which allows access to the manufacturer data (e.g., lot codes, number of deep cycles, discharge patterns, deepest discharge, etc., contained in the battery.

Write Block Routine

As mentioned above, the battery may receive data from an external device to be used in a control command calculation, or, as an alarm threshold value. The write block **775** illustrated in FIG. **17**, controls this transfer of data to the battery. First, at step **776**, a determination is made as to whether the data value to be read from the external host device is greater than two bytes long. In the preferred embodiment, most control commands will write a data value to the battery that is two bytes long. If the data is longer than two bytes, i.e., if count >2, then the variable "w" is set equal to the number of address locations allocated for and corresponding to length of data in number of bytes at step **778**. Then, at step **780**, a determination is made as to whether the previously determined count value has been set equal to the address locations allocated. If this is not the case, then an error flag is set at step **790** indicating that an inordinate amount of data is to be sent, or, that there is not enough locations allocated for receiving the data. If the previously determined count value "count" has been set equal to the number of address locations allocated, then the program enters a loop indicated as steps **781**, **783** and **785** wherein each byte of data is sequentially written to the I^2C bus to the battery address location [Adr] (step **783**). After each byte is sent, the count of the number of bytes is decremented and the address location for the next sequential data byte to be written is incremented. Until count=0, indicating that the last byte of data has been transmitted to the battery as shown at step **785**, the loop will continue and enter at step **781** to determine if the battery has read each data byte (RDVAL=1) sent by the external device and indicating that the data byte has been successfully transmitted. If the read acknowledge flag has been received after each byte transfer, the loop continues at step **783** until the last data byte is sent. If the read acknowledge flag has not been received, then an error may have occurred and the program proceeds to step **782** where a determination is made as to whether a bus error or timeout has occurred. If none of these instances has occurred, then the program will proceed to step **787** to determine if the bus master has terminated the transmission. If the bus master has terminated the transmission, then an error flag is set at step **790** indicating that an inordinate amount of data is being transmitted and the transmission will be terminated at step **795**. If the bus master has not terminated the transmission, then the system will continue to look for the RDVAL flag

until an internal handshake timer (not shown) times out (step **782**) and an unknown error flag is set and the transmission will be terminated, as shown at steps **792** and **795**. In view of FIG. **17**, it is understood that in some cases, a fixed two-byte data word is to be read, as indicated at step **776**, and the algorithm will proceed directly to step **783** where the first data byte is read by the battery at the first battery address location.

After the last data byte has been received, as indicated at step **786**, a determination is made as to whether the stop bit flag has been received from the modified I^2C bus master indicating the end of bus control due to the fact that the external device will not be sending any more data. If the stop bit is received the write block routine is exited. If the stop bit has not been received, then an error may have occurred and the program proceeds to step **788** where a determination is made as to whether a bus error or timeout has occurred. If an error or timeout has occurred, then the program will proceed to set an unknown error flag and the transmission will be terminated, as shown at steps **792** and **795**. If none of these instances has occurred, then the program will proceed to step **789** to determine if the RDVAL flag has been set to indicate if the last data byte has been successfully read. If it has been successfully read, then this is an indication that the external device has not finished sending data or that not enough address locations have been allocated and an error flag will be set as shown at step **790** and the transmission will be terminated at step **795**. If the last data value has been successfully read at step **789**, then the process will continue to look for the modified I^2C bus master stop bit at step **786** until either an internal handshake timer (not shown) times out or an error occurs (step **788**).

Read Block Routine

As mentioned above, the battery will return a calculated or measurement data value to a specified address location as indicated by the read block routine **800** as illustrated in FIG. **18**. At step **802**, a determination is first made as to whether the data value to be written to the host device is greater than two bytes long. If the data is longer than two bytes, i.e., if count >2, then the address is pointed to at step **805** and the program enters a loop indicated as steps **808**, **812**, and **815** wherein each byte of data is sequentially written to the SMBus bus to an address location of the requesting host device as indicated at step **812**. After each byte is sent, the count of the number of bytes is decremented and the address location for the next byte to be written is incremented. Until count=0, indicating that the last byte of data has been transmitted to the external device as shown at step **815**, the loop will continue and enter at step **808** to determine if the acknowledge bit has been sent by the external device indicating that the current data byte has been successfully transmitted. If the acknowledge bit has been received after each byte transfer, the loop continues at step **812** until the last data byte is sent. If the acknowledge bit has not been received, then an error may have occurred and the program proceeds to step **821** where a determination is made as to whether a bus error, termination, or timeout has occurred. If none of these instances has occurred, then the program will proceed to step **808** to again determine if the data byte acknowledge bit has been received. This process will continue until an internal handshake timer (not shown) times out wherein the process will continue at step **825** where an unknown error flag is set and the transmission will be terminated. After it is determined that the last data byte has been sent (step **818**) then a flag indicating that the last byte has been sent is set at step **818** of FIG. **18**. In view of FIG. **18**, it is understood that in some cases, no data is to be returned as shown at step **802**, and the algorithm will proceed directly to step **812** and bypass the receipt acknowledgment bit step **808**.

