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(54) **APPARATUS AND METHOD FOR PHASE
LOCK LOOP GAIN CONTROL USING UNIT
CURRENT SOURCES**

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(21) Appl. No.: **11/095,117**

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(57) **ABSTRACT**

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6,838,947, which is a continuation of application No.
09/811,611, filed on Mar. 20, 2001, now Pat. No.
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327/157; 375/374

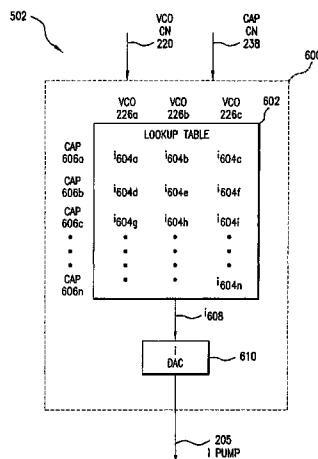
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20 Claims, 13 Drawing Sheets



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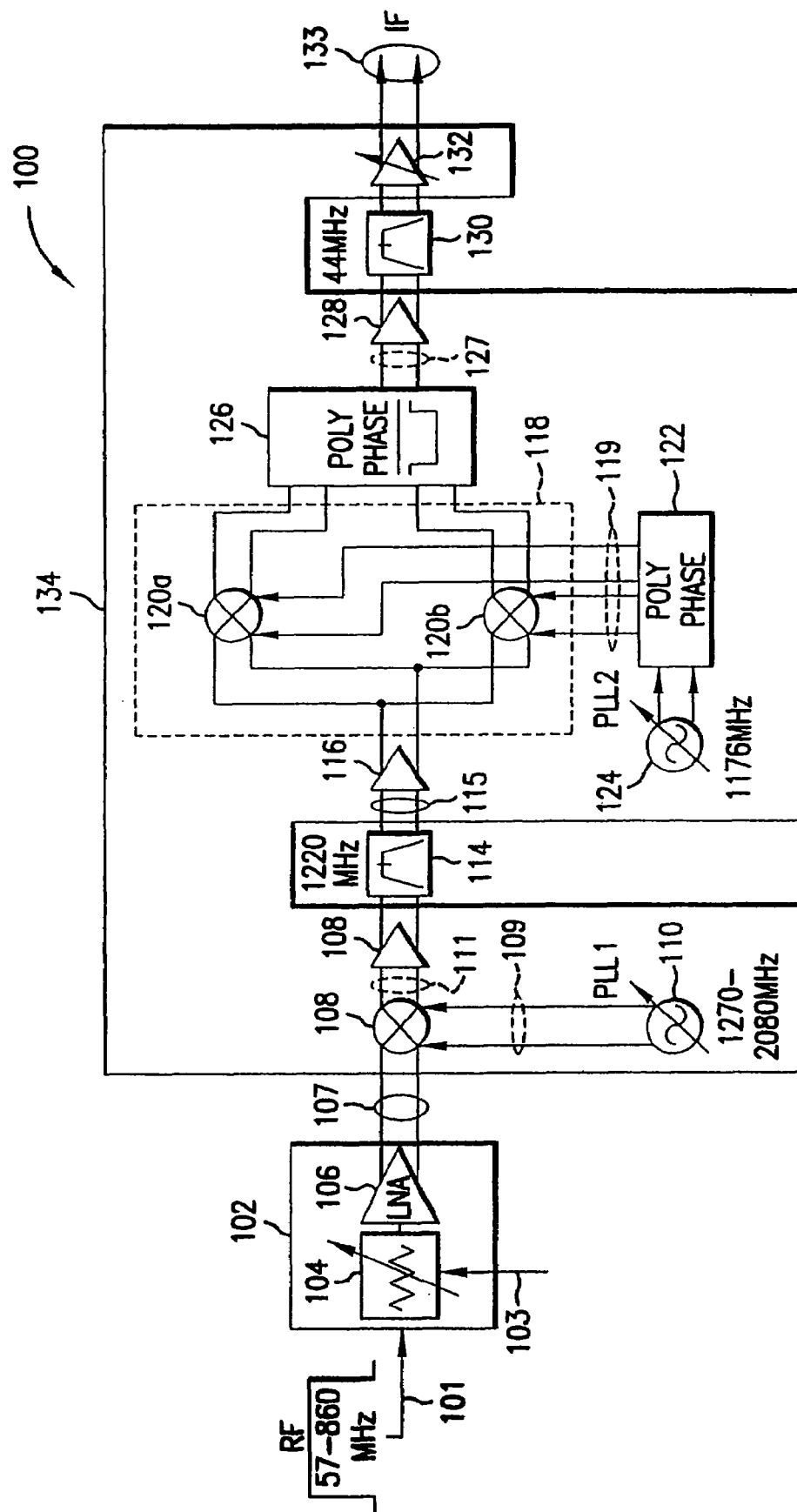


