US009771692B2

(12) **United States Patent**
Sawyer et al.

(10) **Patent No.: US 9,771,692 B2**
(45) **Date of Patent: *Sep. 26, 2017**

(54) **BASE FOR TURF SYSTEM**

(71) Applicant: **Brock USA, LLC**, Boulder, CO (US)

(72) Inventors: **Steven Lee Sawyer**, Huntington Beach, CA (US); **Daniel C. Sawyer**, Boulder, CO (US); **Richard R. Runkles**, Windsor, CO (US)

(73) Assignee: **Brock USA, LLC**, Boulder, CO (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

This patent is subject to a terminal disclaimer.

(21) Appl. No.: **15/336,270**

(22) Filed: **Oct. 27, 2016**

(65) **Prior Publication Data**

US 2017/0044724 A1 Feb. 16, 2017

Related U.S. Application Data

(63) Continuation of application No. 13/711,689, filed on Dec. 12, 2012, which is a continuation of application
(Continued)

(51) **Int. Cl.**
E01C 13/02 (2006.01)
E01C 13/08 (2006.01)

(52) **U.S. Cl.**
CPC ***E01C 13/02*** (2013.01); ***E01C 13/08*** (2013.01); *Y10T 428/16* (2015.01); *Y10T 428/169* (2015.01); *Y10T 428/17* (2015.01); *Y10T 428/192* (2015.01); *Y10T 428/23979* (2015.04); *Y10T 428/24273* (2015.01); *Y10T 428/24355* (2015.01); *Y10T 428/24479* (2015.01); *Y10T 428/249953* (2015.04)

(58) **Field of Classification Search**
CPC .. E01C 13/08; E01C 13/02; Y10T 428/23979; Y10T 428/24479; Y10T 428/24273; Y10T 428/249953
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,515,847 A 7/1950 Winkler
2,746,365 A 5/1956 Darneille
(Continued)

FOREIGN PATENT DOCUMENTS

CH 577328 A5 7/1976
CH 671787 A5 9/1989
(Continued)

OTHER PUBLICATIONS

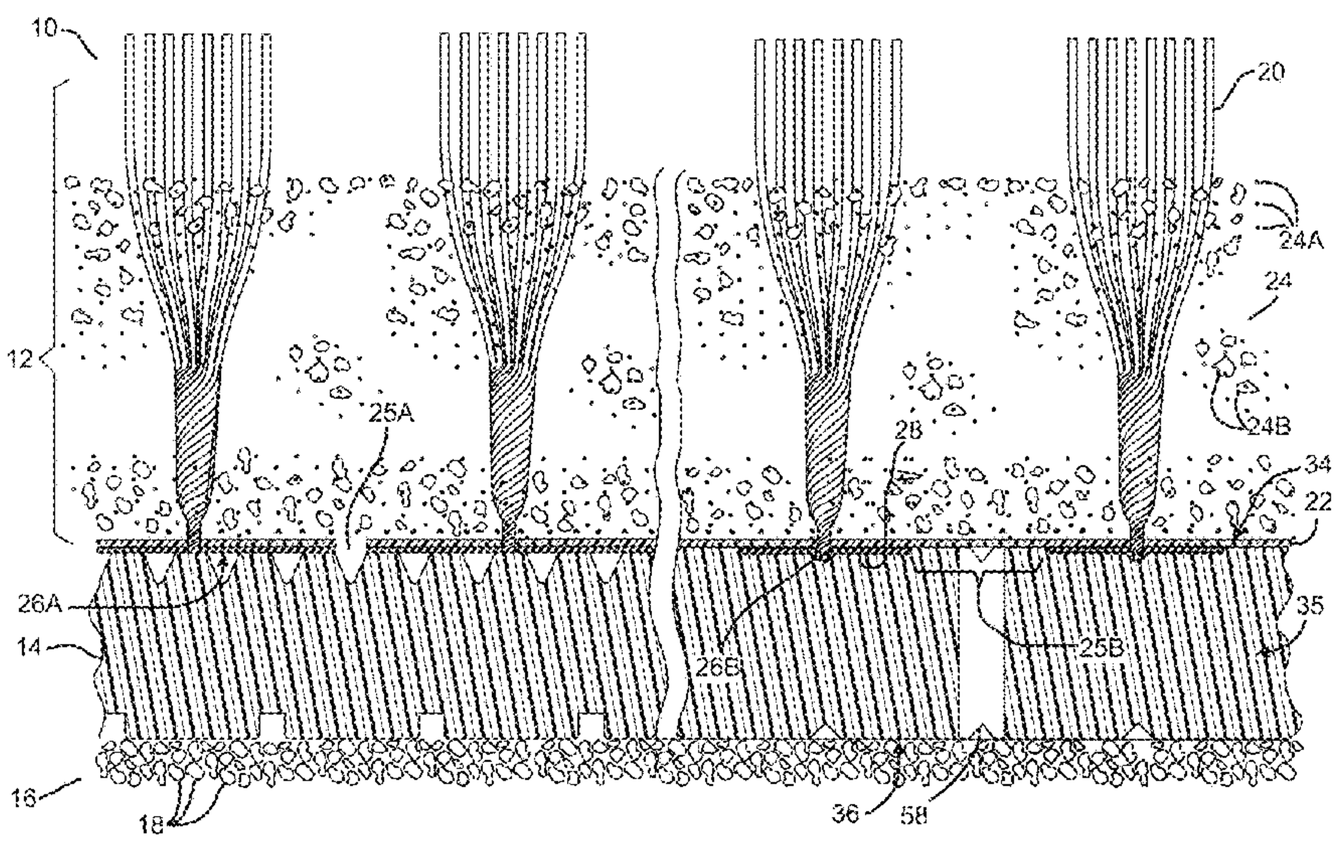
Aero-Spacer Dri-Lex, Hydrofil, FaytexCorp.
(Continued)

Primary Examiner — Cheryl Juska
(74) *Attorney, Agent, or Firm* — MacMillan, Sobanski & Todd, LLC

(57) **ABSTRACT**

An underlayment layer is configured to support an artificial turf assembly. The underlayment layer comprises a core with a top side and a bottom side. The top side has a plurality of spaced apart, upwardly oriented projections that define channels suitable for fluid flow along the top side of the core when the underlayment layer is positioned beneath an overlying artificial turf assembly.

12 Claims, 15 Drawing Sheets



Related U.S. Application Data

No. 13/568,611, filed on Aug. 7, 2012, now Pat. No. 8,568,840, which is a continuation of application No. 12/009,835, filed on Jan. 22, 2008, now Pat. No. 8,236,392.

(60) Provisional application No. 60/881,293, filed on Jan. 19, 2007, provisional application No. 60/927,975, filed on May 7, 2007, provisional application No. 61/000,503, filed on Oct. 26, 2007, provisional application No. 61/003,731, filed on Nov. 20, 2007.

(56) **References Cited**

U.S. PATENT DOCUMENTS

3,438,312	A	4/1969	Becker et al.	
3,577,894	A	5/1971	Emerson	
3,626,702	A	12/1971	Monahan	
3,757,481	A	9/1973	Skinner	
3,802,790	A	4/1974	Blackburn	
3,909,996	A	10/1975	Ettlinger, Jr. et al.	
4,026,083	A	5/1977	Hoyt et al.	
4,146,599	A	3/1979	Lanzetta	
4,287,693	A *	9/1981	Collette	A47G 27/0212 428/134
4,405,665	A	9/1983	Beaussier et al.	
4,445,802	A	5/1984	Loov	
4,629,358	A	12/1986	Springston et al.	
4,637,942	A	1/1987	Tomarin	
4,658,554	A	4/1987	Riley et al.	
4,727,697	A	3/1988	Vaux	
5,044,821	A *	9/1991	Johnsen	E02D 31/02 405/50
5,073,061	A	12/1991	Jones	
5,102,260	A	4/1992	Horvath et al.	
5,102,703	A	4/1992	Colonel et al.	
5,292,130	A	3/1994	Hooper	
5,342,141	A	8/1994	Close	
5,363,614	A	11/1994	Faulkner	
5,383,314	A	1/1995	Rothberg	
5,460,867	A	10/1995	Magnuson et al.	
5,514,722	A	5/1996	DiGeronimo	
5,531,044	A	7/1996	Wallenius	
5,640,801	A	6/1997	Rynberk	
5,888,614	A	3/1999	Slocum et al.	
5,916,034	A	6/1999	Lancia	
5,920,915	A	7/1999	Bainbridge et al.	
5,957,619	A	9/1999	Kinoshita et al.	
6,032,300	A	3/2000	Bainbridge et al.	
6,033,146	A	3/2000	Shaw et al.	
6,055,676	A	5/2000	Bainbridge et al.	
6,098,209	A	8/2000	Bainbridge et al.	
6,301,722	B1	10/2001	Nickerson et al.	
6,357,054	B1	3/2002	Bainbridge et al.	
6,453,477	B1	9/2002	Bainbridge et al.	
6,468,629	B1	10/2002	Lodder	
6,551,016	B2	4/2003	Guidon	
6,616,542	B1 *	9/2003	Reddick	A63B 69/3661 428/17
6,740,387	B1	5/2004	Lemieux	
6,796,096	B1	9/2004	Heath	
6,802,669	B2	10/2004	Ianniello et al.	
6,818,274	B1	11/2004	Buck et al.	
6,877,932	B2	4/2005	Prevost	
7,014,390	B1	3/2006	Morris	
7,090,430	B1	8/2006	Fletcher	
7,114,298	B2	10/2006	Kotler	
7,131,788	B2	11/2006	Ianniello et al.	
7,244,076	B2	7/2007	Whitson	
7,244,477	B2	7/2007	Sawyer et al.	
7,273,642	B2	9/2007	Prevost	
7,387,832	B2	6/2008	Hashiba et al.	
7,487,622	B2	2/2009	Wang	
7,516,587	B2	4/2009	Barlow	
7,563,052	B2	7/2009	Van Reijen	
7,587,865	B2	9/2009	Moller, Jr.	
7,645,501	B2	1/2010	Sawyer et al.	
7,662,468	B2	2/2010	Bainbridge	
7,722,287	B2	5/2010	Swank	
7,771,814	B2 *	8/2010	Grimble	B27N 5/00 249/16
7,900,416	B1	3/2011	Yokubison et al.	
D637,318	S	5/2011	Sawyer et al.	
7,955,025	B2	6/2011	Murphy et al.	
D645,169	S	9/2011	Runkles	
8,109,050	B2	2/2012	Ovaert	
8,221,856	B2	7/2012	Stroppiana	
8,225,566	B2	7/2012	Prevost et al.	
8,236,392	B2 *	8/2012	Sawyer	E01C 13/02 404/35
8,341,896	B2	1/2013	Moller, Jr. et al.	
8,353,640	B2 *	1/2013	Sawyer	E01C 11/225 404/2
8,568,840	B2 *	10/2013	Sawyer	E01C 13/02 428/131
8,597,754	B2 *	12/2013	Sawyer	E01C 13/02 428/131
8,603,301	B2 *	12/2013	Heins	B01D 1/065 159/47.3
8,662,787	B2	3/2014	Sawyer et al.	
9,289,085	B2 *	3/2016	Thrush	B32B 3/02
2001/0002497	A1	6/2001	Scuero	
2001/0048849	A1	12/2001	Rinninger	
2003/0020057	A1	1/2003	Sciandra	
2003/0223826	A1	12/2003	Ianniello	
2004/0058096	A1 *	3/2004	Prevost	A63C 19/04 428/17
2004/0069924	A1	4/2004	Lemieux et al.	
2005/0028475	A1	2/2005	Barlow et al.	
2005/0042394	A1 *	2/2005	Sawyer	E01C 13/08 428/17
2006/0032170	A1	2/2006	Vershum et al.	
2006/0081159	A1	4/2006	Chapman et al.	
2006/0141231	A1	6/2006	Lemieux	
2007/0166508	A1	7/2007	Waterford	
2008/0113161	A1 *	5/2008	Grimble	B27N 5/00 428/174
2008/0216437	A1 *	9/2008	Prevost	E01C 13/08 52/589.1
2008/0219770	A1	9/2008	Prevost et al.	
2008/0240860	A1 *	10/2008	Ianniello	E01C 13/02 405/53
2009/0162579	A1	6/2009	McDuff	
2009/0188172	A1	7/2009	Duharme et al.	
2009/0208674	A1	8/2009	Murphy et al.	
2009/0232597	A1	9/2009	Zwier et al.	
2009/0325720	A1	12/2009	Chapman	
2010/0104778	A1	4/2010	Wise	
2010/0173116	A1	7/2010	Bainbridge	
2010/0239790	A1	9/2010	Stricklen et al.	
2010/0279032	A1	11/2010	Chereau et al.	
2012/0301638	A1 *	11/2012	Sawyer	E01C 13/02 428/17
2013/0101351	A1 *	4/2013	Sawyer	E01C 13/02 405/38
2013/0101777	A1 *	4/2013	Sawyer	E01C 13/02 428/58
2013/0142971	A1 *	6/2013	Sawyer	E01C 13/02 428/33

FOREIGN PATENT DOCUMENTS

DE	9310473	U1	9/1993
DE	20119065	U1	5/2002
EP	1243698	A1	9/2002
FR	871775		5/1979
FR	2495453	A1	6/1982
FR	2616655	A1	12/1988
FR	2762635	A1	10/1998
GB	1378494		12/1974
JP	54032371	U	3/1979
JP	H03197703	A	8/1991

(56) **References Cited**

FOREIGN PATENT DOCUMENTS

JP	7-137189		5/1995
JP	8049209	A	2/1996
JP	2000-034823		2/2000
JP	2006130288		5/2006
JP	2008008039	A	1/2008
KR	100881167	B1	2/2009
KR	20120004054	U	6/2012
NL	1004405	C1	2/1997
WO	9856993		12/1998
WO	9926784	A	6/1999
WO	9928557		6/1999
WO	02/09825	A1	2/2002
WO	02075053	A1	9/2002
WO	03/000994	A1	1/2003
WO	2004/011724	A1	2/2004
WO	2006116450	A2	11/2006
WO	2007/002442	A1	1/2007
WO	2008011708	A1	1/2008

OTHER PUBLICATIONS

Cork Underlayment—Rolls & Sheets, www.ecobydesign.com/shop/cork/cork_underlayment.html., Jul. 24, 2003.

Dynamic Cushioning Performance, JSP International, 1998.

European Examination Report, Application No. EP 10 734 609.0 dated Apr. 9, 2013.

European Examination Report, Application No. EP 10734609.0 dated Jun. 27, 2014.

European Office Communication, Application No. EP 10 734 609.0-1601 dated Oct. 16, 2013.

European Search Report, Application No. 10195632A, dated Apr. 12, 2012.

European Search Report, Application No. 10195633.2, dated Apr. 12, 2012.

PCT International Search Report, Application No. PCT/US2010/041046, dated Aug. 17, 2011.

Porex Porous Plastics High Performance Materials, Porex Technologies, 1989.

Product Samples, The engineered plastic foams of JSP International, JSP International, www.jspi.com.

Quiet Walk, Midwest Padding, www.midwestpadding.com/quietwalk/lintro.html, Jul. 24, 2003.

Silent Walk, The Silent Partner in Laiminating Flooring, www.sponge-cushion.com/silent2.htm, Jul. 24, 2003.

Tuplex—General—underlay, flooring underlay, parquet underlay, Tuplex Corp., www.snt-group.net/tuplex/usa/corp.htm., Jul. 24, 2003.