Next, as indicated at step **822**, a determination is made as to whether the stop bit flag has been received from the I^2C bus master indicating the end of bus control due to the fact that the external device will not be receiving any more data. If the stop bit is received the read block is exited. If the stop bit has not been received, then an error may have occurred and the program proceeds to step **824** where a determination is made as to whether a bus error or timeout has occurred. If none of these instances has occurred, then the program will proceed to step **822** to again determine if the stop bit has been received. This process will continue until an internal handshake timer (not shown) times out wherein the process will continue at step **825** where an unknown error flag is set and the transmission will be terminated.

Alarm Control

All of the alarm status flags heretofore mentioned indicate that the battery has reached a certain state of charge (fully charged, empty discharged) or a critical state (maximal temperature, being overcharged). These events are encoded in the Al_Status battery register and the warning message AlarmWarning ( ) is sent the by the battery to an external device when the battery detects an alarm condition. In this event, the battery becomes the bus master and alternately notifies the host computer or battery charger of any critical and/or alarm conditions at a rate of preferably once every five seconds, until the critical state is corrected. The alarm condition may be broadcast to the host computer for 10 seconds if the alarm condition is such that the battery charger does not need to be notified of an alarm condition, for e.g., REMAINING_CAP_ALARM warning message is not the broadcast to the charger device. If alarm conditions such as OVER_CHARGED_ALARM, TERMINATE_CHARGE_ALARM, DTEMP_ALARM, OVER_TEMP_ALARM, and TERMINATE_DISCHARGE_ALARM exist, then the alarm is broadcast, alternating between the charger device and the host device, in five (5) second intervals.

The modified SMBus protocol for communicating alarm or warning messages are illustrated in the alarm control routine **152** as shown in detail in FIG. **19**. This routine runs through all possible alarm conditions for possible broadcast to a host device after a capacity calculation is performed as shown in FIG. **3**.

The first step, indicated as step **901** in FIG. **19** is to verify the status of the remaining capacity. Specifically, a determination is made as to whether the AL_REM_CAP run value is greater than 0 and that the remaining capacity (less the uncertainty error) is less than the AL_REM_CAP value. If these conditions hold true, the REMAINING_CAPACITY_ALARM bit is set at step **904**. If none of these conditions holds true, the REMAINING_CAPACITY_ALARM bit is cleared at step **906**. Next, the C_rate based on the one minute rolling average current is calculated and the residual capacity based on the C_rate [pd_avg:=pd(C_rate(I_avg), T)] is accessed from the look-up table of FIG. **22**(*a*). Then, at step **910**, a determination is made as to whether the battery state is capacity decreasing. If the battery capacity is decreasing, then a determination is made at step **913** as to whether the AL_REM_TIME alarm threshold value is greater than zero (0). If so, then the estimated remaining time at the present discharge rate is calculated at step **915** by the AverageTimeToEmpty ( ) command code. When the calculated remaining time falls below the AL_REM_TIME threshold value, as determined

at step **917**, the program sets the REMAINING_TIME_ALARM bit as indicated at step **919** and the program proceed at step **925** shown in FIG. **19**. If, it is determined either that the battery state is not capacity decreasing (step **910**), or, that the AL_REM_TIME is equal to zero (step **913**), or, that the calculated remaining time falls below the AL_REM_TIME threshold value (step **917**), then the program clears the REMAINING_TIME_ALARM bit as indicated at step **921** and the program proceed at step **925** shown in FIG. **19**.