FIG. 1A

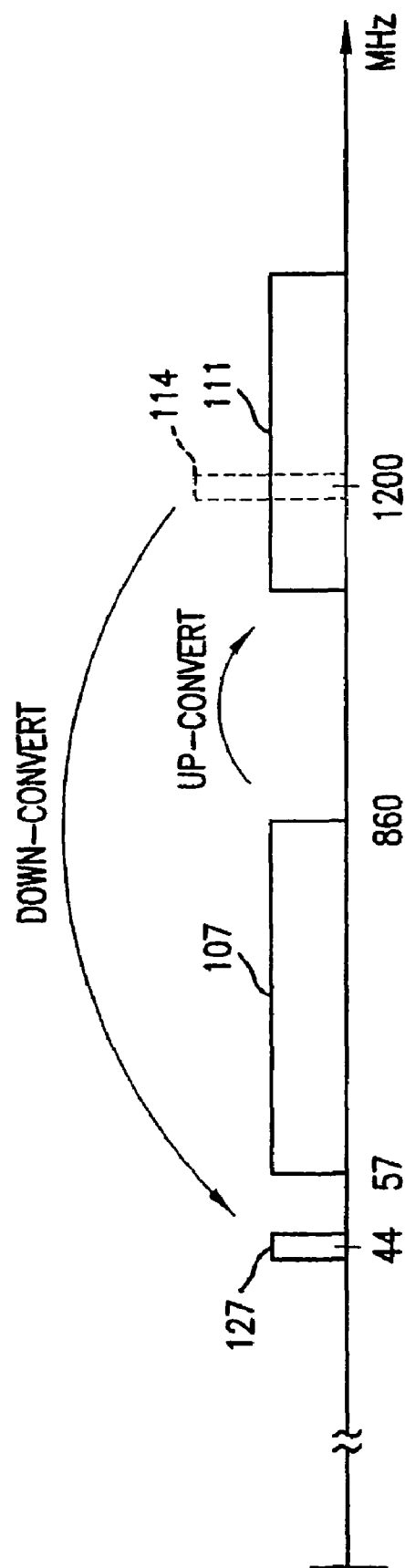


FIG. 1B