* cited by examiner

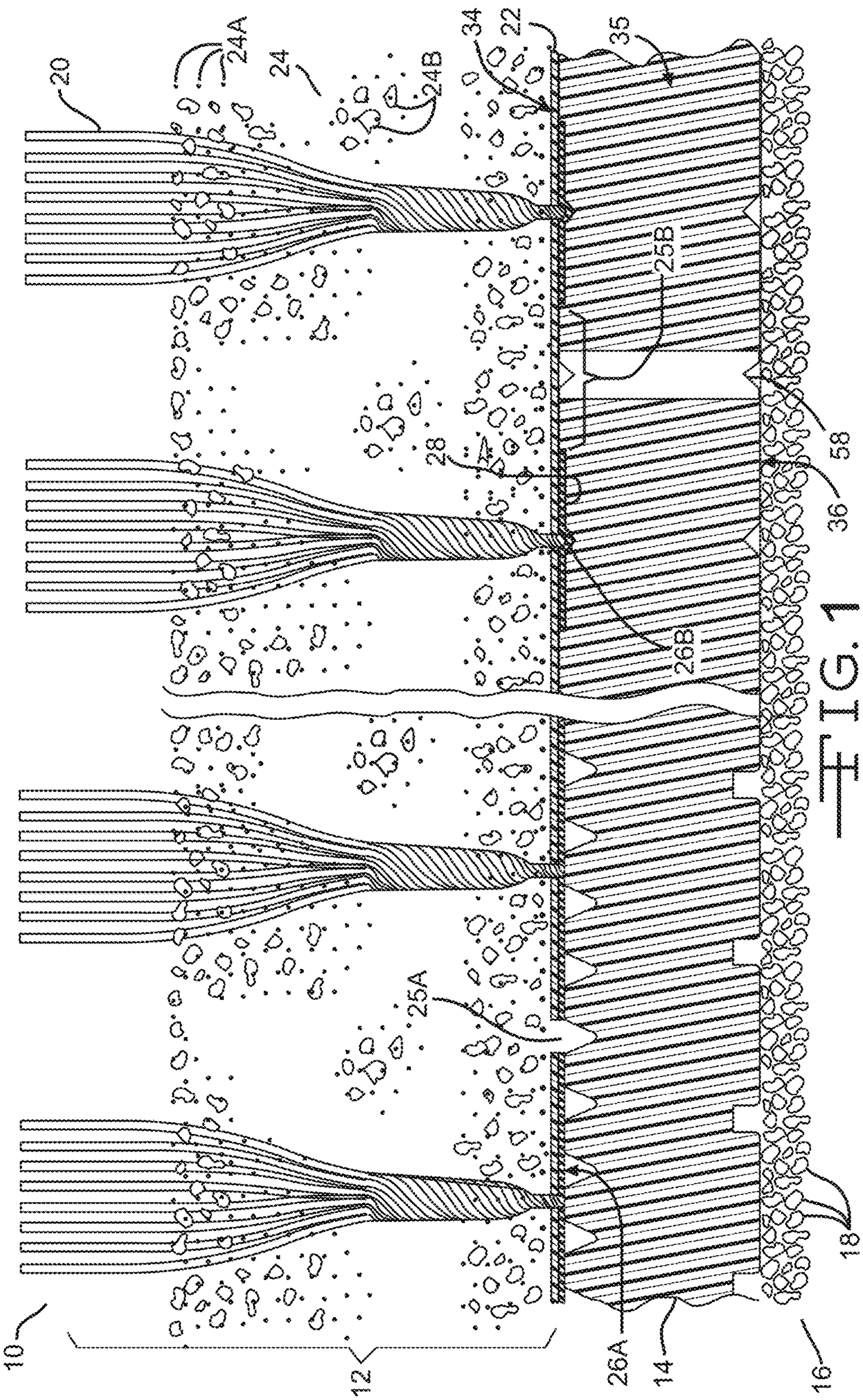


FIG. 1

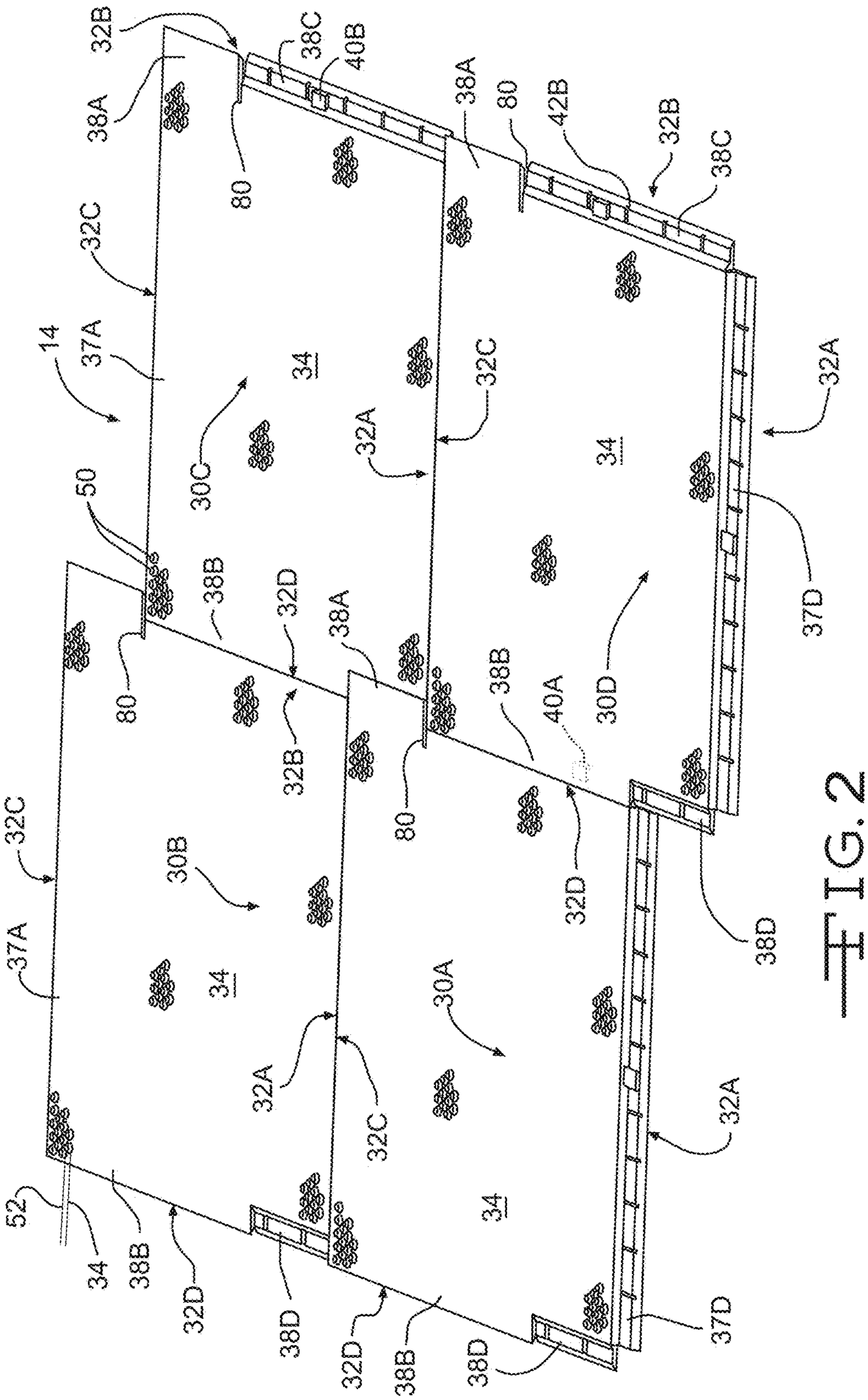

32B
38C
40B
38A
80
42B
32B
38C
32C
14
37A
34
50
30C
32C
32A
34
38B
32D
38A
80
32B
38B
40A
30D
37D
32A
30B
32C
37A
34
32A
30A
32C
52
34
38B
32D
38D
32D
38B
38D
37D
38D