As shown at step **925**, the upper byte of the Alarm status register is checked to determine if any alarm bits, e.g., alarm bits such as OVER_CHARGED_ALARM, TERMINATE_CHARGE_ALARM, DTEMP_ALARM, OVER_TEMP_ALARM, TERMINATE_DISCHARGE_ALARM, REMAINING_CAPACITY_ALARM, and, REMAINING_TIME_ALARM have been set. If so, then a check of the alarm broadcast flag "alarming" is made at step **927**. If the upper byte of the Alarm status register indicates no alarm condition, i.e., no bits set, then the process will continue at step **926** and the alarming broadcast flag is cleared. Note, that upon initialization, the alarming broadcast flag is not set. However, as long as an alarm condition exists, this flag will be set. Therefore, as shown at step **927**, if the alarming flag is cleared, the process continues and the alarming flag is set at step **930**. Additionally, at step **930**, the alarm broadcast timer is set to zero, and, the "alarm to host" flag is set indicating that the alarm will be sent to a host external device and not a battery charger. The process continues at step **933**, where a determination is made as to whether the alarm broadcast timer has timed out (=0). Since the broadcast timer has been set to zero at step **930** for this first operating cycle of the alarm condition, or, if the alarm broadcast timer has timed out, then the process will continue at step **935**. If the timer has not timed out, then the alarm control process is exited. At step **935**, the address location for the alarm broadcast is set to the host device, and the command code is set equal to the battery status [BatteryStatus ( )] function described above. This will initiate the transfer of the particular alarm to the host device. A determination is then made at step **937** as to whether the alarm to host flag is cleared (=0). During the first operating cycle of the alarm condition (step **930**), the alarm to host flag had been set (=1) so the algorithm skips over steps **940** and **943** (discussed below) and performs the send message routine **945** which changes the function of the battery as having bus master control so that the alarm message can be sent. Details of the send message routine **945** will be explained in detail below. Afterwards, at step **947**, the broadcast alarm timer is reset to its 10 second time (N_ALARM) and the alarm sent to host flag is toggled to the alarm sent to charger flag.

After the message is initiated to broadcast an alarm warning message to the host device at step **945** (by the send message routine), and, the alarm broadcast timer has been reset, then the process continues. After the next capacity calculation (FIG. **3**), if the alarm condition still exists (i.e., the alarm bits are set) at step **925**, the process is continued. However, for the next and subsequent operating cycles of the alarm condition, the alarming flag has already been set as determined (at step **927**), so the alarm broadcast timer (initialized as 10 seconds) is decremented at step **931** until the timer has timed out or the alarm status has been changed. Thus, after the broadcast timer has decremented, the process continues at step **933**, where a determination is made as to whether the alarm broadcast timer has timed out (=0). If the broadcast timer has not timed out, then the alarm control routine is exited and these set of steps will continue until the alarm broadcast timer has timed out (step **933**). Until the alarm message has been broadcast to the host device for preferably five (5) seconds, then steps **935** and **937** will not be performed. When the broadcast timer has timed out, and, since the alarm to host flag has toggled (during the first operating cycle of the alarm condition), the condition at step **937** will be true. Therefore, the address location for the alarm broadcast is changed and set to the battery charger at step **940**, and the program will proceed to step **943** where a determination is made as to whether the particular alarm warning message is meant to be sent to the battery charger for the next 10 seconds. If, the alarm condition is not meant to be transmitted to the battery charger, then the send message routine (step **945**) will be bypassed, and the broadcast timer will be reset at step **947** and the alarm to host bit toggled so that the message will be retransmitted to the host device.

Charger Control

Whenever the BatteryMode ( ) CHARGER MODE bit is set to zero, and the battery detects the presence of a smart battery charger, the battery is able to communicate with the smart battery charger and will send ChargingCurrent ( ) and ChargingVoltage ( ) values to the smart battery charger. The ChargingCurrent ( ) function sets the maximum current that a smart battery charger may deliver to the battery and will return the desired charging rate in mA. This allows the battery charger to dynamically adjust its output current to match optimal recharging requirements. A maximum value of 0×FFFF means constant voltage charging with the output value of ChargingVoltage ( ). Results are broadcast with the battery as active bus master under the conditions set forth in the charger control routine **154** of FIGS. **3** and **20**.