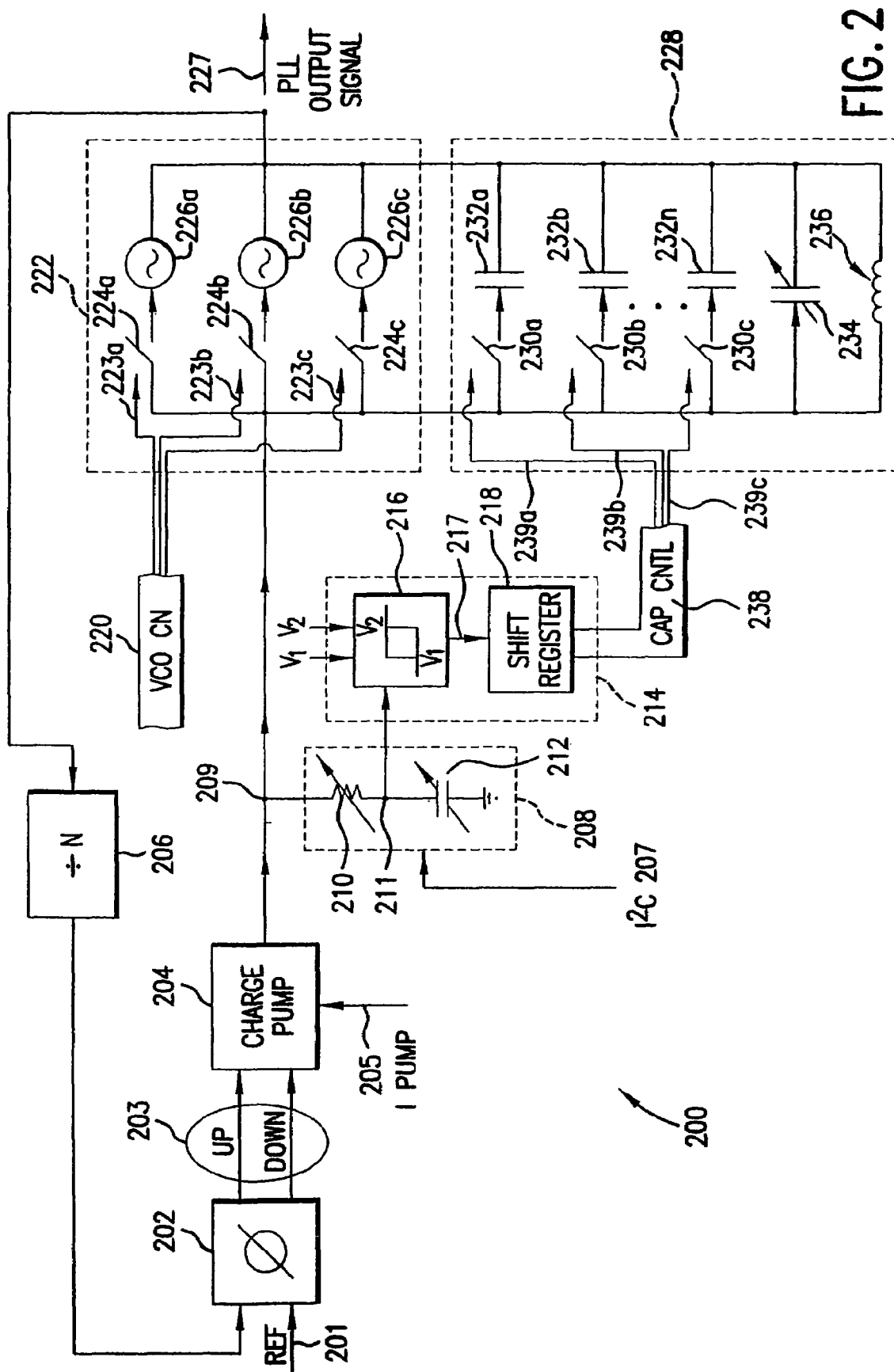


FIG. 2

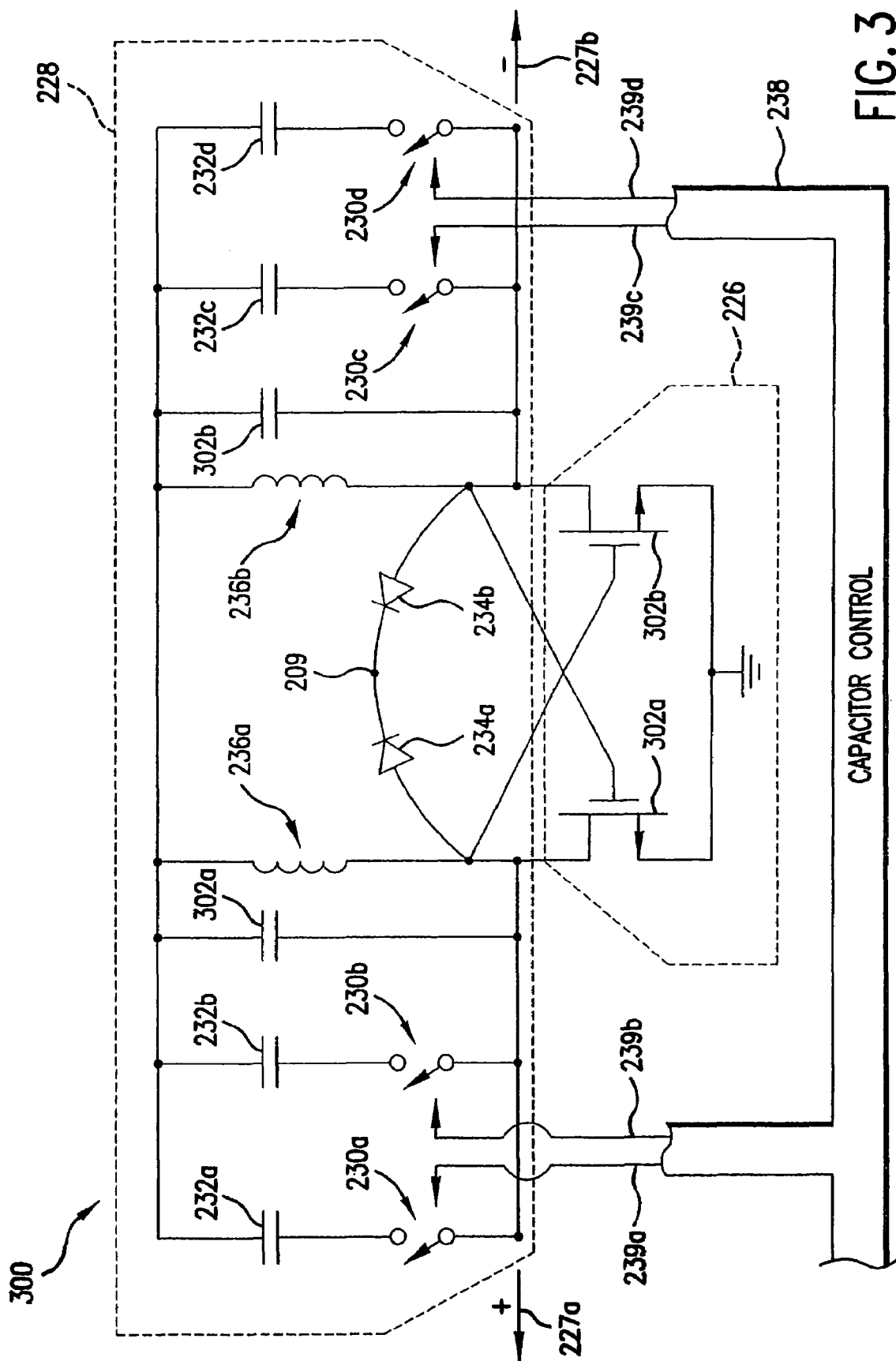