FIG. 2

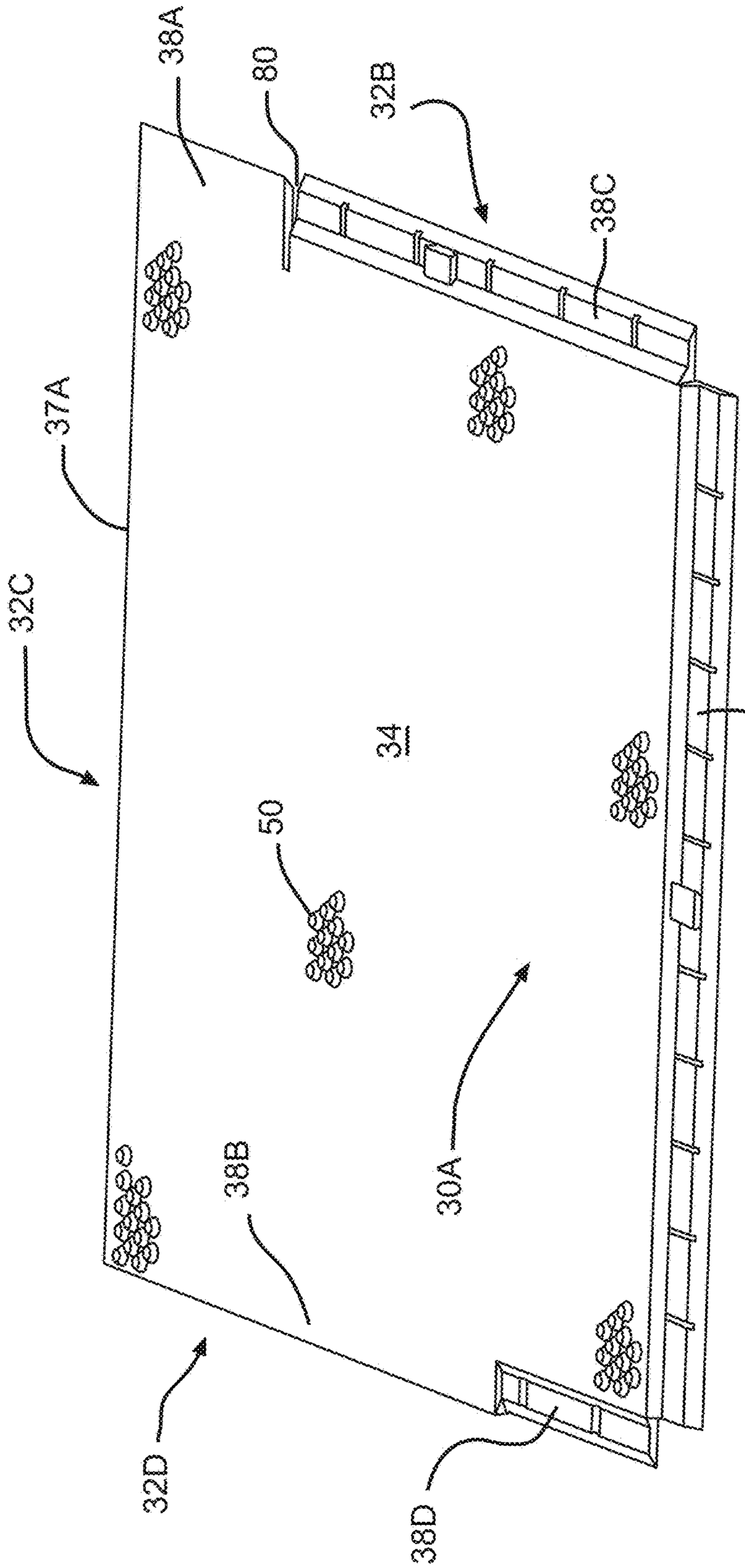


FIG. 2A

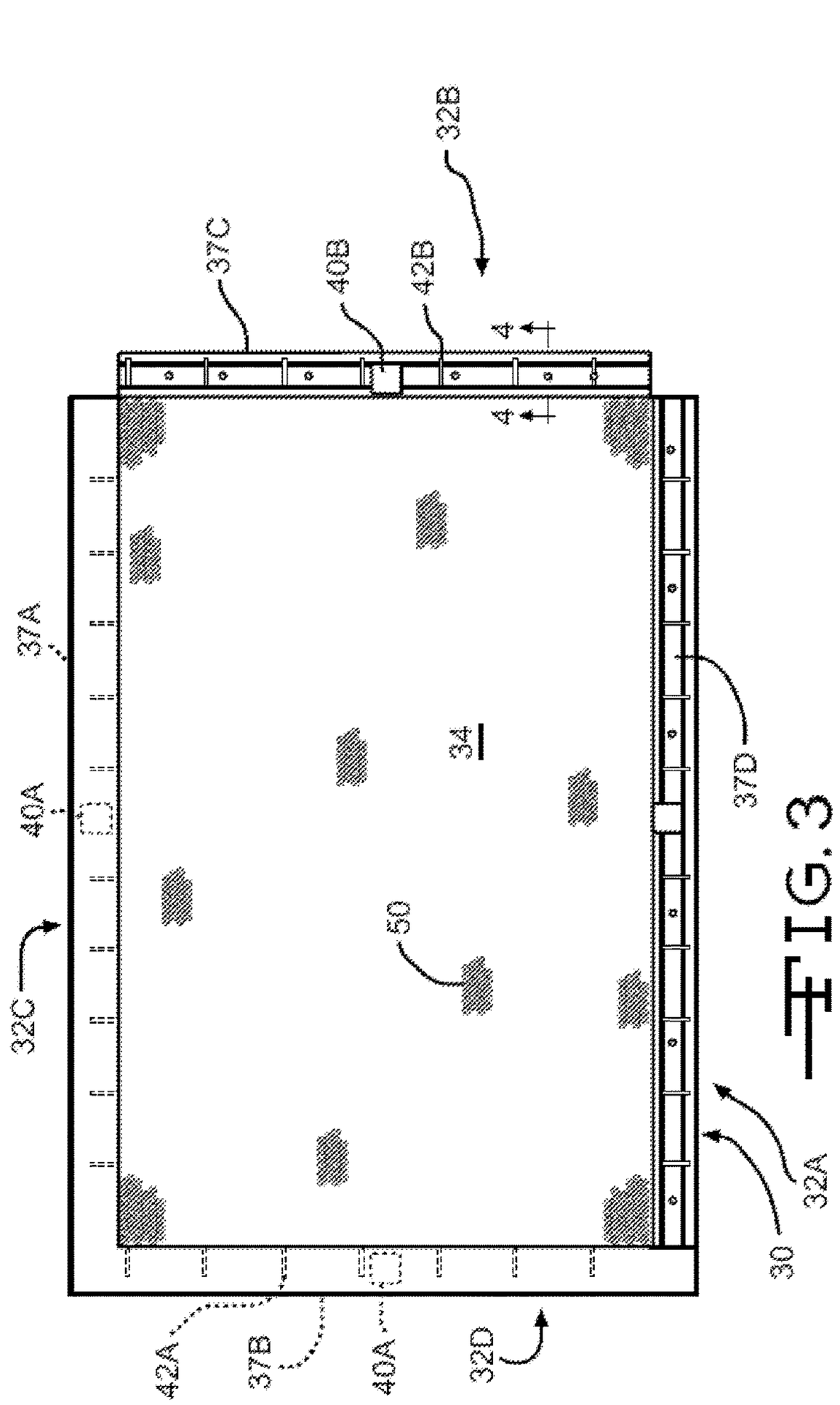

32B
37C
40B
42B
4
4
37A
40A
34
37D
50
32C
42A
37B
40A
32D
30
32A

FIG. 3

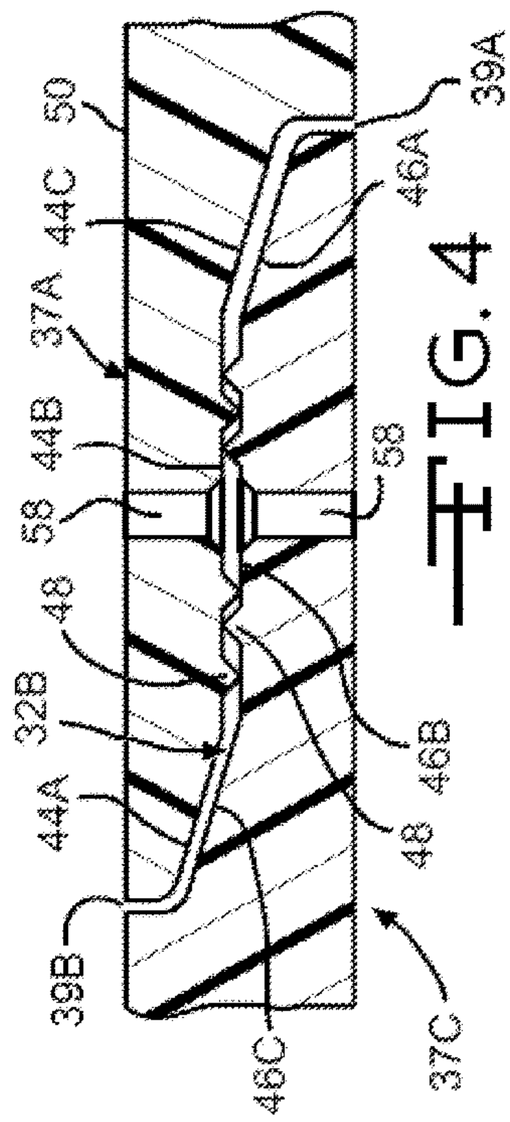

50
39A
46A
44C
37A
44B
58
58
48
32B
48
46B
44A
48
39B
46C
37C

FIG. 4

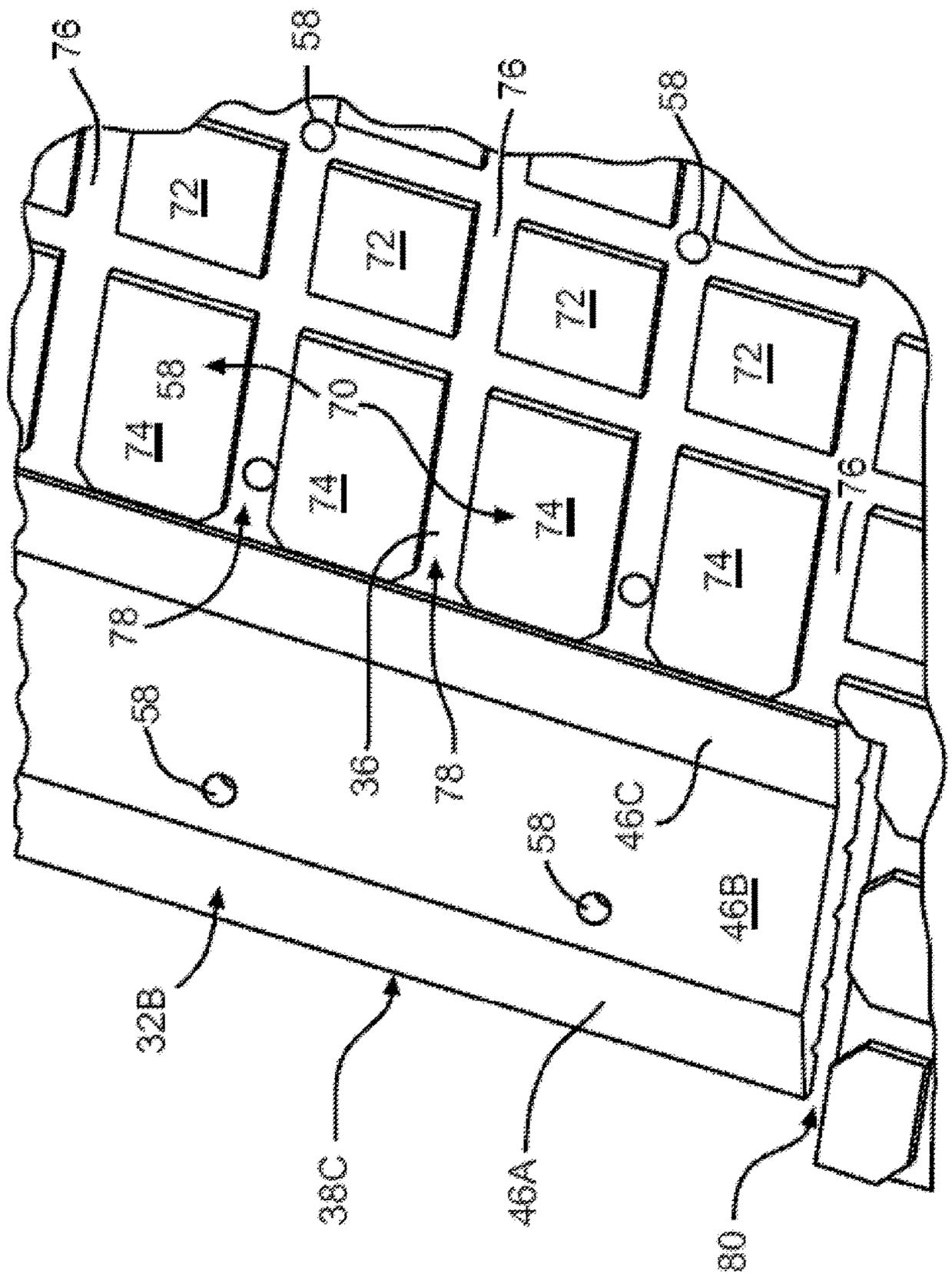

76
58
76
58
72
72
72
72
72
74
58
74
70
74
74
74
76
78
58
36
78
58
46C
46B
32B
38C
46A
80

FIG. 5

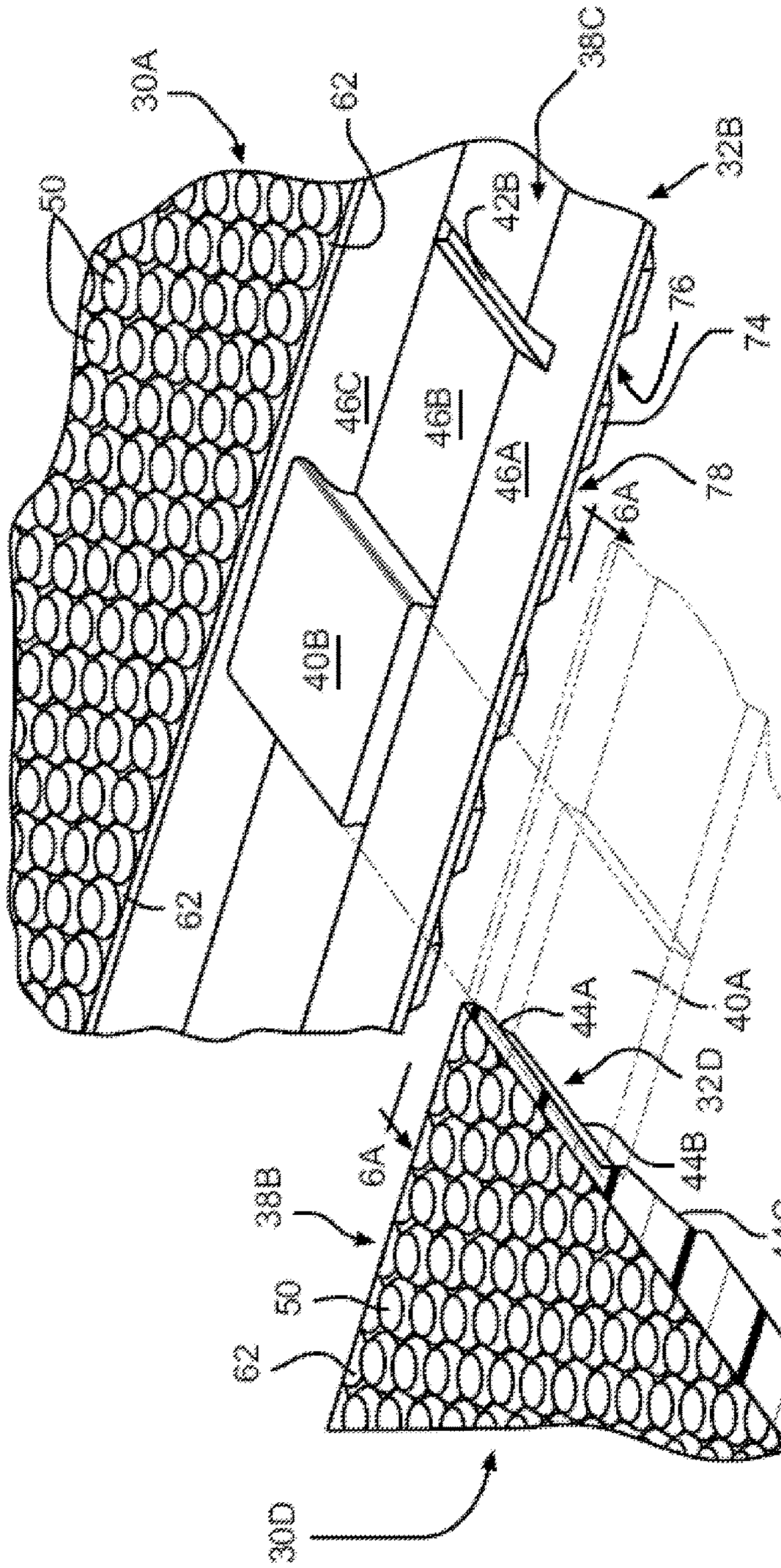

30A
62
38C
32B
42B
50
46C
46B
46A
74
76
78
6A
40B
62
44A
40A
32D
44B
44C
6A
38B
50
62
30D
35

FIG. 6

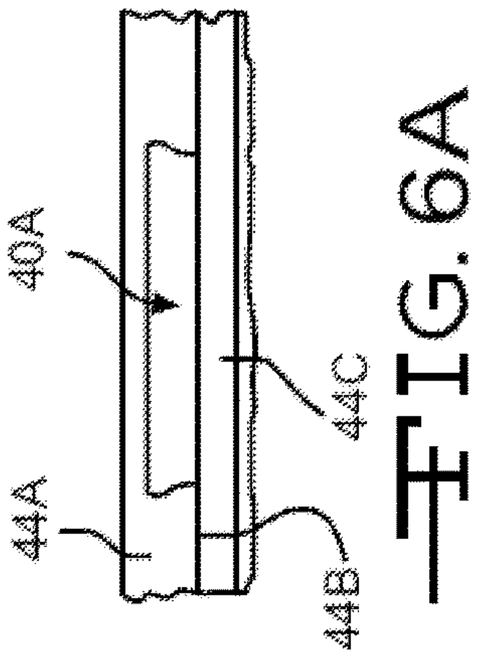

40A
44A
44C
44B

FIG. 6A

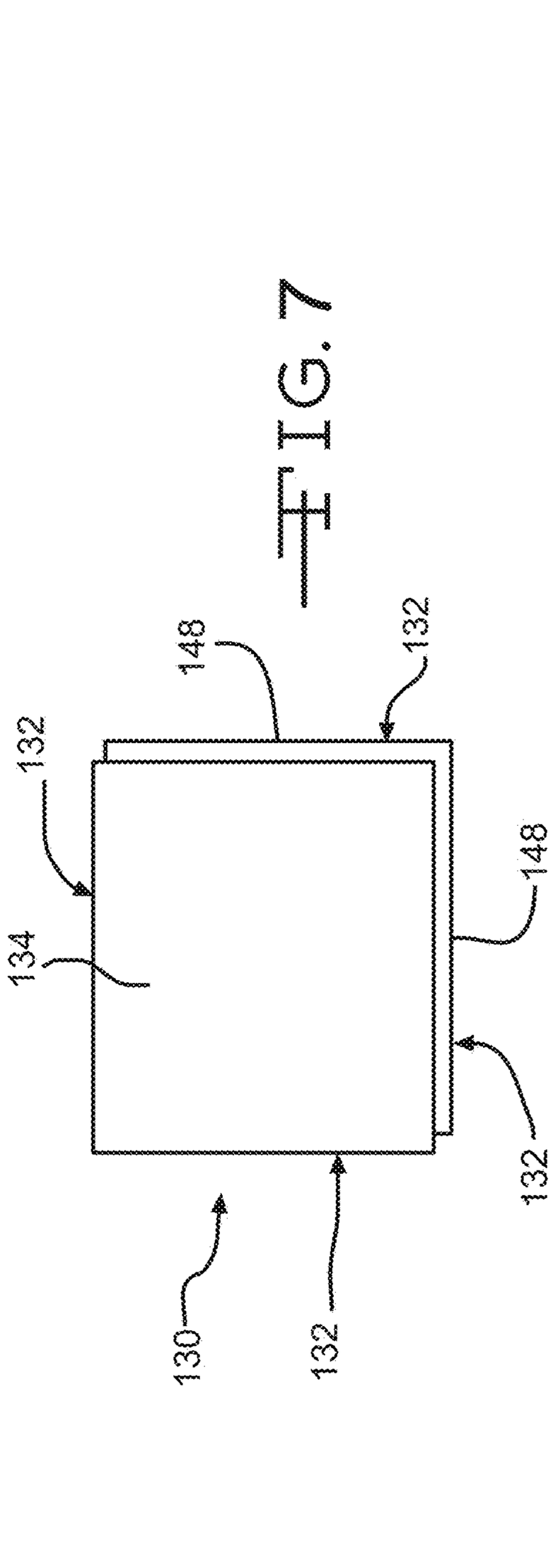

130
132
134
148
132
148
132
130
132
134
148

FIG. 7

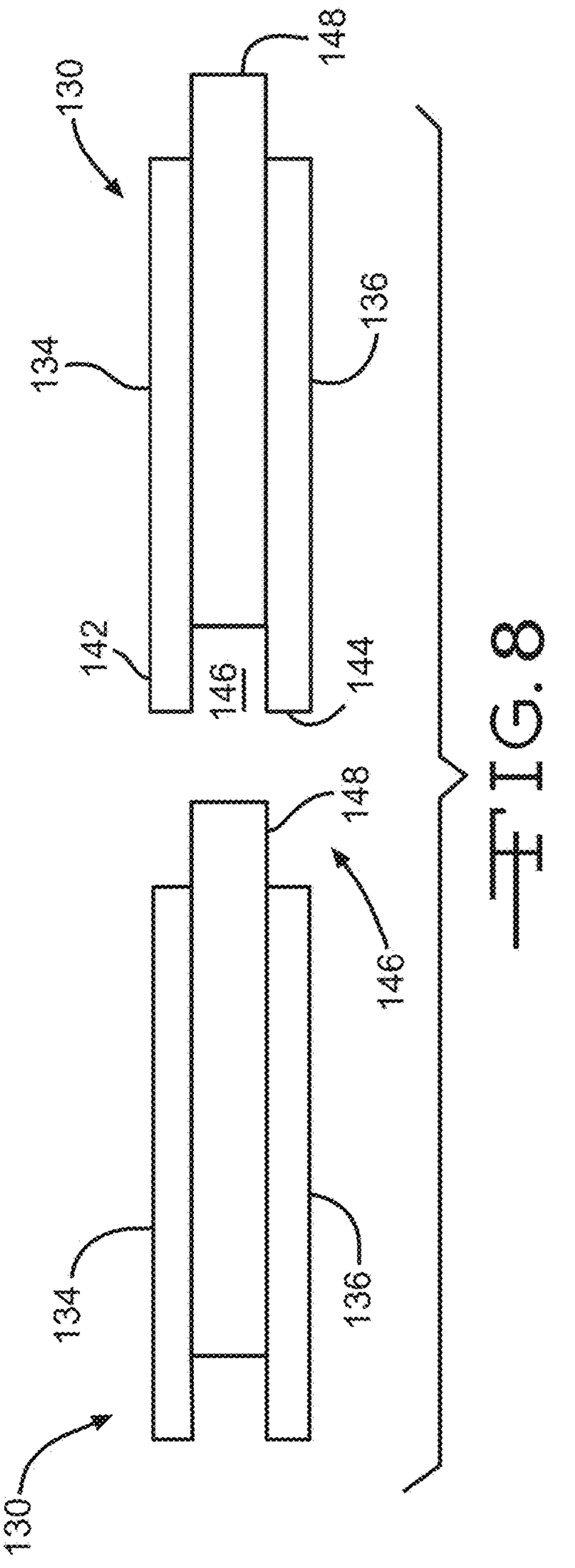

130
134
148
136
142
146
144
148
146
134
136

FIG. 8

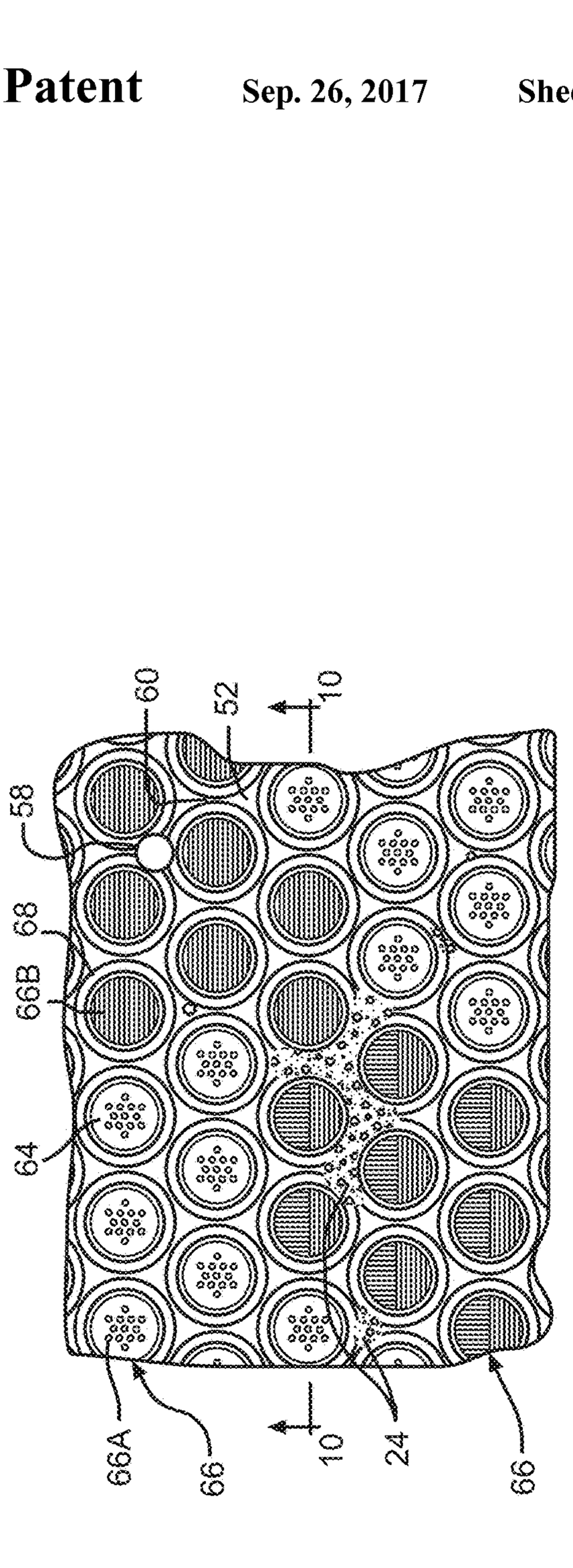

60
52
10
58
68
66B
64