The first step **850** in FIG. **20** is to determine whether the battery is in the system. If not, CAPACITY_MODE and CHARGER_MODE variables are cleared at step **853** and the routine is exited. If the battery is installed in the system, a determination is made at step **855** as to whether the battery was just inserted in the system. If the battery was just inserted, then the message timer is set to one (1), and the CAPACITY_MODE and CHARGER_MODE variables are cleared at step **857** and the algorithm continues at step **859**. If the battery has not just been inserted (step **855**), then the algorithm skips to step **859** where a determination is made as to the state of the charger mode bit. If the bit is not cleared at step **859**, then the routine is exited. If the CHARGER_MODE bit is set at step **859** then the timer is decremented at step **861**. The next step at **863** is to determine whether the message timer has timed out. If it has, then the message timer is reset at step **865** and the charging current calculation is additionally made. If the message timer has not timed out at step **863**, then the routine is exited. The next step **866** is to determine whether the returned value of the calculated charging current is zero. If the charging current value returned is zero, then the process proceeds at step **868**. If the charging current is not zero, then the determination is made at step **867** as to whether the state is capacity increasing (CI). If the battery is in a CI state, then the process proceeds at step **868**. If the capacity is decreasing, then the routine is exited.

At step **868**, the address location for the charger broadcast is set to the battery charger, and the command code is set equal to the command code ChargingCurrent ( ). Next, at step **870**, the charging current command message is sent to the battery charger by the send message routine (discussed below). Then, at step **872**, the maximum value (hex FFFF) fed into the ConstantVoltage ( ) function which indicates that

the charger will be a constant current charging device. This instruction is broadcast to the charger via the send message routine at step **874**. After the charging current is broadcast, the routine is finally exited.

Send Message Routine

As indicated at step **945** in FIG. **19** and step **870** in FIG. **20**, the send message routine changes the function of the battery to have bus master control so that the alarm messages can be sent. FIG. **21** illustrates the send message routine.

The first step **950** is to determine the data bus availability. If it is determined that the data bus is available, then the first piece of data to be sent is the slave address, i.e., the address of the external host device or battery charger, as indicated at step **952**. As soon as the data bus is acquired, then two flags are set; the first flag is an internally generated flag that is set to indicate that the battery now has bus master control (step **953**), and, the second flag is the transmission termination flag that is cleared at step **954**. The next step, as indicated at step **955**, is a check as to whether the acknowledge bit has been sent, i.e., whether the first byte of data (slave address) has been received by the slave device. If the acknowledge bit has not been sent, then a check is made at step **958** to determine if the bus is busy. If the bus is now busy, then the program continues at step **960** of FIG. **21**. If the bus is not busy at step **958**, then a determination is made as to whether a bus error or timeout flag has been generated at step **959**. If an error or timeout has occurred, then the program will proceed to step **973** where the transmission will be terminated and the routine exited. If an error or timeout condition does not exist, the routine will continue at step **955** until an acknowledge bit has been sent by the slave indicating that the data has been received. If the acknowledge bit has been received, then the current command code is transmitted at step **957**. It should be understood that when the send message routine is invoked during a critical alarm condition, then the command code word is set to the battery address (see step **935**, FIG. **19**) and the slave will recognize that only two bytes of data are to be sent. The next step, as indicated at step **960**, is a check as to whether the acknowledge bit has been sent, i.e., whether the command code (or battery address) has been received by the slave device. If the acknowledge bit has not been received, then a check is made at step **962** to determine whether a bus error or timeout flag has been generated. If an error or timeout has occurred, then the program will proceed to step **973** where the transmission will be terminated and the routine exited. If an error or timeout condition does not exist, the routine will continue at step **960** until it is acknowledged that the command code (or battery address) has been received. If the acknowledge bit has been received, then the first byte of data is transmitted to the specified address location (see step **935**, FIG. **19**) at step **965**. The next step, as indicated at step **966**, is a check as to whether the acknowledge bit has been sent, i.e., whether the first byte of command code data has been received by the slave device. If the acknowledge bit has not been received, then a check is made at step **967** to determine whether a bus error or timeout flag has been generated. If an error or timeout has occurred, then the program will proceed to step **973** where the transmission will be terminated and the routine exited. If an error or timeout condition does not exist, the routine will continue at step **966** until it is acknowledged that the first data byte has been received. If the acknowledge bit has been received, then the second byte of data is transmitted to the next address location at step **968**. The next step, as indicated at step **969**, is a check as to whether the acknowledge bit has been sent, i.e., whether the second byte of command code data has been received by the slave device. If the acknowledge bit has not been received, then a check is made at step **971** to determine whether a bus error or timeout flag has been generated. If an error or timeout has occurred, then the program will proceed to step **973** where the transmission will be terminated and the routine exited. If an error or timeout condition does not exist, the routine will continue at step **969** until it is acknowledged that the second data byte has been received. After the full message has been transmitted by the battery to the slave device, the send message routine is exited.