FIG. 3

CAPACITOR CONTROL

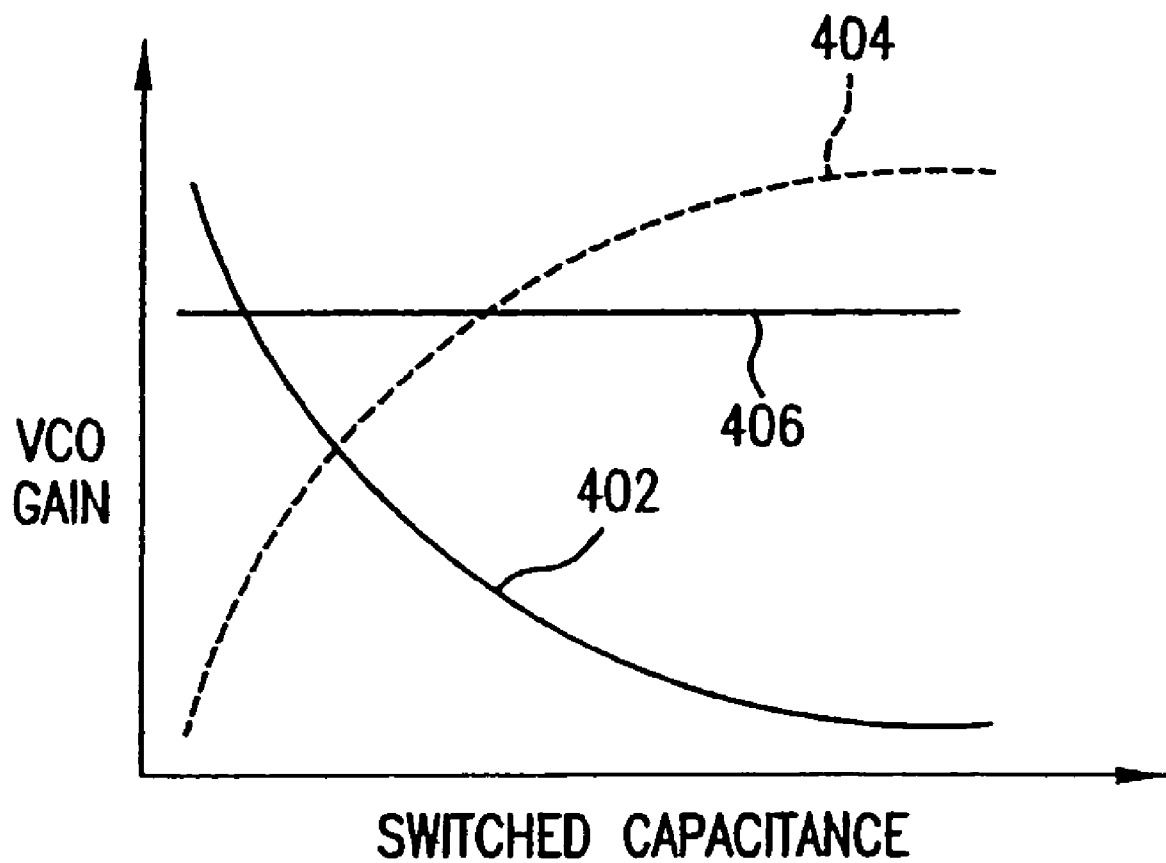