66A
66
10
24
66

FIG. 9

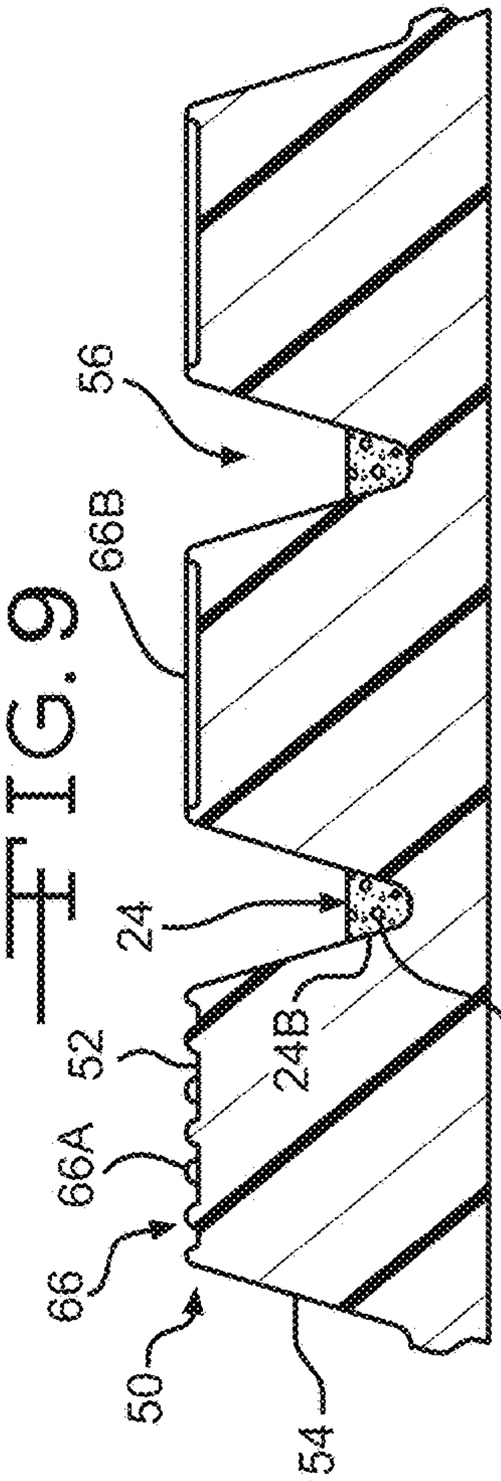

56
66B
24
52
66A
24B
66
24A
50
54

FIG. 10

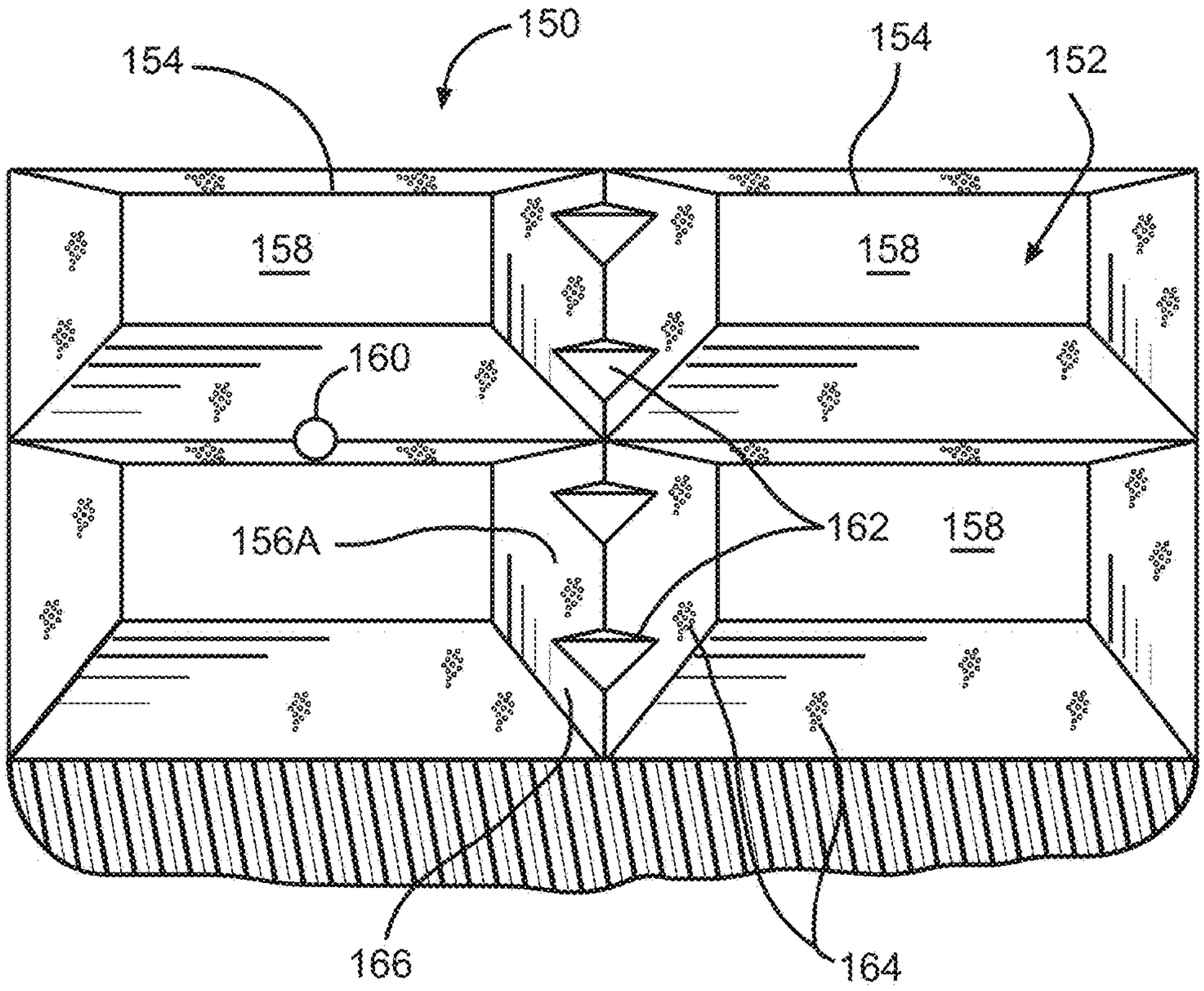


FIG. 11

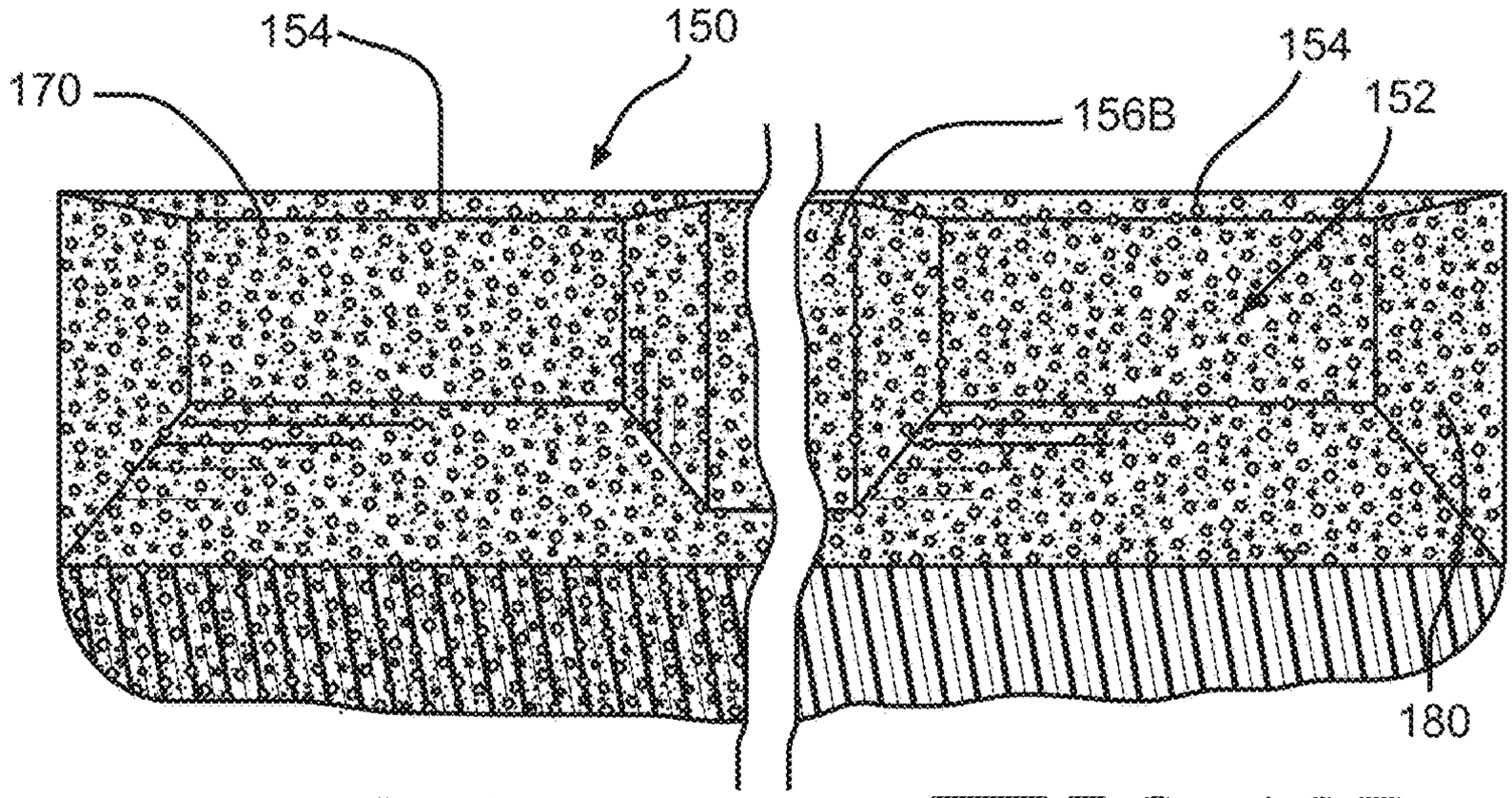


FIG. 12A FIG. 12B

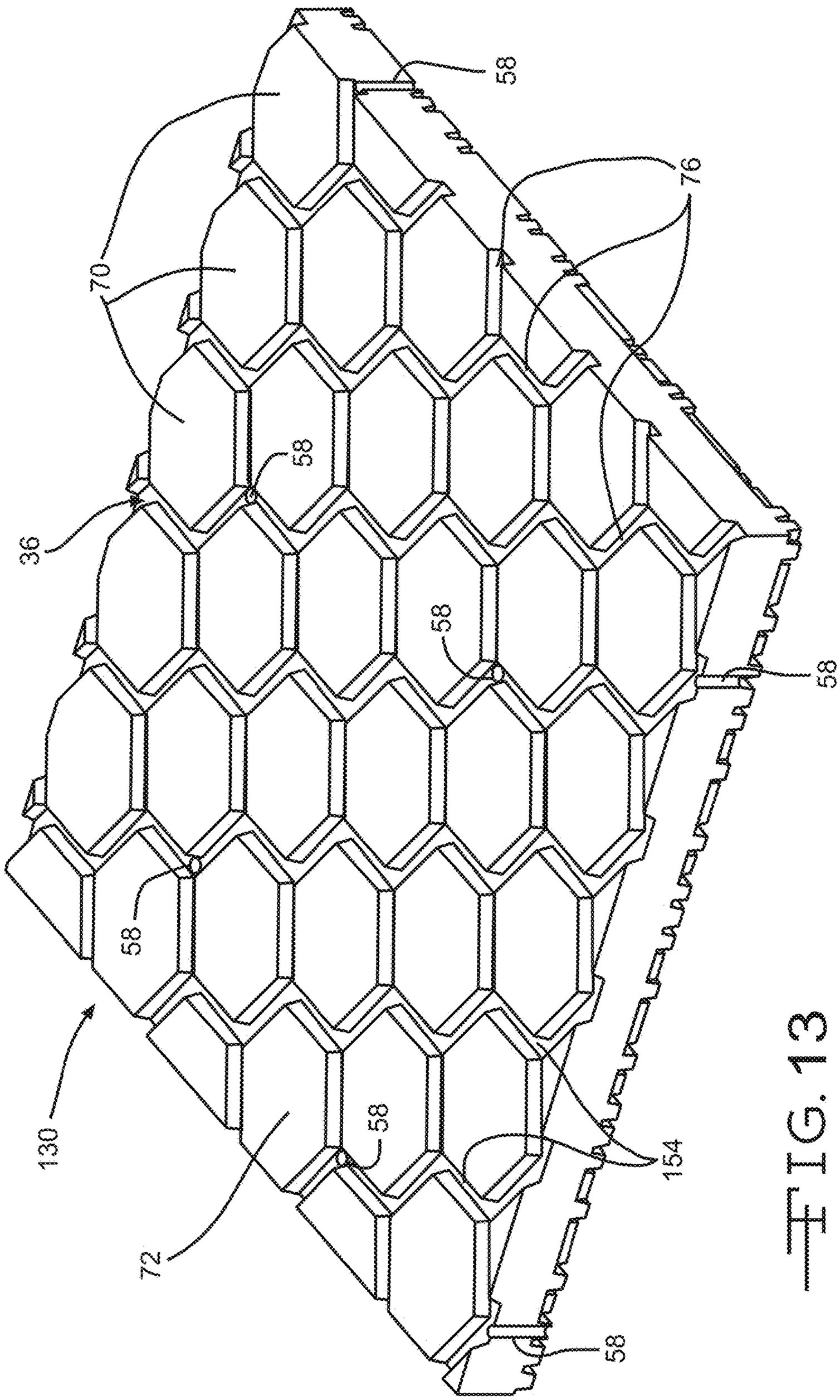


FIG. 13

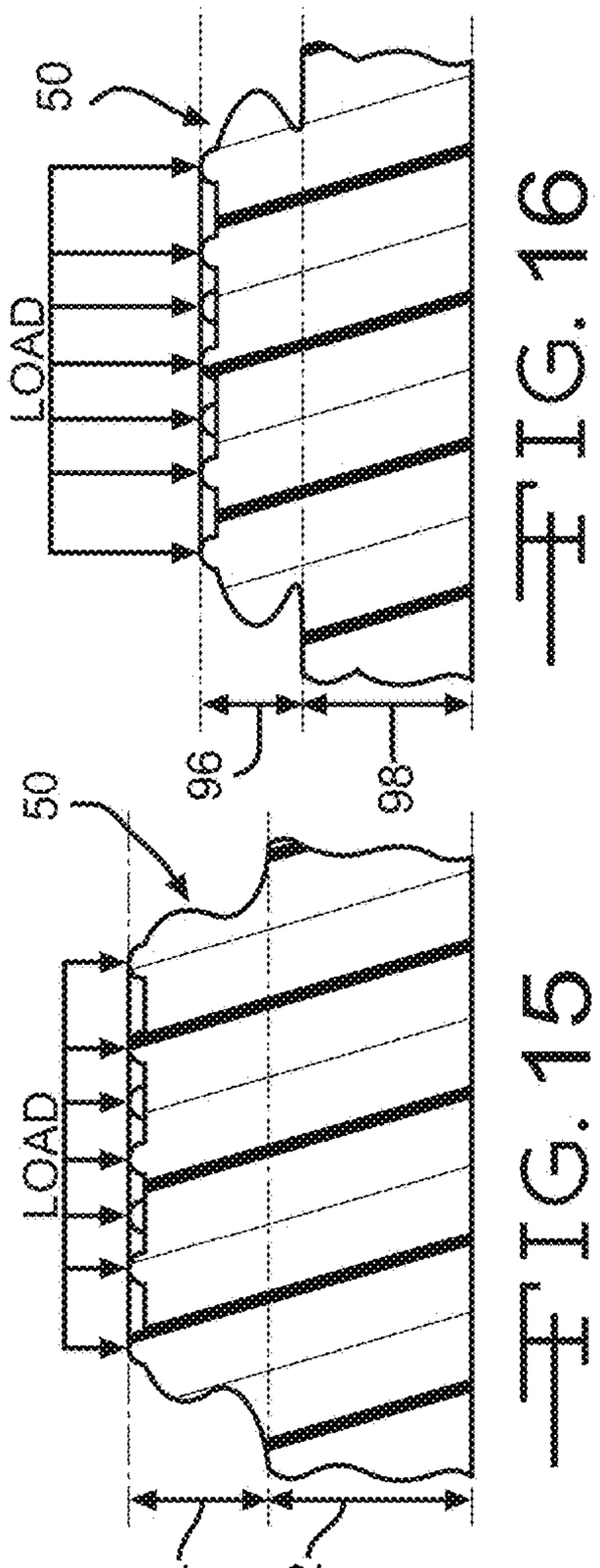


FIG. 16

FIG. 15

FIG. 14

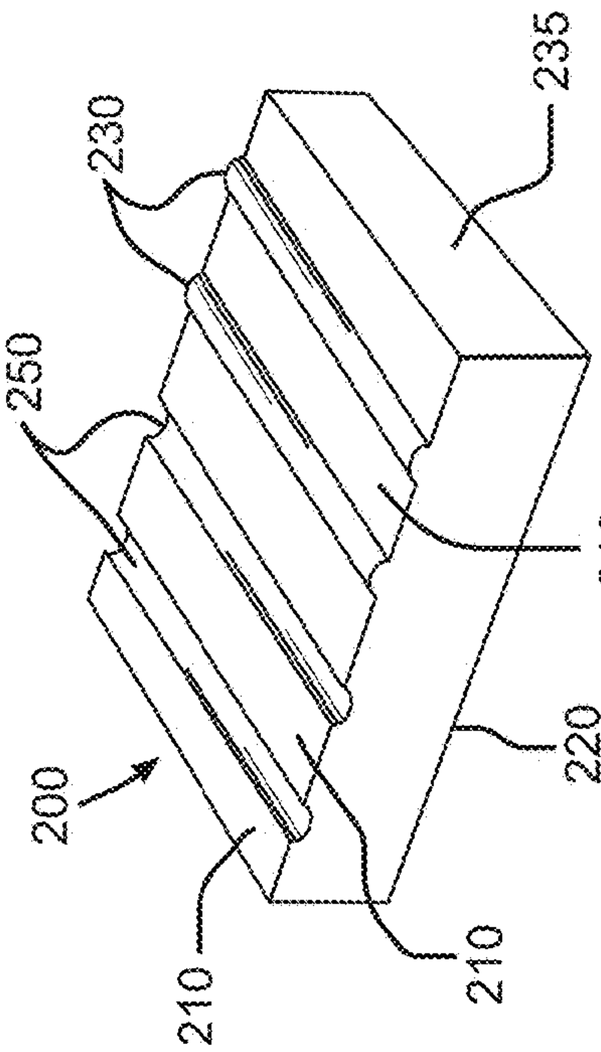


FIG. 17

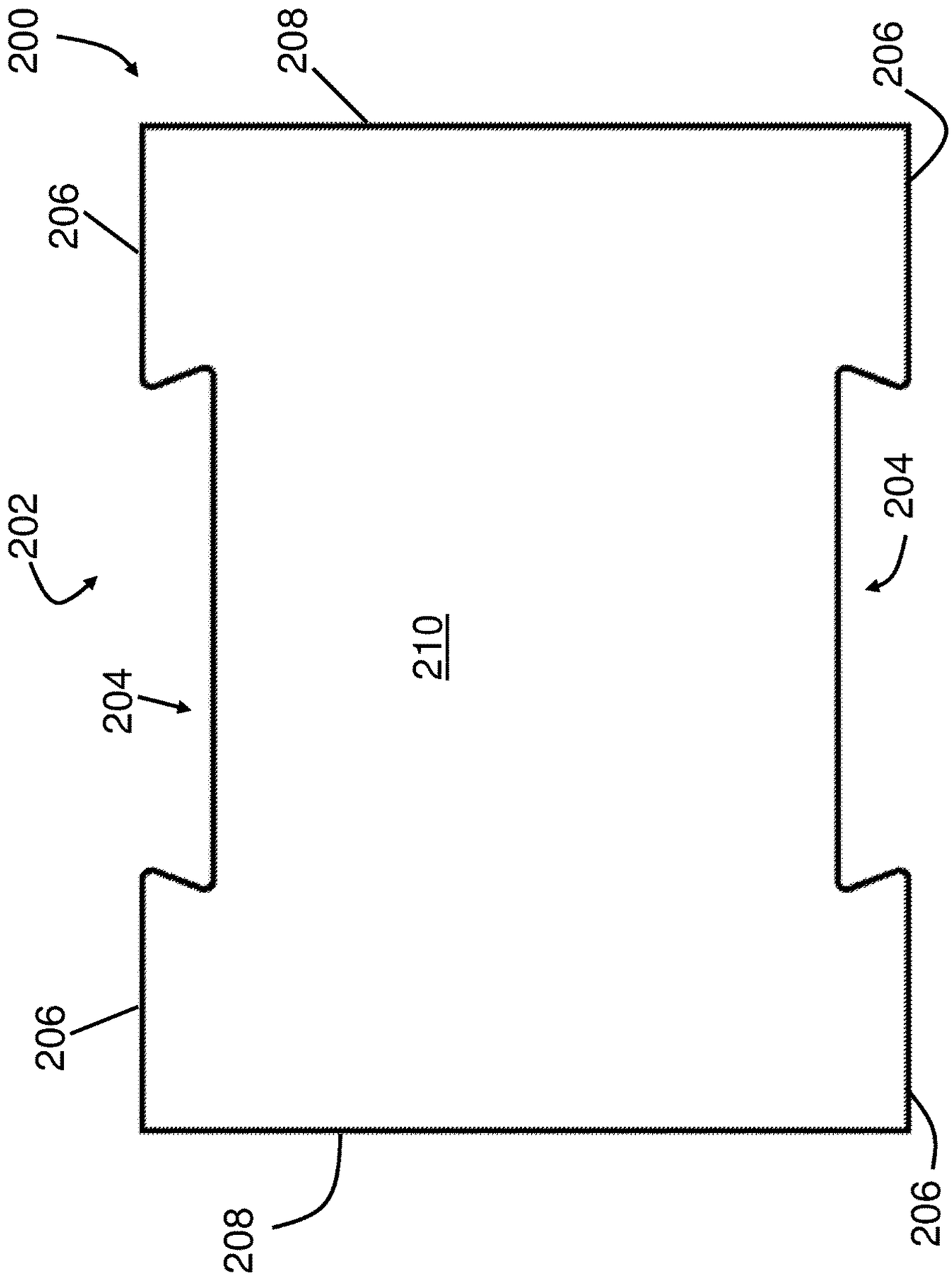


FIG. 18

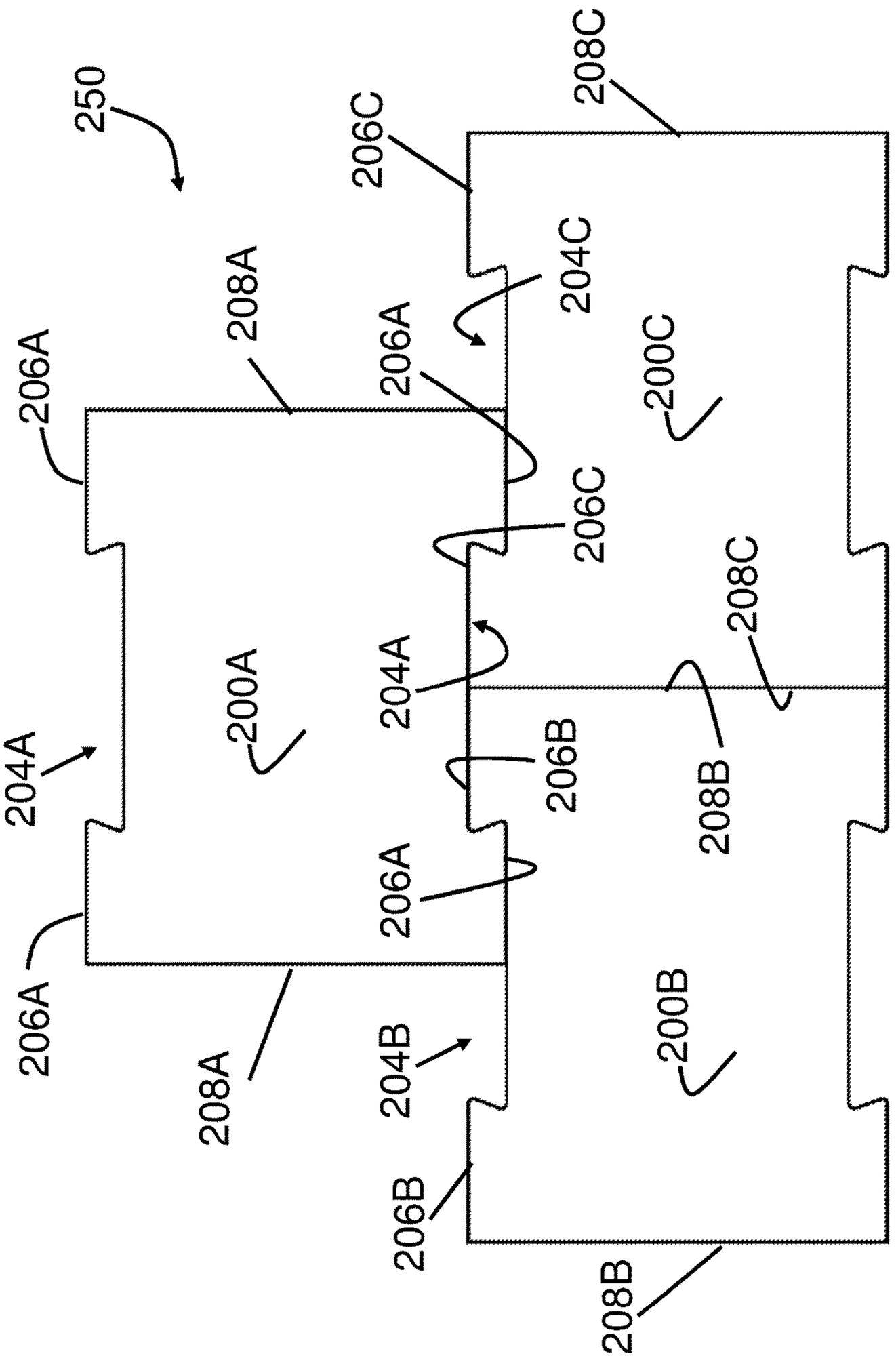

250
206C
208C
206A
208A
206A
204C
200C
206C
204A
200A
206B
208C
204A
206A
208B
206A
208A
204B
200B
206B
208B

FIG. 19

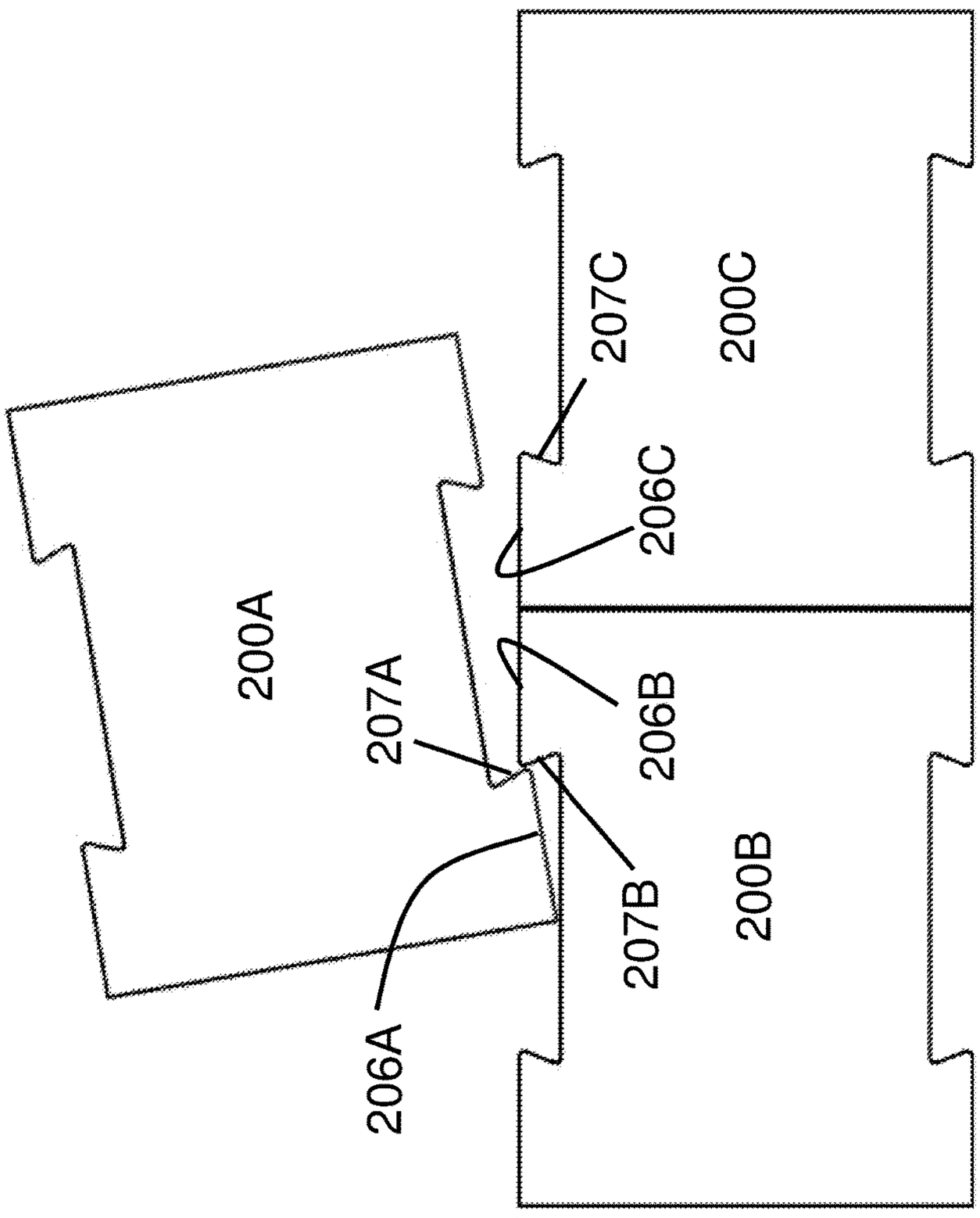


FIG. 2C

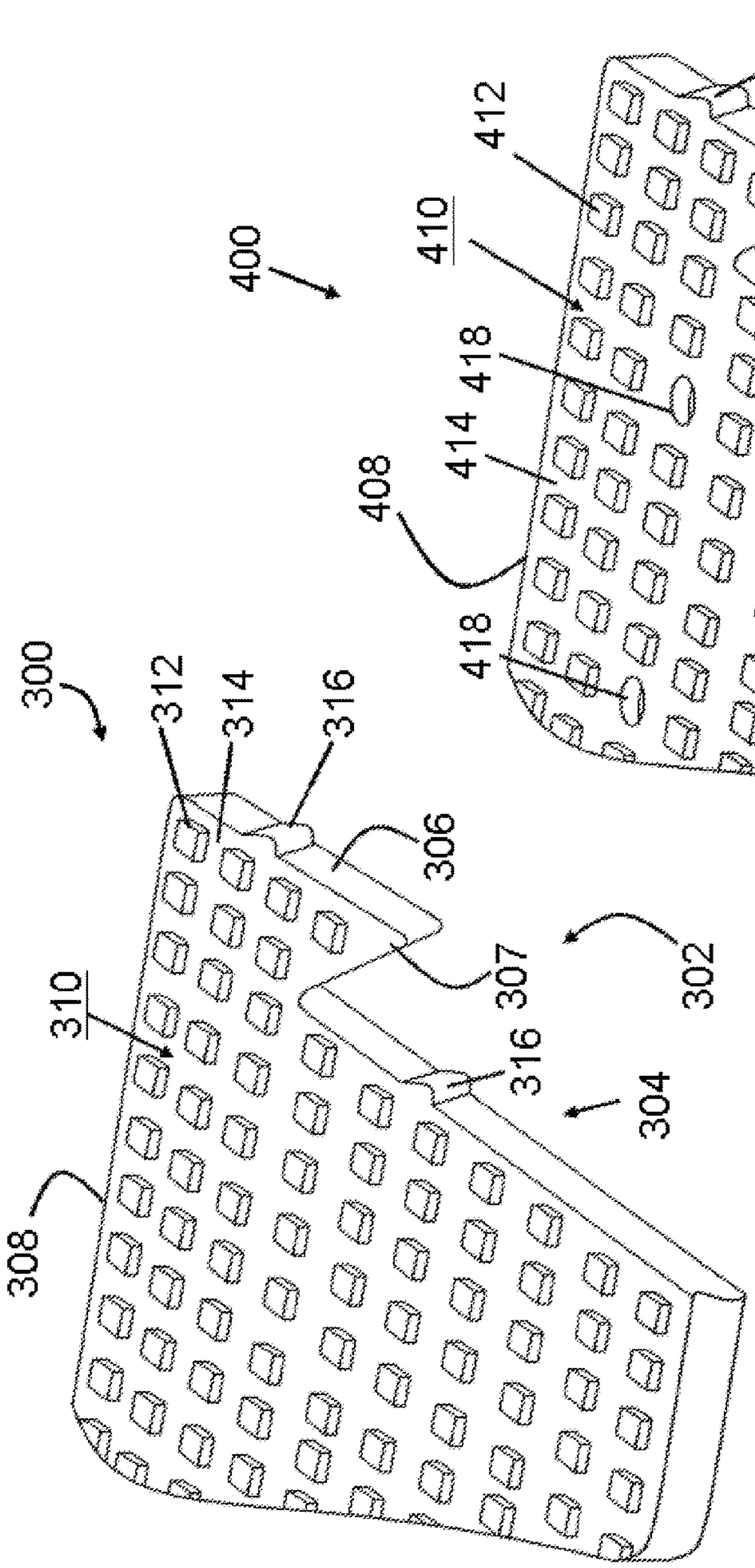

300
312
314
316
306
310
307
302
316
304
308

FIG. 21

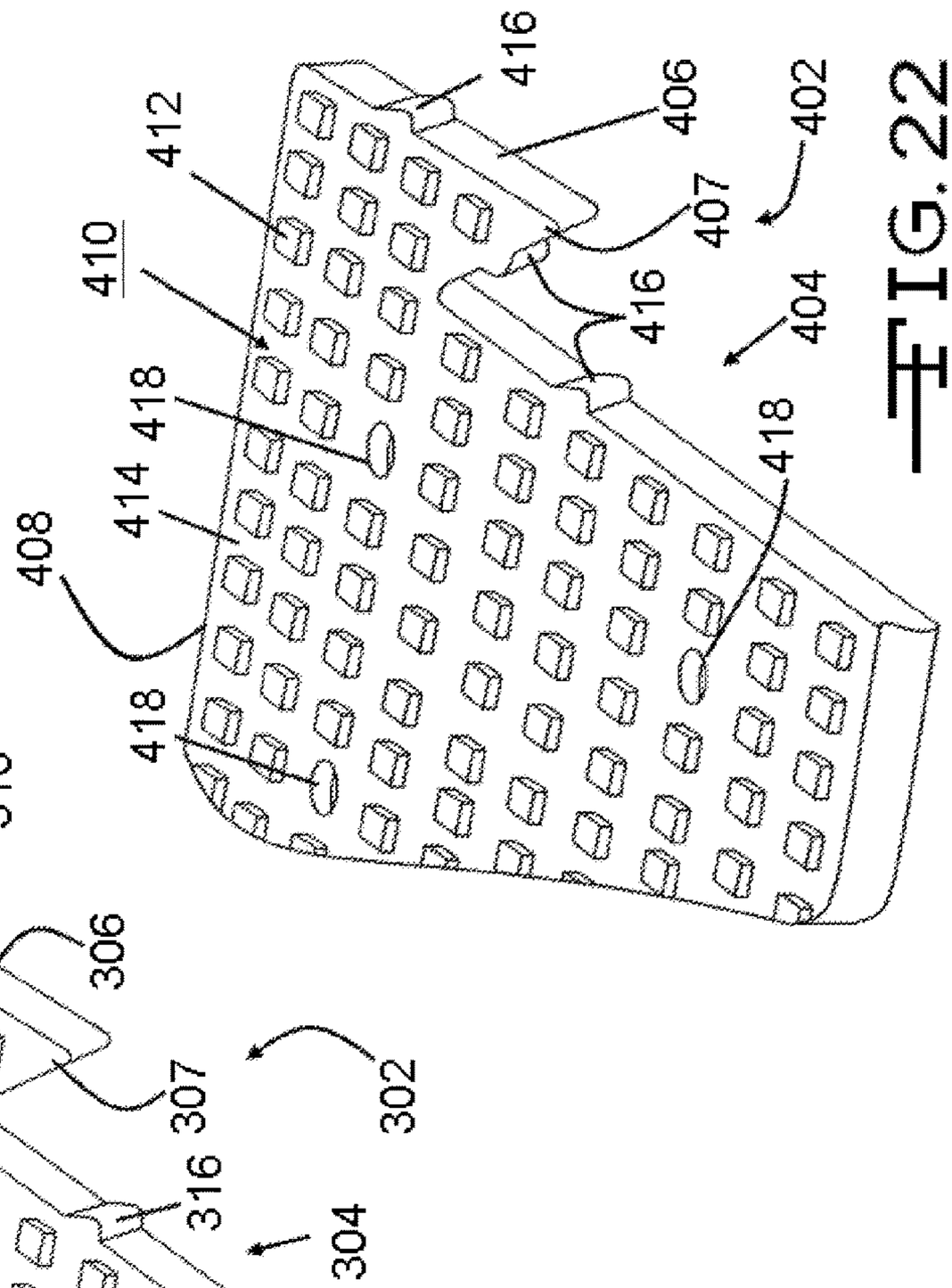

400
412
410
416
406
402
407
416
404
418
414
418
408
418

FIG. 22

BASE FOR TURF SYSTEM

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a Continuation of application of U.S. patent application Ser. No. 13/711,689, filed Dec. 12, 2012, now abandoned. U.S. patent application Ser. No. 13/711,689 is a Continuation of application of U.S. patent application Ser. No. 13/568,611, filed Aug. 7, 2012, now U.S. Pat. No. 8,568,840, issued on Oct. 29, 2013. U.S. Pat. No. 8,568,840 is a Continuation application of U.S. patent application Ser. No. 12/009,835, filed Jan. 22, 2008, now U.S. Pat. No. 8,236,392, issued Aug. 7, 2012, which claims the benefit of U.S. Provisional Application No. 60/881,293, filed Jan. 19, 2007; U.S. Provisional Application No. 60/927,975, filed May 7, 2007; U.S. Provisional Application No. 61/000,503, filed Oct. 26, 2007; and U.S. Provisional Application No. 61/003,731, filed Nov. 20, 2007, the disclosures of which are incorporated herein by reference.