LED Display

As shown in FIG. **2**(*a*), the battery **10** of the instant invention provides manually controlled four (4) segment light emitting diode (LED) display indicating the relative state of charge of the battery (similar to a fuel gauge) with respect to the full_cap value. After the capacity calculation, alarm control **152**, and charger control **154** routines are performed during each 500 msec period (operating cycle), the system will look for a hardware trigger of the LED display. At any time, a user can initiate the LED display by a switch **35** on the battery **10** as shown in FIG. **2**(*a*). The control logic for generating the LED display is described in detail (in view of steps **975** through **996** of FIG. **15**) in copending patent application (U.S. Ser. No. 08/318,004).

While the invention has been particularly shown and described with respect to the preferred embodiments thereof, it will be understood by those skilled in the art that the foregoing and other changes in form and details may be made therein without departing from the spirit and scope of the invention, which should be limited only by the scope of the appended claims.

We claim:

1. A smart battery which provides electrical power and which reports predefined battery parameters to an external device having a power management system, said smart battery comprising:

(a) at least one rechargeable cell connected to a pair of terminals to provide electrical power to an external device during a discharge mode and to receive electrical power during a charge mode, as provided or determined by said remote device,

(b) a data bus for reporting predefined battery identification and charge parameters to the external device,

(c) an analog means for generating analog signals representative of battery voltage and current at said terminals, and an analog signal representative of battery temperature at said cell,

(d) a hybrid integrated circuit (Ic) having a microprocessor for receiving the analog signals and converting them to digital signals representative of battery voltage, current and temperature, and calculating actual charge parameters over time from said digital signals, said calculations including a capacity reset and an error calculation which is incremented after each partial charge and extinguished at each capacity reset;

(e) a data memory defined within said hybrid IC for storing said predefined battery identification and actual charge parameters, even when nominally fully discharged, said charge parameters including a cumulative error value,

(f) a bus controller defined within said hybrid IC for sending battery messages to said remote device over said data bus, said messages including said predefined battery identification and said actual charge parameters.

2. A battery pack comprising:

terminal means for connecting the battery pack to a battery powered device and to a battery recharger;

a battery including at least one rechargeable battery cell connected to the terminal means, said battery having

i) discharging periods for supplying electrical power to the battery powered device, and

ii) charging periods for receiving electrical power from the terminal means;

means to sense and to generate signals representing battery voltage, battery temperature or battery current;

a processor for receiving the signals representing battery voltage, battery temperature or battery current, and for performing a predefined series of calculations using said signals, wherein said predefined calculations include calculating an actual full capacity of the battery at the ends of at least selected ones of the discharging periods; and

a memory area for storing data values including at least values representing battery voltage, battery temperature and battery current.

3. A battery pack according to claim **2**, wherein:

the processor maintains

i) an uncertainty value representing an uncertainty in the full capacity of the battery, and

ii) a nominal full capacity value representing a nominal full capacity of the battery;

after each end of the selected ones of the discharging periods, if the uncertainty value is less than a given percentage of the nominal full capacity value, then the processor calculates the actual full capacity of the battery.

4. A battery pack according to claim **2**, wherein:

the processor includes means to determine a correction value; and

at the end of a given discharging period, when the processor calculates a new value for the actual full capacity value of the battery, the processor calculates said new value according to the equation

$$nCAP_{FC}=oCAP_{FC}+(oCAP_{FC})x-CAP_{REM}$$

where:

$nCAP_{FC}$ is the new value for the actual full capacity of the battery,

$oCAP_{FC}$ is the most recently previously calculated value for the actual full capacity of the battery, x is the correction value determined by the processor, and

CAP_{REM} is the capacity of the battery at the end of the given charge-discharge cycle.