FIG. 4

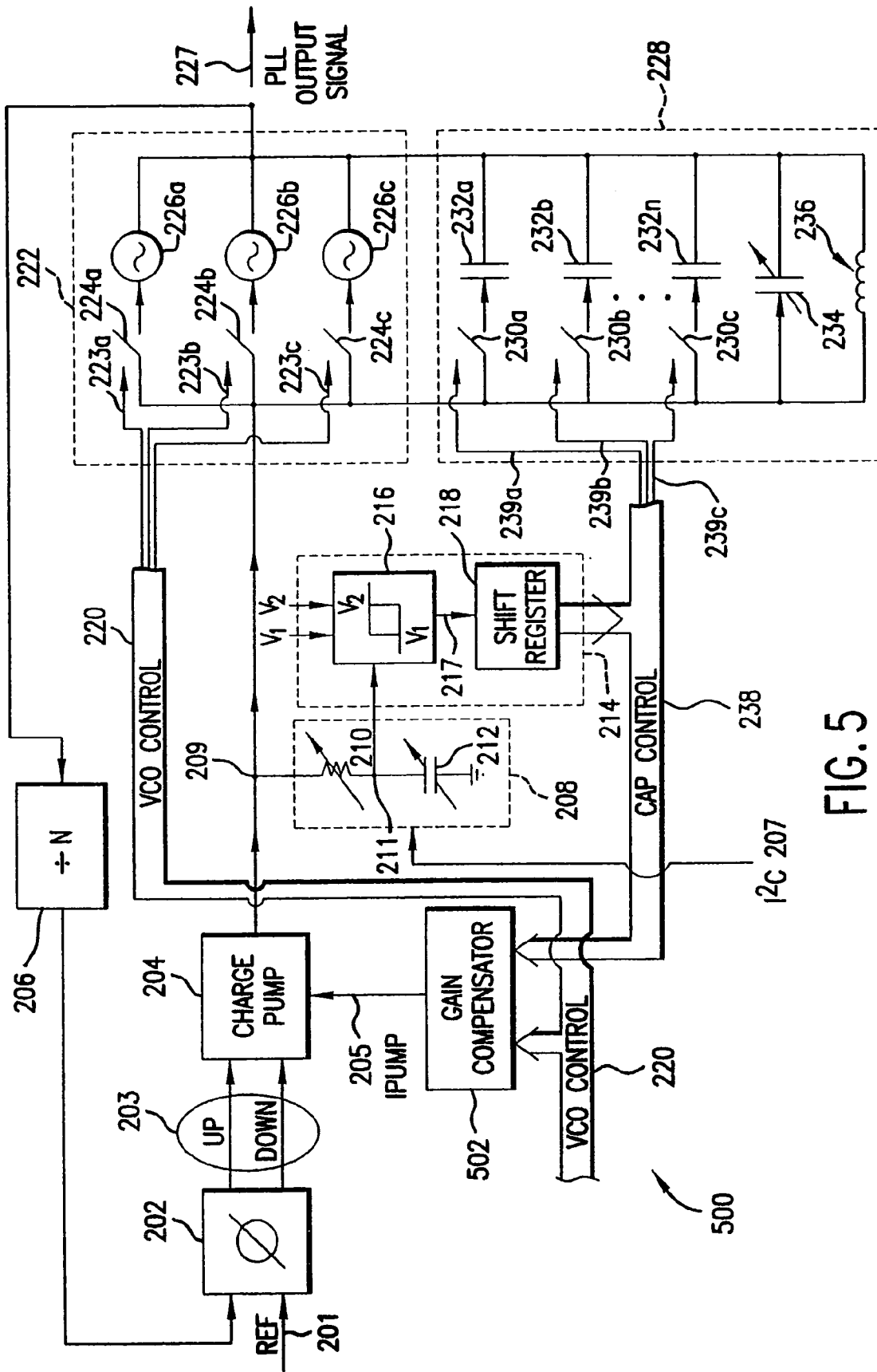