TECHNICAL FIELD

This invention relates in general to artificial turf systems of the type used in athletic fields, ornamental lawns and gardens, and playgrounds.

BACKGROUND OF THE INVENTION

Artificial turf systems are commonly used for sports playing fields and more particularly to artificial playing fields. Artificial turf systems can also be used for synthetic lawns and golf courses, rugby fields, playgrounds, and other similar types of fields or floor coverings. Artificial turf systems typically comprise a turf assembly and a foundation, which can be made of such materials as asphalt, graded earth, compacted gravel or crushed rock. Optionally, an underlying resilient base or underlayment layer may be disposed between the turf assembly and the foundation. The turf assembly is typically made of strands of plastic artificial grass blades attached to a turf backing. An infill material, which typically is a mixture of sand and ground rubber particles, may be applied among the vertically oriented artificial grass blades, typically covering the lower half or ⅔ of the blades.

SUMMARY OF THE INVENTION

This invention relates to a turf underlayment layer configured to support an artificial turf assembly. The turf underlayment layer has panels including edges that are configured to interlock with the edges of adjacent panels to form a vertical interlocking connection. The interlocking connection is capable of substantially preventing relative vertical movement of one panel with respect to an adjacent connected panel. The underlayment comprises a core with a top side and a bottom side. The top side has a plurality of spaced apart, upwardly oriented projections that define channels suitable for water flow along the top side of the core when the underlayment layer is positioned beneath an overlying artificial turf assembly.

The top side may include an upper support surface in contact with the artificial turf assembly. The upper support surface, in turn, may have a plurality of channels configured to allow water flow along the top side of the core. The upper support surfaces may be substantially flat. The bottom side may include a lower support surface that is in contact with a foundation layer and also have a plurality of channels configured to allow water flow along the bottom side of the core. A plurality of spaced apart drain holes connects the upper support surface channels with the lower support surface channels to allow water flow through the core.

The plurality of spaced apart projections on the top side are deformable under a compressive load. The projections define a first deformation characteristic associated with an athletic response characteristic and the core defines a second deformation characteristic associated with a bodily impact characteristic. The first and second deformation characteristics are complimentary to provide a turf system bodily impact characteristic and a turf system athletic response characteristic.

A method of assembling an underlayment layer to an adjacent underlayment layer includes providing a first underlayment layer on top of a substrate. The underlayment layer has at least one edge with a top side flap, a bottom side flap, and a flap assembly groove disposed therebetween. A second underlayment layer is positioned adjacent to the first underlayment layer and on top of the substrate. The second underlayment layer also ahs at least one edge with a top side flap, a bottom side flap, and a flap assembly groove disposed therebetween. The first underlayment layer top side flap is deflected in an upward direction between a corner and the flap assembly groove. The second underlayment layer bottom side flap is inserted under the upwardly deflected first underlayment layer top side flap. Finally, the first underlayment layer top side flap is downwardly deflected into engagement with the second underlayment layer bottom side flap.

Various aspects of this invention will become apparent to those skilled in the art from the following detailed description of the preferred embodiment, when read in light of the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** is a schematic cross-sectional view in elevation of an artificial turf system.

FIG. **2** is a schematic perspective view of an embodiment of an underlayment panel assembly.

FIG. **2**A is an enlarged, perspective view of an underlayment panel of the panel assembly of FIG. **2**.

FIG. **3** is an enlarged plan view of an alternative embodiment of an underlayment panel.

FIG. **4** is an enlarged cross sectional view, in elevation, of the interlocking edge of the underlayment panel of FIG. **3** and an adjacent mated underlayment panel.

FIG. **5** is an enlarged view of an embodiment of an interlocking edge and bottom side projections of the underlayment panel.

FIG. **6** is a schematic perspective view of the assembly of the interlocking edges of adjacent underlayment panels.

FIG. **6**A is a schematic plan view of the interlocking edge of FIG. **6**.

FIG. **7** is a plan view of an alternative embodiment of the interlocking edges of the underlayment panels.

FIG. **8** is an elevation view of the assembly of the interlocking edges of adjacent underlayment panels of FIG. **7**.

FIG. **9** is an enlarged plan view of an embodiment of a drainage channel and infill trap and a frictional surface of the underlayment panel.

FIG. **10** is an elevation view in cross section of the drainage channel and infill trap of FIG. **9**.

FIG. **11** is a plan view of another embodiment of a frictional surface of the underlayment panel.

FIG. **12**A is a plan view of another embodiment of a frictional surface of the underlayment panel.

FIG. **12**B is a plan view of another embodiment of a frictional surface of the underlayment panel.

FIG. **13** is a perspective view of an embodiment of a bottom side of the underlayment drainage panel.

FIG. **14** is a cross-sectional view in elevation of an underlayment panel showing projections in a free-state, unloaded condition.

FIG. **15** is a cross-sectional view in elevation of the underlayment panel of FIG. **14** showing the deflection of the projections under a vertical load.

FIG. **16** is a cross-sectional view in elevation of the underlayment panel of FIG. **15** showing the deflection of the projections and panel core under an increased vertical load.

FIG. **17** is a perspective view of a panel with spaced apart friction members configured to interact with downwardly oriented ridges on the artificial turf assembly.

FIG. **18** is a schematic, plan view of another embodiment of an underlayment panel.

FIG. **19** is a schematic, plan view of an underlayment panel assembly formed from panels similar to the panel of FIG. **18**.

FIG. **20** is a schematic, plan view of a method of assembling the underlayment panel assembly of FIG. **19**.

FIG. **21** is a sectioned, perspective view of another embodiment of an underlayment panel.

FIG. **22** is a sectioned, perspective view of yet another embodiment of an underlayment panel, similar to the underlayment panel of FIG. **21**.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The turf system shown in FIG. **1** is indicated generally at **10**. The turf system includes an artificial turf assembly **12**, an underlayment layer **14** and a foundation layer **16**. The foundation layer **16** can comprise a layer **18** of crushed stone or aggregate, or any other suitable material. Numerous types of foundation layers are known to those skilled in the art. The crushed stone layer **18** can be laid on a foundation base, such as compacted soil, a poured concrete base, or a layer of asphalt paving, not shown. Alternatively, the underlayment layer **14** may be applied over the asphalt or concrete base, omitting the crushed stone layer, if so desired. In many turf systems used for an athletic field, the foundation layers are graded to a contour such that water will drain to the perimeter of the field and no water will pool anywhere on the surface.

The artificial turf assembly **12** includes strands of synthetic grass blades **20** attached to a turf backing **22**. An optional infill material **24** may be applied to the grass blades **20**. The synthetic grass blades **20** can be made of any material suitable for artificial turf, many examples of which are well known in the art. Typically the synthetic grass blades are about 5 cm in length although any length can be used. The blades **20** of artificial grass are securely placed or tufted onto the backing **22**. One form of blades that can be used is a relatively wide polymer film that is slit or fibrillated into several thinner film blades after the wide film is tufted onto the backing **22**. In another form, the blades **20** are relatively thin polymer films (monofilament) that look like individual grass blades without being fibrillated. Both of these can be colored to look like blades of grass and are attached to the backing **22**.

The backing layer **22** of the turf assembly **12** is typically water-porous by itself, but is often optionally coated with a water-impervious coating **26**A, such as for example urethane, for dimensional stability of the turf. In order to allow water to drain vertically through the backing **22**, the backing can be provided with spaced apart holes **25**A. In an alternative arrangement, the water impervious coating is either partially applied, or is applied fully and then scraped off in some portions, such as drain portion **25**B, to allow water to drain through the backing layer **22**. The blades **20** of grass fibers are typically tufted onto the backing **22** in rows that have a regular spacing, such as rows that are spaced about 2 centimeters to about 4 centimeters apart, for example. The incorporation of the grass fibers **20** into the backing layer **22** sometimes results in a series of spaced apart, substantially parallel, urethane coated corrugations or ridges **26**B on the bottom surface **28** of the backing layer **22** formed by the grass blade tufts. Ridges **26**B can be present even where the fibers are not exposed.

The optional infill material **24** of the turf assembly **12**, when applicable, is placed in between the blades **20** of artificial grass and on top of the backing **22**. If the infill material **24** is applied, the material volume is typically an amount that covers only a bottom portion of the synthetic grass blades **20** so that the top portions of the blades stick out above the infill material **24**. The typical purpose of the optional infill material **24** is to add stability to the field, improve traction between the athlete's shoe and the play surface, and to improve shock attenuation of the field. The infill material **24** is typically sand **24**A or ground up rubber particles or synthetic particulate **24**B or mixtures of these, although other materials can be used.

When the backing layer **22** has holes **25**A or a porous section **25**B for water drainage, then some of the infill material **24** is able to wash through the backing layer porous section **25**B or the backing layer drainage holes **25**A and onto the turf underlayment layer **14**. This infill migration, or migration of the infill constituents, is undesirable because the depletion of the infill material **24** results in a field that doesn't have the initially designed stability and firmness characteristics. Excessive migration of the infill material **24**, or the infill constituent components, to the turf underlayment layer **14** can create a hard layer which makes the whole system less able to absorb impacts.

The turf underlayment layer **14** is comprised of expanded polyolefin foam beads, which can be expanded polypropylene (EPP) or expanded polyethylene (EPE), or any other suitable material. The foam beads are closed cell (water impervious) beads. In one optional method of manufacture, the beads are originally manufactured as tiny solid plastic pellets, which are later processed in a controlled pressure chamber to expand them into larger foam beads having a diameter within the range of from about 2 millimeters to about 5 millimeters. The foam beads are then blown into a closed mold under pressure so they are tightly packed. Finally, steam is used to heat the mold surface so the beads soften and melt together at the interfaces, forming the turf underlayment layer **14** as a solid material that is water impervious. Other methods of manufacture can be used, such as mixing the beads with an adhesive or glue material to form a slurry. The slurry is then molded to shape and the adhesive cured. The slurry mix underlayment may be porous through the material thickness to drain water away. This porous underlayment structure may also include other drainage feature discussed below. The final EPP material can be made in different densities by starting with a different density bead, or by any other method. The material can also

be made in various colors. The resulting underlayment structure, made by either the steam molding or the slurry mixing processes, may be formed as a water impervious underlayment or a porous underlayment. These resulting underlayment layer structures may further include any of the drainage, deflection, and interlocking features discussed below.

Alternatively, the turf underlayment layer **14** can be made from a molding and expansion of small pipe sections of foamed material, similar to small foamed macaroni. The small pipe sections of foamed material are heated and fused together in the mold in the same way as the spherical beads. The holes in the pipe sections keep the underlayment layer from being a totally solid material, and some water can drain through the underlayment layer. Additionally, varying the hollow section geometry may provide an ability to vary the material density in order to selectively adjust the performance of the turf system.

In the embodiment illustrated in FIG. **2**, the turf underlayment layer **14** is comprised of a plurality of underlayment panels **30**A, **30**B, **30**C, and **30**D. Each of the panels have similar side edges **32**A, **32**B, **32**C, and **32**D. The panels further have substantially planar major faces, i.e., top sides **34** and bottom sides **36**. The substantially flat planar faces, top sides **34** and bottom sides **36**, define a core **35** therebetween. There are flaps **37**, **38**, and fittings, indicated generally at **40**A and **40**B, are arranged along the edges **32**A-D as shown. In one embodiment shown in FIGS. **2** and **2**A, the flaps **37** and **38** are configured to include top side flaps **37**A, **38**A, **38**B and bottom side flaps **37**D, **38**C, **38**D. For reference purposes only, top side flaps **38**A and **38**B are shown in FIGS. **2** and **2**A as having a patterned surface contiguous with, the top side **34**. Likewise, FIG. **3** shows the top side flaps **37**A and **37**B of panel **30**A-D having a substantially flat surface adjacent to an upper support surface **52** that supports the backing layer **22** of the turf assembly **12**. Alternatively, the top side flaps **37**A, **37**B, **38**A and **38**B can have either a substantially flat surface adjacent to, or a patterned surface contiguous with, the top side **34**. Bottom side flaps are similarly associated with the bottom side **36** or a lower support surface **70** of the panels **30** contacting the underlying strata, such as the foundation layer **16**.

The top side flap **38**A may be of unequal length relative to the adjacent bottom side flap **38**C, as shown positioned along edge **32**B in FIGS. **2** and **2**A. Alternatively, for example, the top side flap **38**A and the bottom side flap **38**C, positioned along the edge **32**B, may be of equal length. In FIG. **2**, the panels **30**A-D further show edges **32**A and **32**C having substantially continuous top side flaps **37**A and bottom side flaps **37**D, respectively, though such a configuration is not required. The edges **32**A and **32**C may have flaps similarly configured to edges **32**B and **32**D. As shown in FIG. **3**, the top side flap **37**A may extend along the length of the edge **32**C and the bottom side flap **38**C may extend along the oppositely positioned edge **32**A.

When assembled, the flaps along edges **32**A and **32**B are configured to interlock with the mating edges **32**C and **32**D, respectively. The top side flap **38**A and adjacent bottom side flap **38**C overlap and interlock with the mating bottom side flap **38**D and top side flap **38** B, respectively. The recessed fitting **40**A of top side flap **38**B, of panel **30**D interlocks with the projecting fitting **40**B of panel **30**A, as shown in FIGS. **2** and **6**. In an alternative embodiment, the surface of the projecting fitting **40**B may extend up to include the projections **50**. In this embodiment, the mating recessed fitting **40**A of the top side flap **38**B has a corresponding void or opening to receive the projected fitting **40**B. These mating flaps **37**, **38** and fittings **40** form a vertical and horizontal interlock connection, with the flaps **38**A and **38**B being positioned along flaps **38**D and **38** C, respectively, substantially preventing relative vertical movement of one panel with respect to an adjacent connected panel. The projecting and recessed fittings **40**A and **40**B, respectively, substantially prevent horizontal shifts between adjacent panels **30** due to mechanically applied shear loads, such as, for example, from an athlete's foot or groundskeeping equipment.

In one embodiment, the vertical interlock between adjacent panels **30** is sufficient to accommodate heavy truck traffic, necessary to install infill material, without vertical separation of the adjacent panels. The adjacent top side flaps **38**A and **38**B and adjacent bottom side flaps **38**C and **38**D also substantially prevent horizontal shifting of the panels due to mechanically applied shear loads. The cooperating fittings **40**A and **40**B, along with adjacent flaps **38**A, **38**B and **38**C, **38**D, provide sufficient clearance to accommodate deflections arising from thermal expansion. The flaps **38** may optionally include drainage grooves **42**B and drainage ribs or projections **42**A that maintain a drainage channel between the mated flaps **38**A-D of adjoining panels, as will be discussed below. The drainage projections **42**A and the drainage grooves **42**B may be oriented on mated flaps of adjacent panels in an offset relative relationship, in a cooperatively engaged relationship, or applied to the mated flaps **38**A-D as either solely projections or grooves. When oriented in a cooperating engaged relationship, these projections **42**A and grooves **42**B may additionally supplement the in-plane shear stability of the mated panel assemblies **30** when engaged together. The drainage projections **42**A and drainage grooves **42**B may be equally or unequally spaced along the flaps **38**A and **38**B, respectively, as desired.

Optionally, the drainage grooves **42**B and projections **42**A can perform a second function, i.e. a retention function. The turf underlayment **30** may include the cooperating drainage ribs or projections **42**A and grooves **42**B for retention purposes, similar to the fittings **40**. The projections **42**A and fittings **40**B may include various embodiments of differently shaped raised recessed structures, such as square, rectangular, triangular, pyramidal, trapezoidal, cylindrical, frustoconical, helical and other geometric configurations that may include straight sides, tapering sides or reversed tapering sides. These geometric configurations cooperate with mating recesses, such as groove **42**B and recessed fitting **40**A having complementary geometries. The cooperating fittings, and optionally the cooperating projections and grooves, may have dimensions and tolerances that create a variety of fit relationships, such as loose fit, press fit, snap fit, and twist fit connections. The snap fit relationship may further provide an initial interference fit, that when overcome, results in a loose or line-to-line fit relationship. The twist fit relationship may include a helical surface on a conical or cylindrical projection that cooperates with a recess that may or may not include a corresponding helical surface. The press fit, snap fit, and twist fit connections may be defined as positive lock fits that prevent or substantially restrict relative horizontal movement of adjacent joined panels.

The drainage projections **42**A and grooves **42**B, either alone or in a cooperating relationship, may provide a vertically spaced apart relationship between the mating flaps **38**A-D, or a portion of the mating flaps **38**A-D, of adjoining panels to facilitate water drainage away from the top surface **34**. Additionally, the drainage projections **42**A and grooves **42**B may provide assembled panels **30** with positioning

datums to facilitate installation and accommodate thermal expansion deflections due to environmental exposure. The projections **42**A may be either located in, or offset from, the grooves **42**B. Optionally, the edges **32**A-D may only include one of the projections **42**A or the grooves **42**B in order to provide increased drainage. Not all panels may need or require projections **42**A and grooves **42**B disposed about the outer perimeter. For example, it may be desired to produce specific panels that include at least one edge designed to abut a structure that is not a mating panel, such as a curb, trim piece, sidewalk, and the like. These panels may have a suitable edge, such as a frame, flat end, rounded edge, point, and the like, to engage or abut the mating surface. For panels that mate with adjacent panels, each panel may include at least one projections along a given edge and a corresponding groove on an opposite side, positioned to interact with a mating projection to produce the required offset.