5. A battery pack according to claim **4**, wherein the means to determine the correction value includes means to determine the correction value based on battery temperature and battery current.

6. A battery pack according to claim **5**, wherein the means to determine the correction value includes:

a look-up table having a multitude of stored values; and

means to select one of said stored values based on the battery temperature and battery current.

7. A battery pack according to claim **3**, wherein the predefined calculations further include calculating the uncertainty value at predetermined times.

8. A battery pack according to claim **7**, wherein the uncertainty value is reset to zero at given times.

9. A battery pack according to claim **8**, wherein:

the processor includes means to detect a plurality of predefined end of charge conditions during the charging periods, and to terminate each of the charging periods when one of said end of charge conditions is detected during said each of the changing periods; and

the processor resets the uncertainty value to zero when one of said end of charge conditions is detected.

10. A battery pack according to claim **8**, wherein:

the processor includes means to detect a plurality of predefined end of discharge conditions during the discharging periods, and to terminate each of the discharging periods when one of said end of discharge conditions is detected during said each of the discharging periods; and

the processor resets the uncertainty value to zero when one of said end of discharge conditions is detected.

11. A battery pack according to claim **8**, wherein:

the processor includes means to determine the accumulated amount of current conducted to the battery during each of the charging periods; and

when the uncertainty value is calculated during one of the charging periods, the calculated uncertainty value is based on the accumulated amount of current conducted to the battery during said one of the charging periods.

12. A battery according to claim **8**, wherein:

the processor includes means to determine the accumulated amount of current discharged from the battery during each of the discharging periods; and

when the uncertainty value is calculated during one of the discharging periods, the calculated uncertainty value is based on the accumulated amount of current discharged from the battery during the said one of the discharging periods.

13. A method of operating a battery system having a rechargeable battery connected to a battery powered device, a processor and a memory area, the method comprising:

discharging the battery during discharging periods to power the battery powered device;

charging the battery during charging periods;

sensing, and generating signals representing, battery voltage, battery temperature and battery current;

storing data values in the memory area, said stored data values including at least values representing battery voltage, battery temperature and battery current; and

the processor performing predefined calculations using the signals representing battery voltage, battery temperature and battery current, including the step of calculating actual full capacity of the battery at the ends of at least selected ones of the discharging periods.

14. A method according to claim **13**, wherein:

the step of performing predefined calculations further includes the steps of the processor

i) maintaining an uncertainty value representing an uncertainty in the full capacity of the battery, and

ii) maintaining a nominal full capacity value representing a nominal full capacity of the battery; and

the step of calculating the actual full capacity of the battery includes the step of, after each end of the selected ones of the discharging periods, calculating the actual full capacity of the battery if the uncertainty value is less than a given percentage of the nominal full capacity value.

15. A method according to claim **13**, wherein:

the step of performing predefined calculations further includes the step of determining a correction value; and

the step of calculating the actual full capacity of the battery includes the step of

calculating a new value for the actual full capacity of the battery according to the equation

$$nCAP_{FC}=oCAP_{FC}+(oCAP_{FC})x-CAP_{REM}$$

where

$nCAP_{FC}$ is the new value for the actual full capacity of the battery,

$oCAP_{FC}$ is the most recently previously calculated value for the actual full capacity of the battery,

x is the determined correction value, and

CAP_{REM} is the capacity of the battery at the time said new value is calculated.

16. A method according to claim **15**, wherein the step of determining the correction value includes the step of determining the correction value based on battery temperature and battery current.

17. A method according to claim **16**, wherein the memory area includes a look-up table having a multitude of stored values, and wherein the step of determining the correction value includes the step of selecting one of the values from the look-up table on the basis of the battery temperature and the battery current.

18. A method according to claim **15**, wherein the step of determining the uncertainty value includes the step of calculating the uncertainty value at predefined times.

19. A method according to claim **18**, wherein the step of determining the uncertainty value further includes the step of resetting the uncertainty value to zero at given times.

20. A method according to claim **19**, wherein:

the method further includes the step of,

during each of the discharging periods, the processor detecting one of a plurality of predefined end of discharge conditions, and terminating the discharging period when said one of said end of discharge conditions is detected; and

the step of resetting the uncertainty value to zero includes the step of resetting the uncertainty value to zero when one of said end of discharge conditions is detected.