FIG. 5

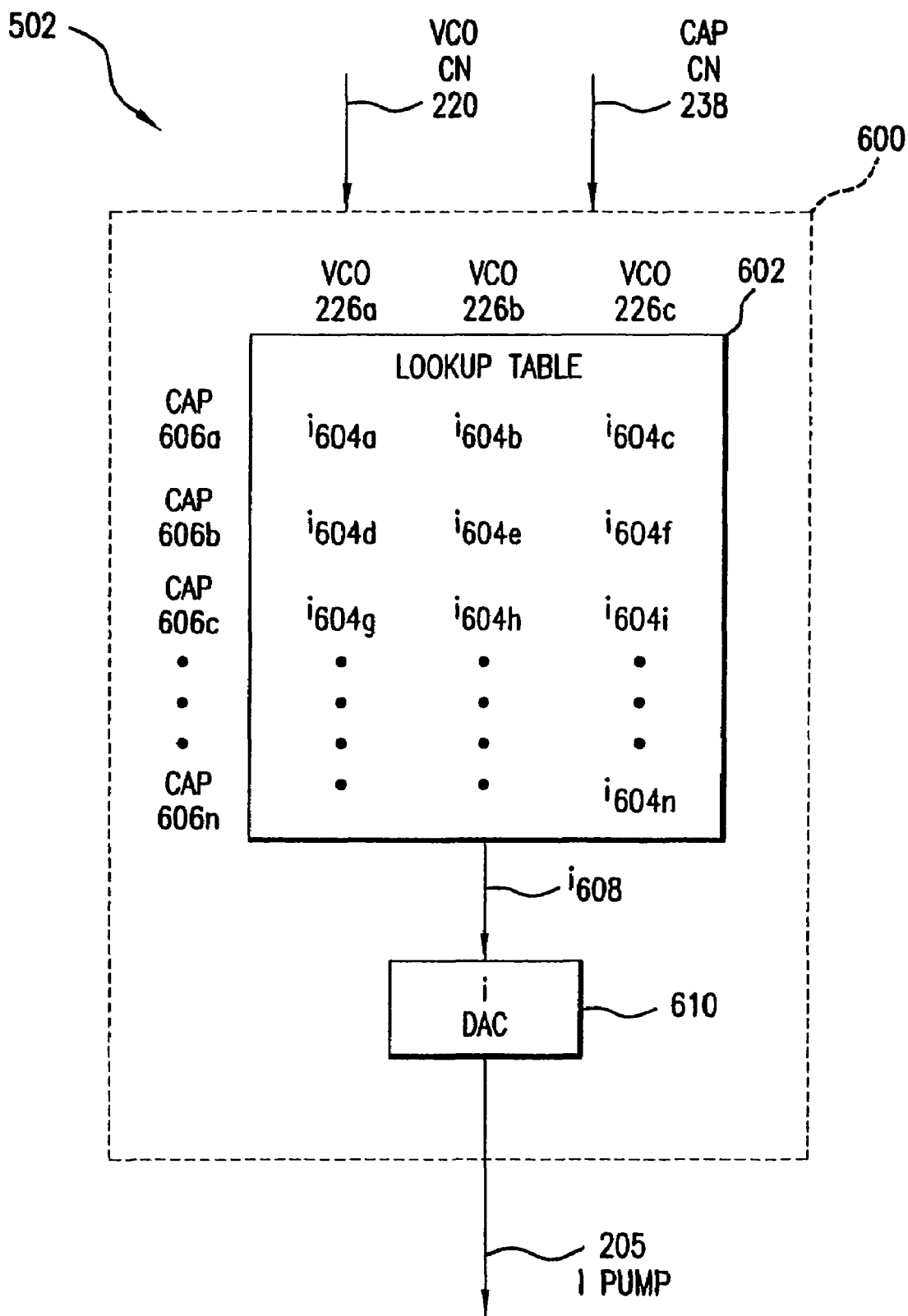