FIG. **4** illustrates an embodiment of a profile of cooperating flaps **37**A and **37**C. The profiles of flaps **38**A and **38**C include complimentary mating surfaces. The top side flap **38**A includes a leading edge bevel **44**A, a bearing shelf **44**B and a back bevel **44**C. The bottom side flap **38**C includes a leading edge bevel **46**A configured to be positioned against back bevel **44**C. Likewise, a bearing shelf **46**B is configured to contact against the bearing shelf **44**B and the back bevel **46**C is positioned against the leading edge bevel **44**A. The bearing shelves **44**B and **46**B may optionally include ribs **48** extending longitudinally along the length of the respective flaps. The ribs **48** may be a plurality of outwardly projecting ribs that cooperate with spaces between adjacent ribs of the mating flap. Alternatively, the top side flap **38**A may have outwardly projecting ribs **48** and the bottom side flap **38**C may include corresponding recesses (not shown) of a similar shape and location to cooperatively engage the ribs **38**. Additionally, drain holes **58** may extend through the flaps **38** to provide water drainage, as will be described below.

As can be seen in FIG. **4**, which illustrates two panels in an abutting relationship, the abutment of the edges of the adjacent panels defines a bottom water flow connector slot **39**A at the intersection of the abutting panels. The bottom water flow connector slot **39**A is in fluid communication with the bottom side water drainage channels **76** of each of the two abutting panels, thereby providing a path for the flow of water from the bottom side water drainage channels **76** of one panel to the bottom side water drainage channels **76** of an abutting panel. In one embodiment, the bottom water flow connector slot **39**A is in fluid communication with more than one bottom side water drainage channel **76** of each of the two abutting panels. In one embodiment, as can be seen in FIG. **4**, the water flow connector slot **39**A is substantially parallel to the edges of the panels. As shown in FIG. **5**, in one embodiment, the bottom side water drainage channels **76** of each of the two abutting panels are oriented to intersect the edges of the panel at an angle substantially transverse to the edges of the panel, and the water flow connector slot **39**A is substantially parallel to the edges of the panels. In one embodiment, there is a top water flow connector slot **39**B in fluid communication with the top side water drainage channels **56** of adjacent panels.

Referring now to FIGS. **18** and **19**, an alternative embodiment of an underlayment panel, shown generally at **200**, includes an interlocking structure to assemble individual panels to form a turf underlayment layer **250**. The panel **200** includes an interlocking edge **202** having a dovetail recess **204** and corresponding dovetail projections **206**. In a particular embodiment, the interlocking edge **202** is substantially identical on opposite sides of the underlayment panel **200**, though such is not required. Alternatively, the opposite side of panel **200** may have a differently configured interlocking structure as described in other embodiments disclosed herein. The dovetail projections **206** are each sized to comprise generally half of the dovetail recess **204** so that two abutting panels **200** can be interlocked with the dovetail of a third panel to form a turf underlayment layer, as shown in FIG. **19**. The dovetail projections **206** may alternatively be asymmetrical if desired. The panel **200** includes abutting edges **208** that are illustrated as generally straight edges. The abutting edges **208**, however, may be configured with overlapping flaps, drainage or thermal expansion projections, tongue and groove structures, or other suitable features described herein to form the turf underlayment layer. The panel **200** also includes a top surface **210** and a bottom surface (not shown) that may be configured with projections, turf carpet friction enhancing features, drainage channels, and drainage holes as also described in the various embodiments described herein.

Referring now to FIG. **19**, the turf underlayment layer **250** is comprised of a plurality of underlayment panels **200**A, **200**B, and **200**C. Though shown as three interlocked panels, it is to be understood that the underlayment layer **250** includes a sufficient number of panels to cover the desired area intended as the artificial turf surface. Each of the panels **200**A, **200**B, and **200**C are configured similarly to the panel **200** of FIG. **18**. Two panels **200**B and **200**C are aligned along their respective abutting edges **208**B and **208**C such that the dovetail projections **206**B and **206**C are generally aligned and form the male counterpart feature that is accepted into dovetail **204**A of panel **200**A.

The fit between the interlocking panels may be snug or loose and may be varied depending on climactic conditions that impact the installation. When the fit between panels **200**A, **200**B, and **200**C is generally loose of a slight clearance fit, the dovetail recess **204**A of panel **200**A may brought down onto the abutted dovetail projections **206**B and **206**C of panels **200**B and **200**C. As shown in FIG. **20**, when the panels **200**A, **200**B, and **200**C are configured with a snug or slight compression fit, a hook portion **207**A of panel **200**A may be rotated into contact with a mating hook portion **207**C of panel **200**C and pulled against the dovetail projection **206**C in order to slightly compress panels **200**B and **200**C together. In such a fit arrangement, the panels may include projections that are deformable during installation and further accommodate the effects of thermal expansion and contraction to maintain the desired relative fits of the panels, as described herein. These assembly techniques are merely illustrative and are not restricted to any particular fit arrangement but may provide ease of installation for different underlayment layer fits.

Referring now to FIG. **21**, an embodiment of an underlayment panel, shown generally at **300**, includes an interlocking edge **302**, similar to the interlocking edge **202**, described above. The panel **300** includes a dovetail recess **304** that is defined by dovetail projections **306** and hook portions **307** spaced on either side and an abutting panel edge **308** similar to those described above. An upper surface or top side **310** of the panel **300** includes a plurality of spaced-apart projections **312** that define drainage channels **314** to facilitate the flow of water across the panel **300**. The bottom side (not shown) of panel **300** may be similarly configured, if desired. Alternatively, the bottom side may include only drainage channels (not shown). Though shown as square projections having rounded corners and straight sides, the projections **312** may be any suitable geometric shape desired. The panel **300** further includes projections

316 disposed along the interlocking edge 302 that space abutting panels apart. The projections 316 may provided in any suitable number and position along the perimeter of the panel 300, as desired. When the panel 300 is connected to similar panels to form an underlayment layer and the assembled panels are spaced apart, a drainage space or passage is formed to permit water runoff to exit the topside 310 of the panel 300 and migrate to a subsurface support layer (not shown). The projections 316 may also act as crush ribs or discrete deflection points that permit relative movement of abutting panels in response to thermal conditions or load-applied deflections.

Referring now to FIG. 22, there is illustrated another embodiment of an underlayment panel, shown generally at 400. The underlayment panel 400 is similar to panel 300, described above, and includes similar features, such as an interlocking edge 402 having a dovetail recess 404 defined by dovetail projections 306 (only one is shown) and hook portions 407. The panel 400 further includes abutting edges 408 (one shown). An upper or top surface 410 of panel 400 includes projections 412 that provide support for an artificial turf carpet (not shown). The spaced-apart projections 412 define top side drainage channels 414 that provide for water flow. The top side drainage channels 414 are in fluid communication with a plurality of drain holes 418 that are sufficiently sized and spaced across the top surface 410 to facilitate water drainage to the substrate layer below. The drain holes 418 may be in fluid communication with the bottom side (not shown) that includes any of the bottom side embodiments described herein. The interlocking edge 402 of the panel 400 includes at least one projection 416, and preferably a plurality of projections 416. The projections 416 may be positioned on the dovetail projection, the dovetail recess 404, the hook portion 407, and the abutting edge 408 (not shown) if desired.

Referring to FIGS. 2, 2A, and 5, a flap assembly groove 80 is shown positioned between the top side flap 38A and the bottom side flap 38C. The flap assembly groove 80, however, may be positioned between any adjacent interlocking geometries. The groove 80 allows relative movement of adjacent flaps on an edge of a panel so that adjoining panel flaps can be assembled together more easily. When installing conventional panels, adjoining panels are typically slid over the compacted base and twisted or deflected to position the adjoining interfaces together. As the installers attempt to mate adjoining prior art panel interfaces together, they may bend and bow the entire panel structure to urge the mating sections into place. The corners and edges of these prior art panels have a tendency to dig into the compacted base causing discontinuities which is an undesirable occurrence.

In contrast to the assembly of prior art panels, the grooves 80 of the panels 30A, 30B, 30C, and 30D allow the top side flap 38A to flex relative to bottom side flap 38C. To illustrate the assembly method, panels 30A, 30B and 30D are relatively positioned in place and interlocked together on the foundation layer. To install panel 30C, the top side flap 38A of panel 30A is deflected upwardly. Additionally, the mated inside corner of panels 30A and 30 D may be slightly raised as an assembled unit. The area under the top side flap 38A of panel 30A is exposed in order to position the mating bottom side flap 38D. The bottom side flap 37D positioned along edge 32A of panel 30A may be positioned under the top side flap 37A on edge 32C of panel 30D. This positioning may be aided by slightly raising the assembled corner of panels 30A and 30D. The positioned flaps may be engaged by a downward force applied to the overlapping areas. By bending the top side flaps of a panel up during assembly, access to the mating bottom side flap location increases thus facilitating panel insertion without significant sliding of the panel across the compacted foundation layer. This assembly technique prevents excessively disrupting the substrate or the previously installed panels. The assembly of panels 30A-D, shown in FIG. 2, may also be assembled by starting with the panel 30C, positioned in the upper right corner. Subsequent top side flaps along the edges 32 may be placed over the bottom side flaps already exposed.

FIG. 2 illustrates an embodiment of assembled panels 30 where the top side flap 38A is shorter than the bottom side flap 38B, as described above, creating a flap offset. The flap offset aligns the panels 30 such that seams created by the mating edges 32 do not line up and thereby create a weak, longitudinal deflection point. The top side and bottom side flaps may be oriented in various offset arrangements along the edge 32. For example, two top side flaps of equal length may be disposed on both sides of the bottom side flap along the edge 32. This arrangement would allow the seam of two adjoining panels to terminate in the center of the next panel.

FIGS. 7 and 8 illustrate an alternative embodiment of the underlayment panels 130, having a plurality of edges 132, a top side 134, a bottom side 136, and flaps configured as tongue and groove structures. The flaps include upper and lower flanges 142, 144 extending from some of the edges 132 of the panels 130, with the upper and lower flanges 142, 144 defining slots 146 extending along the edges 132. An intermediate flange 148 extends from the remainder of the edges of the panels, with the intermediate flange 148 being configured to fit within the slots 146 in a tongue-and-groove configuration. The flanges 148 of one panel 130 fit together in a complementary fashion with the slot 146 defined by the flanges 142, 144 of an adjacent panel. The purpose of the flanges 142, 144, and 148 is to secure the panels against vertical movement relative to each other. When the panels 130 are used in combination with a turf assembly 12, i.e., as an underlayment for the turf assembly, the application of a downward force applied to the turf assembly pinches the upper and lower flanges 142, 144 together, thereby compressing the intermediate flanges 148 between the upper and lower flanges, and preventing or substantially reducing relative vertical movement between adjacent panels 130. The top side 134 may include a textured surface having a profile that is rougher or contoured beyond that produced by conventional smooth surfaced molds and molding techniques, which are known in the art.

FIGS. 1-3 further show a plurality of projections 50 are positioned over the top side 34 of the panels 30. The projections 50 have truncated tops 64 that form a plane that defines an upper support surface 52 configured to support the artificial turf assembly 12. The projections 50 do not necessarily require flat, truncated tops. The projections 50 may be of any desired cross sectional geometric shape, such as square, rectangular, triangular, circular, oval, or any other suitable polygon structure. The projections 50, as shown in FIG. 10, and projections 150 as shown in FIGS. 11 and 12, may have tapered sides 54, 154 extending from the upper support surface 52, 152 outwardly to the top side 34 of the core 35. The projections 50 may be positioned in a staggered arrangement, as shown in FIGS. 2, 6, and 9. The projections 50 may be any height desired, but in one embodiment the projections 50 are in the range of about 0.5 millimeters to about 6 millimeters, and may be further constructed with a height of about 3 millimeters. In another embodiment, the height is in the range of about 1.5 millimeters to about 4 millimeters. The tapered sides 54 of adjacent projections 50 cooperate to define channels 56 that form a labyrinth across

the panel **30** to provide lateral drainage of water that migrates down from the turf assembly **12**. The channels **56** have drain holes **58** spaced apart and extending through the thickness of the panel **30**.

As shown in FIG. **9**, the channels **56** may be formed such that the tapered sides **54** substantially intersect or meet at various locations in a blended radii relationship transitioning onto the top surface **34**. The projections **50**, shown as truncated cone-shaped structures having tapered sides **54**, form a narrowed part, or an infill trap **60**, in the channel **56**. The infill trap **60** blocks free flow of infill material **24** that migrates through the porous backing layer **22**, along with water. As shown in FIGS. **9** and **10**, the infill material **24** becomes trapped and retained between the tapered sides **54** in the channels **56**. The trapping of the infill material **24** prevents excessive migrating infill from entering the drain holes **58**. The trapped infill material may constrict or somewhat fill up the channels **56** but does not substantially prevent water flow due to interstitial voids created by adjacent infill particles, **24**A and **24**B, forming a porous filter.

The size of the drainage holes **58**, the frequency of the drainage holes **58**, the size of the drainage channels **56** on the top side **34** or the channels **76** on the bottom side **36**, and the frequency of the channels **56** and **76** provide a design where the channels can line up to create a free flowing drainage system. In one embodiment, the system can accommodate up to 70 mm/hr rainfall, when installed on field having a slightly-raised center profile, for example, on the order of a 0.5% slope. The slightly-raised center profile of the field tapers, or slopes away, downwardly towards the perimeter. This format of installation on a full sized field promotes improved horizontal drainage water flow. For instance, a horizontal drainage distance of 35 meters and a perimeter head pressure of 175 millimeters.

The cone shaped projections **50** of FIGS. **6** and **9** also form widened points in the channel **56**. The widened points, when oriented on the edge **32** of the panel **30**, form beveled, funnel-like interfaces or edges **62**, as shown in FIG. **6**. These funnel edges **62** may be aligned with similar funnel edges on adjacent panels and provide a greater degree of installation tolerance between mating panel edges to create a continuous channel **56** for water drainage. If the top side projections **50** have a non-curved geometry, the outer edge corners of the projections **50** may be removed to form the beveled funnel edge, as will be discussed below in conjunction with bottom side projections. Additionally, the bottom side projections may be generally circular in shape and exhibit a similar spaced apart relationship as that described above. The bottom side projections may further be of a larger size than the top side projections.

A portion of the bottom side **36** of the panel **30** is shown in FIGS. **5** and **13**. The bottom side **36** includes the lower support surface **70** defined by a plurality of downwardly extending projections **72** and a plurality downwardly extending edge projections **74**. The plurality of projections **72** and edge projections **74** space apart the bottom side **36** of the panel **30** from the foundation layer **16** and further cooperate to define drainage channels **76** to facilitate water flow beneath the panel. The edge projections **74** cooperate to form a funnel edge **78** at the end of the drainage channel **76**. These funnel edges **78** may be aligned with similar funnel edges **78** on adjacent panels and provide a greater degree of installation tolerance between mating panel edges to create a continuous channel **76** for water drainage. The bottom side **36** shown in FIG. **13** represents a section from the center of the panel **30**. The bottom side projections **72** and edge projections **74** are typically larger in surface area than the top side projections **50** and are shallower, or protrude to a lesser extent, though other relationships may be used. The larger surface area and shorter height of the bottom side projections **72** tends to allow the top side projections **50** to deform more under load. Alternatively, the bottom side projections may be generally circular in shape and exhibit a similar spaced apart relationship as that described above. The bottom side projections may further be of a larger size than the top side projections.

The larger size of the bottom side projections **72** allows them to be optionally spaced in a different arrangement relative to the arrangement of the top side projections **50**. Such a non-aligned relative relationship assures that the top channels **56** and bottom channels **76** are not aligned with each other along a relatively substantial length that would create seams or bending points where the panel core **35** may unduly deflect.

Referring again to FIG. **9**, the top side projections **50** may include a friction enhancing surface **66** on the truncated tops **64**. The friction enhancing surface **66** may be in the form of bumps, or raised nibs or dots, shown generally at **66**A in FIG. **9**. These bumps **66**A provide an increased frictional engagement between the backing layer **22** and the upper support surface of the underlayment panel **30**. The bumps **66**A are shown as integrally molded protrusions extending up from the truncated tops **64** of the projections **50**. The bumps **66**A may be in a pattern or randomly oriented. The bumps **66**A may alternatively be configured as friction ribs **66**B. The ribs **66**B may either be on the surface of the truncated tops **64** or slightly recessed and encircled with a rim **68**.

FIGS. **11** and **12** illustrate alternative embodiments of various turf underlayment panel sections having friction enhancing and infill trapping surface configurations. A turf underlayment panel **150** includes a top side **152** of the panel **150** provided with plurality of spaced apart, upwardly oriented projections **154** that define flow channels **156** suitable for the flow of water along the top surface of the panel. The projections **154** are shown as having a truncated pyramid shape, however, any suitable shape, such as for example, truncated cones, chevrons, diamonds, squares and the like can be used. The projections **154** have substantially flat upper support surfaces **158** which support the backing layer **22** of the artificial turf assembly **12**. The upper support surfaces **158** of the projections **154** can have a generally square shape when viewed from above, or an elongated rectangular shape as shown in FIGS. **11** and **12**, or any other suitable shape.

The frictional characteristics of the underlayment may further be improved by the addition of a medium, such as a grit **170** or other granular material, to the underlayment mixture, as shown in FIGS. **12**A and **12**B. In an embodiment shown in FIG. **12**A, the granular medium is added to the adhesive or glue binder and mixed together with the beads. The grit **170** may be in the form of a commercial grit material, typically provided for non-skid applications, often times associated with stairs, steps, or wet surfaces. The grit may be a polypropylene or other suitable polymer, or may be silicon oxide (SiO_2), aluminum oxide (Al_2O_3), sand, or the like. The grit **172** however may be of any size, shape, material or configuration that creates an associated increased frictional engagement between the backing layer **22** and the underlayment **150**. In operation, the application of grit material **172** to the underlayment layer **14** will operate in a different manner from operation of grit applied to a hard surface, such as pavement or wood. When applied to a hard

surface, the non-skid benefit of grit in an application, such as grit filled paint, is realized when shearing loads are applied directly to the grit structure by feet, shoes, or vehicle wheels. Further, grit materials are not applied under a floor covering, such as a rug or carpet runner, in order to prevent movement relative to the underlying floor. Rather, non-skid floor coverings are made of soft rubber or synthetic materials that provide a high shear resistance over a hard flooring surface.