21. A method according to claim **19**, wherein:

the step of calculating the uncertainty value includes the steps of

i) determining the accumulated amount of charge conducted to the battery during each of the charging periods, and

ii) when the uncertainty value is calculated during the charging period, calculating said uncertainty value on the basis of the accumulated amount of charge conducted to the battery during said charging period.

22. A method according to claim **19**, wherein:

the step of calculating the uncertainty value includes the steps of

i) determining the accumulated amount of charge discharged from the battery during each of the discharging periods, and

ii) when the uncertainty value is calculated during one of the discharging periods, calculating said uncertainty value on the basis of the accumulated amount of charge discharged from the battery during said one of the discharging periods.

23. A battery pack comprising:

terminal means for connecting the battery pack to a battery powered device and to a battery recharger;

a battery including at least one rechargeable battery cell connected to the terminal means, said battery having

i) a discharge mode for supplying electrical power to the battery powered device, and

ii) a charge mode for receiving electrical power from the terminal means;

means to sense and to generate signals representing battery voltage, battery temperature, and battery current;

a memory area for storing data values including at least values representing battery voltage, battery temperature and battery current; and

a processor for receiving the signals representing battery voltage, battery temperature and battery current, and for performing predefined calculations using said signals, the processor including

i) means to calculate an uncertainty value, and

ii) means to calculate one of said stored data values at defined times if the uncertainty value is below a given level.

24. A battery pack according to claim **23**, wherein the means to calculate one of said stored data values calculates said one of said stored data values at each of said defined times if and only if at said each of said defined times the uncertainty value is below the given level.

25. A battery pack according to claim **24**, wherein the means to calculate the uncertainty value resets the uncertainty value to zero at predetermined times.

26. A battery pack according to claim **25**, wherein the processor includes means to determine when said predetermined times occur.

27. A battery pack according to claim **25**, wherein:

the battery has charge-discharge cycles, each of said cycles having a discharging portion and a charging portion;

the processor further includes means to detect a plurality of predefined end of discharge conditions during the discharging portion of each charge-discharge cycle, and to terminate the discharging portion of the charge-discharge cycle when one of said end of discharge condition is detected; and

the processor resets the uncertainty values to zero when one of said end of discharge condition is detected.

28. A method of operating a battery system having a rechargeable battery connected to a battery powered device, a processor and a memory area, the method comprising:

sensing, and generating signals representing, battery voltage, battery temperature and battery current;

storing data values in the memory area, said stored data values including at least values representing battery voltage, battery temperature and battery current; and

the processor performing predefined calculations using the signals representing battery voltage, battery temperature and battery current, including the steps of

i) calculating an uncertainty value, and

ii) calculating one of said stored data values at defined times if the uncertainty value is below a given level.

29. A method according to claim **28**, wherein the step of calculating one of said stored data values includes the step of calculating said one of said stored data values at each of said defined times if and only if at said each of said defined times the uncertainty value is below the given level.

30. A method according to claim 28, wherein:

the battery has charge-discharge cycles, each of said cycles having a discharging portion and a charging portion;

in the discharging portion of each of said cycles, current is discharged from the battery;

in the charging portion of each of said cycles, current is conducted to the battery; and

the step of calculating the uncertainty value includes the steps of

i) in the discharging portion of each of said cycles, calculating an uncertainty in the accumulated amount of current conducted from the battery during the discharging portion of the cycle, and

ii) in the charging portion of each of said cycles, calculating an uncertainty in the accumulated amount of current discharged from the battery during the discharging portion of the cycle.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE

CERTIFICATE OF CORRECTION

PATENT NO. : **5,691,621**

DATED : **November 25, 1997**

INVENTOR(S) : **Duong Van Phuoc**

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Column 1, line 23: "device" should read --devices--

Column 6, line 58: "2(c)" should read –22(c)–

Column 8, line 67: after "which" insert --includes--

Column 12, line 1: "R_{REF} " should read –V_{REF}

Column 12, line 7: "S1" should read --SI--

Column 14, line 15: "2(a)" should read --2(a)) --

Signed and Sealed this

Fourth Day of May, 1999

Attest:

Attesting Officer

Q. TODD DICKINSON

Acting Commissioner of Patents and Trademarks