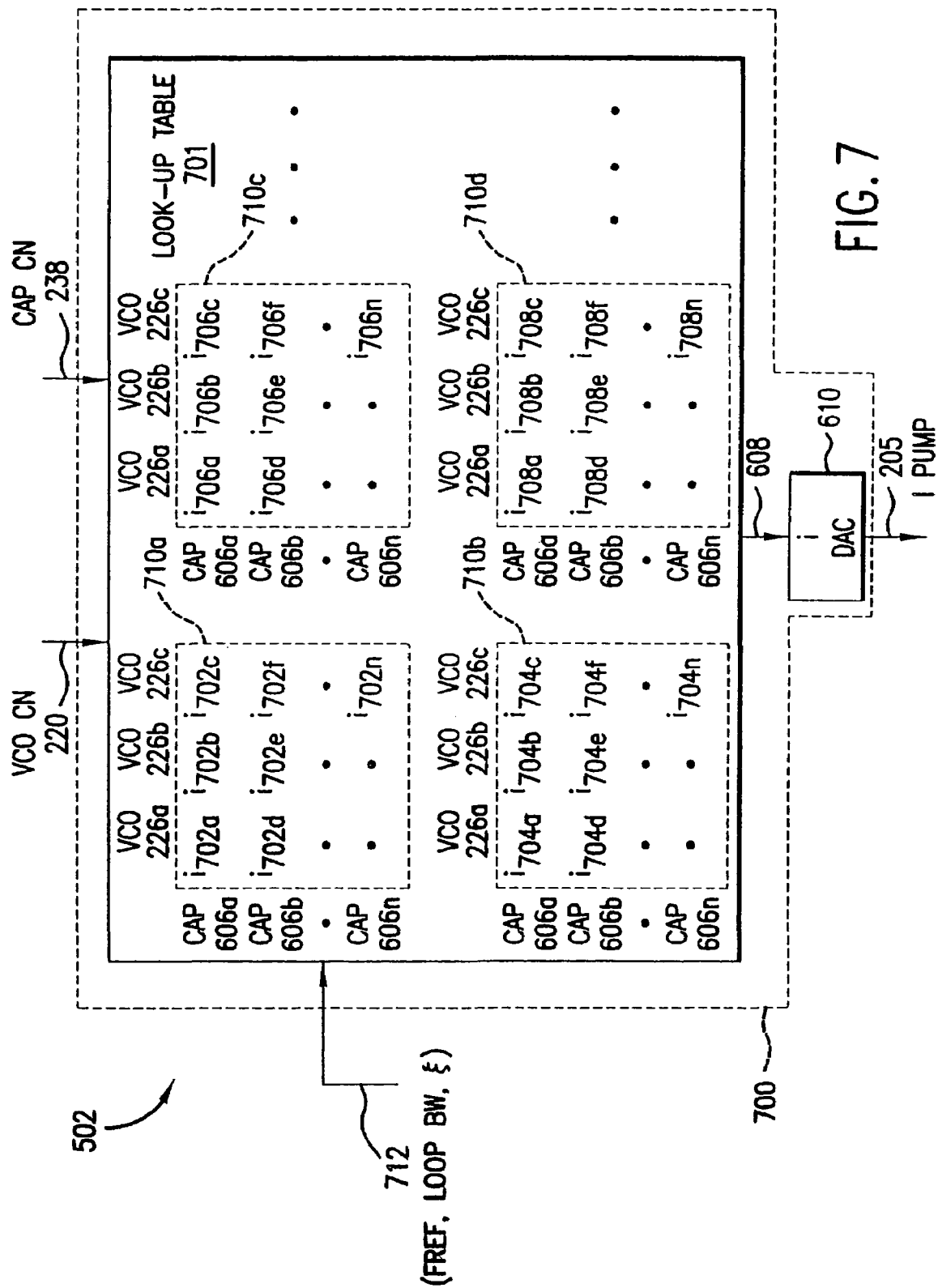
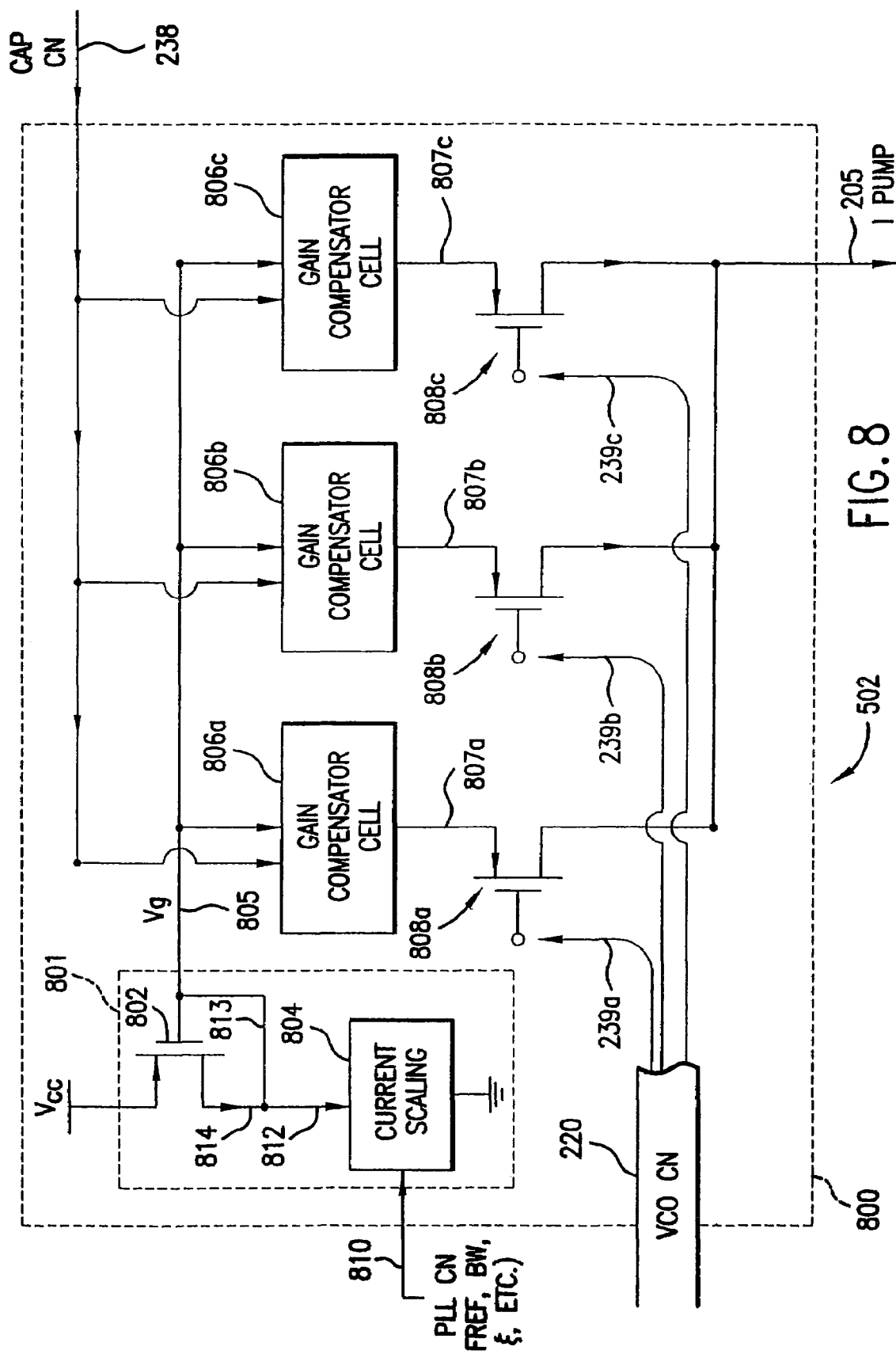