The grit material **170** when applied to the binder agent in the turf underlayment structure provides a positive grip to the turf backing layer **22**. This gripping of the backing layer benefits from the additional weight of the infill medium dispersed over the surface, thus applying the necessary normal force associated with the desired frictional, shear-restraining force. Any concentrated deflection of the underlayment as a result of a load applied to the turf will result in a slight momentary "divot" or discontinuity that will change the frictional shear path in the underlayment layer **14**. This deflection of the surface topography does not occur on a hard surface, such as a painted floor using grit materials. Therefore, the grit material, as well as the grit binder are structured to accommodate the greater elasticity of the underlayment layer, as opposed toe the hard floor surface, to provide improved surface friction. A grit material **180** may alternatively be applied to the top of the bead and binder mixture, as shown in FIG. **12**B, such that the beads within the thickness exhibit little to no grit material **180**. In this instance, the grit material **180** would primarily be on top of and impregnated within the top surface and nearby thickness of the underlayment **150**. Alternatively, the grit material **180** may be sprinkled onto or applied to the mold surface prior to applying the bead and binder slurry so that the predominant grit content is on the top of the underlayment surface after the product is molded.

Another embodiment provides a high friction substrate, such as a grit or granular impregnated fabric applied to and bonded with the upper surface of the underlayment layer **14**, i.e. the top side **34** or the upper support surface **52** as defined by the projections **50**. The fabric may alternatively be a mesh structure whereby the voids or mesh apertures provide the desired surface roughness or high friction characteristic. The mesh may also have a roughened surface characteristic, in addition to the voids, to provide a beneficial gripping action to the underlayment. The fabric may provide an additional load spreading function that may be beneficial to protecting players from impact injury. Also the fabric layer may spread the load transfer from the turf to the underlayment and assist in preserving the base compaction characteristic.

FIG. **17** illustrates an alternative embodiment of an underlayment layer having a water drainage structure and turf assembly frictional engagement surface. The underlayment layer **200** includes a top side **210** configured to support the artificial turf assembly **12**. The underlayment layer **200** further includes a core **235**, a top side **210** and a bottom side **220**. The top side **210** includes a plurality of spaced apart projections **230** that define channels **240** configured to allow water flow along the top side **210**. The top side **210** includes a series of horizontally spaced apart friction members **250** that are configured to interact with the downwardly oriented ridges **26** on the bottom surface **28** of the backing layer **22** of the artificial turf assembly **12**. The friction members **250** engage the ridges **26** so that when the artificial turf assembly **12** is laid on top of the underlayment layer **200** relative horizontal movement between the artificial turf assembly **12** and the underlayment layer **200** is inhibited.

In order to facilitate drainage and infill trapping, the channels **156**A defined by the projections **152** optionally can have a V-shaped cross-sectional shape as shown in FIG. **11**, with walls that are at an acute angle to the vertical. The flow channels **156**B shown in FIG. **12** are slightly different from flow channels **156**A since they have a flattened or truncated V-shaped cross-sectional shape rather than the true V-shaped cross-section of channels **156**A. The purpose of the flow channels **156**A and **156**B is to allow water to flow along the top side **152** of the panels **150**. Rain water on the turf assembly **12** percolates through the infill material **24** and passes though the backing layer **22**. The flow channels **156**A, and **156**B allow this rain water to drain away from the turf system **10**. As the rain water flows across the top side **152** of the panel **150**, the channels **156**A and **156**B will eventually direct the rainwater to a vertical drain hole **160**. The drain holes **160** then allow the rain water to drain from the top side **152** to the bottom side of the turf underlayment layer **14**. The drain hole **160** can be molded into the panel, or can be mechanically added after the panel is formed.

During the operation of the artificial turf system **10**, typically some of the particles of the infill material **24** pass through the backing layer **22**. These particles can flow with the rain water along the channels **156**A and **156**B to the drain holes **160**. The particles can also migrate across the top surface **152** in dry conditions due to vibration from normal play on the turf system **10**. Over time, the drain holes **160** can become clogged with the sand particles and become unable to drain the water from the top surface **152** to the bottom surface. Therefore it is advantageous to configure the top surface **152** to impede the flow of sand particles within the channels **156**A, **156**B. Any suitable mechanism for impeding the flow of infill particles along the channels can be used.

In one embodiment, as shown in FIG. **11**, the channel **156**A contains dams **162** to impede the flow of infill particles. The dams **162** can be molded into the structure of the turf underlayment layer **14**, or can be added in any suitable manner. The dams **162** can be of the same material as the turf underlayment layer, or of a different material. In another embodiment, the flow channels **156**A are provided with roughened surfaces **164** on the channel sidewalls **166** to impede the flow of infill particles. The roughened surface traps the sand particles or at least slows them down.

FIGS. **14-16** illustrate the dynamic load absorption characteristics of projections, shown in conjunction with the truncated cone projections **50** of the underlayment **30**. The projections **50** on the top side provide a dynamic response to surface impacts and other load inputs during normal play on athletic fields. The truncated geometric shapes of the protrusions **50** provide the correct dynamic response to foot and body impacts along with ball bounce characteristics. The tapered sides **54** of the projections **50** incorporate some amount of taper or "draft angle" from the top side **34**, at the base of the projection **50**, to the plane of the upper support surface **52**, which is substantially coplanar with the truncated protrusion top. Thus, the base of the projection **50** defines a somewhat larger surface area than the truncated top surface area. The drainage channels **56** are defined by the tapered sides **54** of adjacent projections **50** and thereby establish gaps or spaces therebetween.

FIG. **14** illustrates the free state distance **90** of the projection **50** and the free state distance **92** of the core **35**. The projections **50** deflect when subjected to an axially applied compressive load, as shown in FIG. **15**. The projection **50** is deflected from the projection free state **90** to a partial load deflection distance **94**. The core **35** is still

substantially at or near a free state distance **92**. The channels **56** allow the projections to deflect outwardly as an axial load is applied in a generally downward direction. The relatively unconstrained deflection allows the protrusions **50** to "squash" or compress vertically and expand laterally under the compressive load or impact force, as shown in FIG. **15**. This relatively unconstrained deflection may cause the apparent spring rate of the underlayment layer **14** to remain either substantially constant throughout the projection deflection or increase at a first rate of spring rate increase.

Continued deformation of the protrusions **50** under a compressive or impact load, as shown in FIG. **16**, causes the projections **50** to deform a maximum amount to a fully compressed distance **96** and then begin to deform the core **35**. The core **35** deforms to a core compression distance **98** which is smaller than the core free state distance **92**. As the core **35** deforms, the apparent spring rate increases at a second rate, which is higher than the first rate of spring rate increase. This rate increase change produces a stiffening effect as a compressively-loaded elastomer spring. The overall effect also provides an underlayment behavior similar to that of a dual density material. In one embodiment, the material density range is between 45 grams per liter and 70 grams per liter. In another embodiment, the range is 50 grams per liter to 60 grams per liter. Under lower compression or impact loads, the projections **50** compress and the underlayment **30** has a relatively low reaction force for a relatively large deflection, thus producing a relatively low hardness. As the compression or impact force increases, the material underlying the geometric shape, i.e. the material of the core, creates a larger reaction force without much additional deformation, which in turn increases the stiffness level to the user.

The ability to tailor the load reactions of the underlayment and the turf assembly as a complete artificial turf system allows adjustment of two competing design parameters, a bodily impact characteristic and an athletic response characteristic. The bodily impact characteristic relates to the turf system's ability to absorb energy created by player impacts with the ground, such as, but not limited to, for example tackles common in American-style football and rugby. The bodily impact characteristic is measured using standardized testing procedures, such as for example ASTM-F355 in the U.S. and EN-1177 in Europe. Turf systems having softer or more impact absorptive responses protect better against head injury, but offer diminished or non-optimized athlete and ball performance. The athletic response characteristic relates to athlete performance responses during running and can be measured using a simulated athlete profile, such as the Berlin Artificial Athlete. Athlete performance responses include such factors as turf response to running loads, such as heel and forefoot contact and the resulting load transference. The turf response to these running load characteristics can affect player performance and fatigue. Turf systems having stiffer surface characteristics may increase player performance, such as running load transference, (i.e. shock absorption, surface deformation and energy restitution), and ball behavior, but also increase injury potential due to lower impact absorption. The underlayment layer and the turf assembly each has an associated energy absorption characteristic, and these are balanced to provide a system response appropriate for the turf system usage and for meeting the required bodily impact characteristics and athletic response characteristics.

In order to accommodate the particular player needs, as well as satisfying particular sport rules and requirements, several design parameters of the artificial turf system may need to be varied. The particular sport, or range of sports and activities undertaken on a particular artificial turf system, will dictate the overall energy absorption level required of the system. The energy absorption characteristic of the underlayment layer may be influenced by changes in the material density, protrusion geometry and size, panel thickness and surface configuration. These parameters may further be categorized under a broader panel material factor and a panel geometry factor of the underlayment layer. The energy absorption characteristic of the turf assembly may be subject to considerations of infill material and depth. The infill material comprises a mixture of sand and synthetic particulate in a ratio to provide proper synthetic grass blade exposure, water drainage, stability, and energy absorption.

The turf assembly **12** provides a lot of the impact shock attenuation for safety for such contact sports as American football. The turf assembly **12** also provides the feel of the field when running, as well as ball bounce and roll in sports such as soccer (football), field hockey, rugby and golf. The turf assembly **12** and the turf underlayment layer **14** work together to get the right balance for hardness in running, softness (impact absorption or energy absorption) in falls, ball bounce and roll, etc. To counteract the changing field characteristics over time, which affect ball bounce and the roll and feel of the field to the running athlete, in some cases the infill material may be maintained or supplemented by adding more infill, and by using a raking machine or other mechanism to fluff up the infill so it maintains the proper feel and impact absorption.

The hardness of the athletic field affects performance on the field, with hard fields allowing athletes to run faster and turn more quickly. This can be measured, for example in the United States using ASTM F1976 test protocol, and in the rest of the world by FIFA, IRB (International Rugby Board), FIH (International Hockey Federation), and ITF (International Tennis Federation) test standards. In the United States, another characteristic of the resilient turf underlayment layer **14** is to provide increased shock attenuation of the infill turf system by up to 20 percent during running heel and running forefoot loads. A larger amount of attenuation may cause athletes to become too fatigued, and not perform at their best. It is generally accepted that an athlete cannot perceive a difference in stiffness of plus or minus 20 percent deviations over a natural turf stiffness at running loads based on the U.S. tests. The FIFA test requirement has minimum and maximum values for shock attenuation and deformation under running loads for the complete turf/underlayment system. Artificial turf systems with shock attenuation and deformation values between the minimum and maximum values simulate natural turf feel.

The softness for impact absorption of an athletic field to protect the players during falls or other impacts is a design consideration, particularly in the United States. Softness of an athletic field protects the players during falls or other impacts. Impact energy absorption is measured in the United States using ASTM F355-A, which gives a rating expressed as Gmax (maximum acceleration in impact) and HIC (head injury criterion). The head injury criterion (HIC) is used internationally. There may be specific imposed requirements for max acceleration and HIC for athletic fields, playgrounds and similar facilities.

The turf assembly is advantageous in that in one embodiment it is somewhat slow to recover shape when deformed in compression. This is beneficial because when an athlete runs on a field and deforms it locally under the shoe, it is undesirable if the play surface recovers so quickly that it "pushes back" on the shoe as it lifts off the surface. This

would provide unwanted energy restoration to the shoe. By making the turf assembly **12** have the proper recovery, the field will feel more like natural turf which doesn't have much resilience. The turf assembly **12** can be engineered to provide the proper material properties to result in the beneficial limits on recovery values. The turf assembly can be designed to compliment specific turf designs for the optimum product properties.

The design of the overall artificial turf system **10** will establish the deflection under running loads, the impact absorption under impact loads, and shape of the deceleration curve for the impact event, and the ball bounce performance and the ball roll performance. These characteristics can be designed for use over time as the field ages, and the infill becomes more compacted which makes the turf layer stiffer.

The panels **30** are designed with optimum panel bending characteristics. The whole panel shape is engineered to provide stiffness in bending so the panel doesn't bend too much when driving over it with a vehicle while the panel is lying on the ground. This also assists in spreading the vehicle load over a large area of the substrate so the contour of the underlying foundation layer **16** won't be disturbed. If the contour of the foundation layer **16** is not maintained, then water will pool in areas of the field instead of draining properly.

In one embodiment of the invention, an artificial turf system for a soccer field is provided. First, performance design parameters, related to a system energy absorption level for the entire artificial turf system, are determined for the soccer field. These performance design parameters are consistent according to the FIFA (Fédération Internationale de Football Association) Quality Concept for Artificial Turf, the International Artificial Turf Standard (IATS) and the European EN15330 Standard. Typical shock, or energy, absorption and deformation levels from foot impacts for such systems are within the range of 55-70% shock absorption and about 4 millimeters to about 9 millimeters deformation, when tested with the Berlin Artificial Athlete (EN14808, EN14809). Vertical ball rebound is about 60 centimeters to about 100 centimeters (EN 12235), Angled Ball Behavior is 45-70%, Vertical Permeability is greater than 180 mm/hr (EN 12616) along with other standards, such as for example energy restitution. Other performance criteria may not be directly affected by the underlayment performance, but are affected by the overall turf system design. The overall turf system design, including the interactions of the underlayment may include surface interaction such as rotational resistance, ball bounce, slip resistance, and the like. In this example where a soccer field is being designed, a performance level for the entire artificial turf system for a specific standard is selected. Next, the artificial turf assembly is designed. The underlayment performance characteristics selected will be complimentary to the turf assembly performance characteristics to provide the overall desired system response to meet the desired sports performance standard. It is understood that the steps in the above example may be performed in a different order to produce the desired system response.

In general, the design of the turf system having complimentary underlayment and turf assembly performance characteristics may for example provide a turf assembly that has a low amount of shock absorption, and an underlayment layer that has a high amount of shock absorption. In establishing the relative complimentary performance characteristics, there are many options available for the turf design such as pile height, tufted density, yarn type, yarn quality, infill depth, infill types, backing and coating. For example, one option would be to select a low depth and/or altered ratio of sand vs. rubber infill, or the use of an alternative infill material in the turf assembly. If in this example the performance of the turf assembly has a relatively low specific shock absorption value, the shock absorption of the underlayment layer will have a relatively high specific value.

By way of another example having different system characteristics, an artificial turf system for American football or rugby may provide a turf assembly that has a high amount of energy absorption, while providing the underlayment layer with a low energy absorption performance. In establishing the relative complimentary energy absorption characteristics, selecting a high depth of infill material in the turf assembly may be considered. Additionally, where the energy absorption of the turf assembly has a value greater than a specific value, the energy absorption of the underlayment layer will have a value less than the specific value.

The principle and mode of operation of this invention have been explained and illustrated in its preferred embodiment. However, it must be understood that this invention may be practiced otherwise than as specifically explained and illustrated without departing from its spirit or scope.

What is claimed is:

1. A turf underlayment layer comprised of an assembly of panels, the panels including a top side having a plurality of projections, a bottom side, and panel edges, the plurality of top side projections forming top side channels that extend across the top side of the panel to allow drainage of fluid across the top side of the panel, and the bottom side having bottom side channels that extend across the bottom side of the panel to allow drainage of fluid across the bottom side of the panel, the panel edges within the turf underlayment layer abutting edges of adjacent panels, the panels further including a plurality of drain holes positioned through the panel to allow fluid to flow from the top side of the panel to the bottom side of the panel, where the panels are made from a plurality of polyolefin beads, the plurality of polyolefin beads bonded together by at least one of pressure and heat to produce a substantially water-impervious surface.

2. The turf underlayment layer of claim **1** in which at least some of the drain holes intersect both a top side channel and a bottom side channel.

3. The turf underlayment layer of claim **1** in which the bottom drainage channels are defined by bottom projections protruding downwardly.

4. A turf underlayment layer comprised of an assembly of panels, the panels including a core having top and bottom surfaces, a plurality of top side projections that extend upwardly above the top surface of the core, the plurality of top side projections forming top side channels that extend across the top surface of the panel, the panels also having bottom side channels that are shaped to allow drainage of fluid across the bottom side of the panel, the panels also including panel edges that are abutting edges of adjacent panels, the panels further including a plurality of drain holes positioned through the panel to allow fluid to flow from the top surface of the panel to the bottom surface of the panel, at least some of the drain holes intersecting the bottom side channels, where the panels are made from a plurality of polyolefin beads, the plurality of polyolefin beads bonded together by at least one of pressure and heat to produce a substantially water-impervious surface.

5. The turf underlayment layer of claim **4** in which at least some of the drain holes intersect both a top side channel and a bottom side channel.

6. The turf underlayment layer of claim 4 in which the bottom drainage channels are defined by bottom projections protruding downwardly.

7. A turf underlayment layer comprised of an assembly of panels, the panels including a core having top and bottom surfaces, the top surface including a plurality of top side channels arranged on the top surface of the panel, and bottom side channels arranged on the bottom surface of the panel, the panels further including panel edges that are abutting edges of adjacent panels, the panels further including a plurality of drain holes positioned through the panel to allow fluid to flow from the top surface of the panel to the bottom surface of the panel, wherein upper ends of at least some of the drain holes are located adjacent to the top side channels to allow direct fluid communication between the top side channels and the drain holes, where the panels are made from a plurality of polyolefin beads, the plurality of polyolefin beads bonded together by at least one of pressure and heat to produce a substantially water-impervious surface.

8. The turf underlayment layer of claim 7 in which at least some of the drain holes intersect both a top side channel and a bottom side channel.

9. The turf underlayment layer of claim 7 in which the bottom drainage channels are defined by bottom projections protruding downwardly.

10. The turf underlayment layer of claim 7 in which the material density is within the range of from about 45 grams per liter to about 70 grams per liter.

11. The turf underlayment layer of claim 7 in which the top projections have a friction enhancing surface configured as one of bumps, raised nibs, ribs, and dots.

12. The turf underlayment layer of claim 7 in which the top projections are substantially square shaped.

* * * * *