FIG. 6





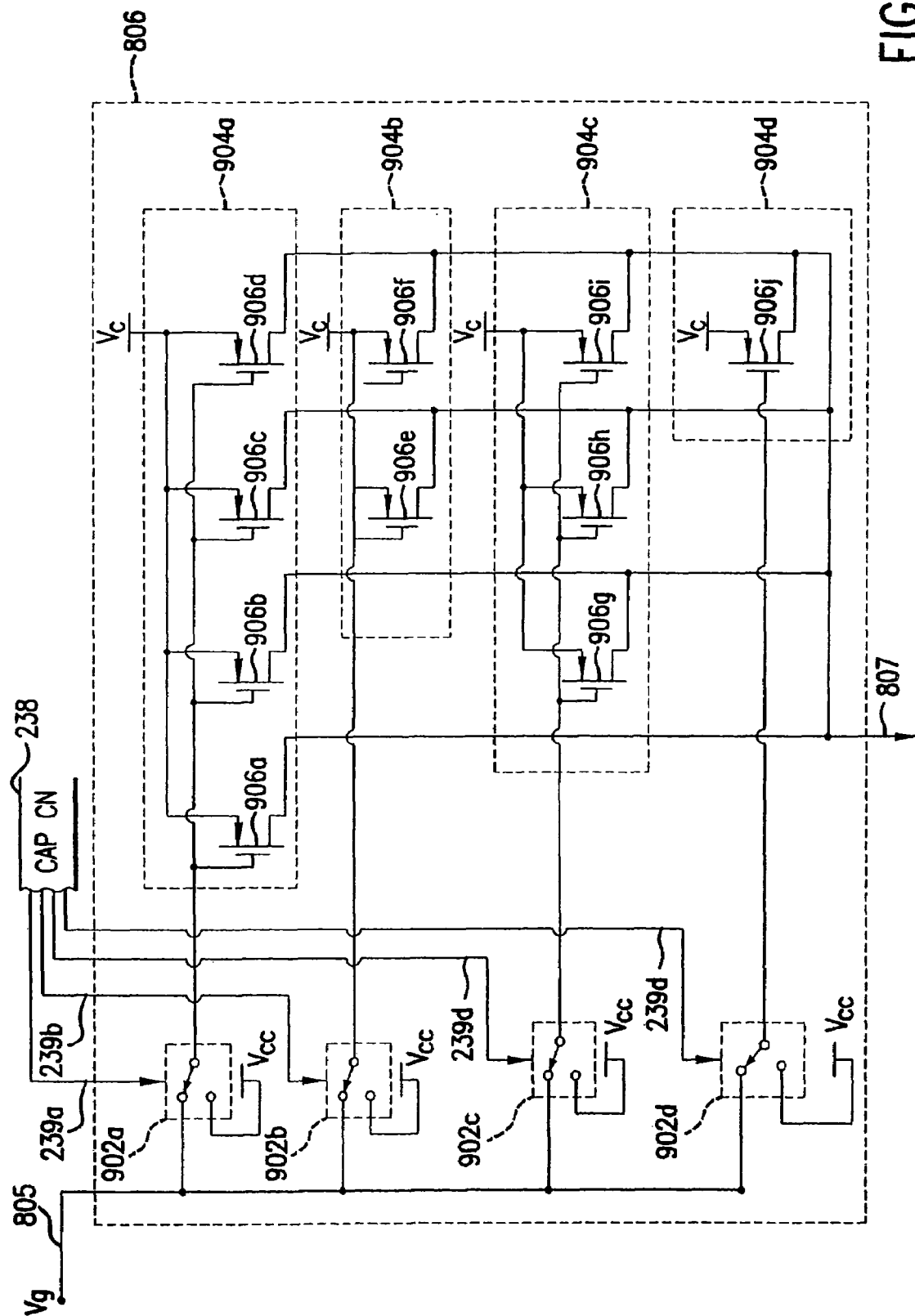


FIG. 9

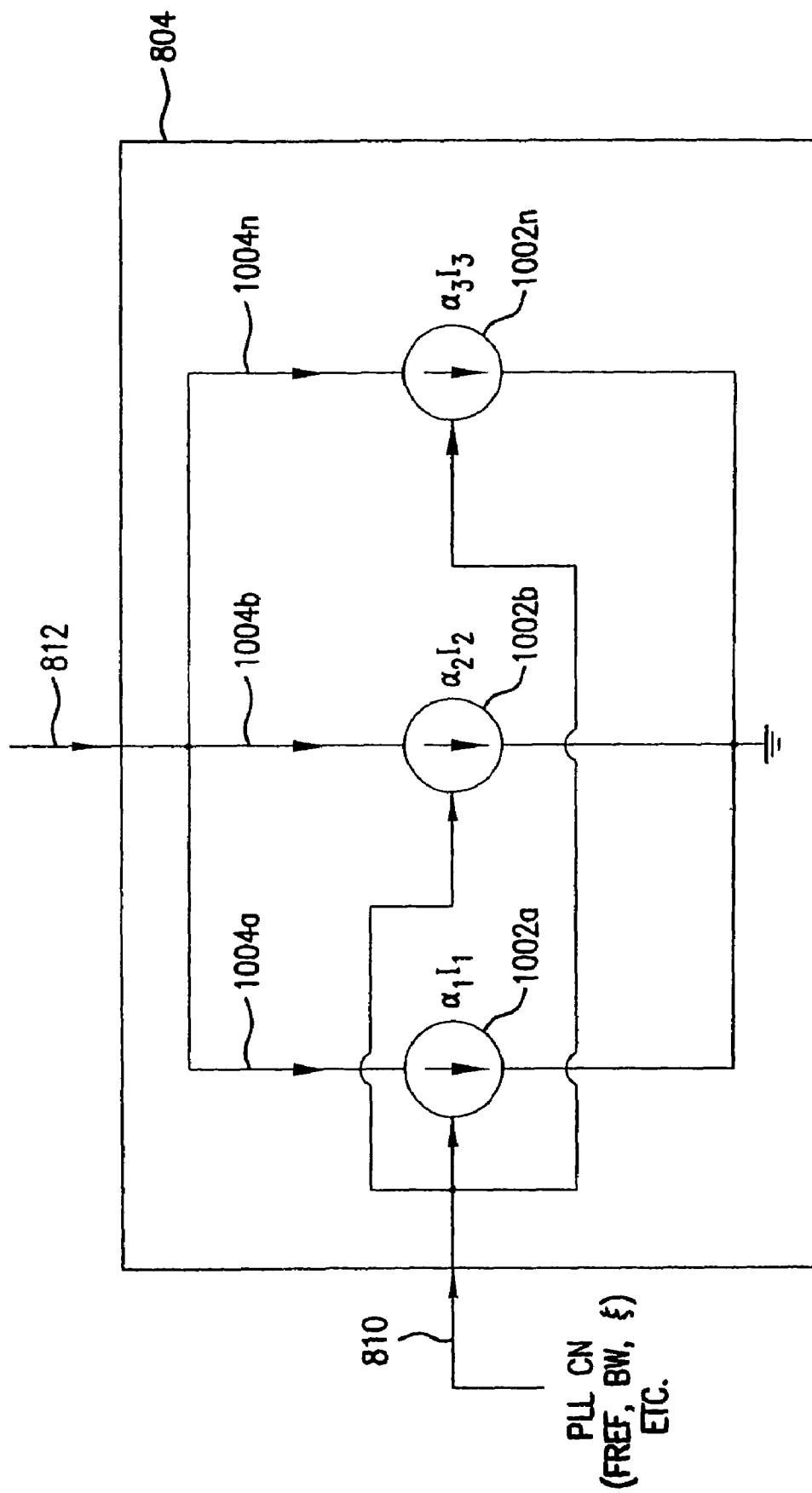


FIG. 10

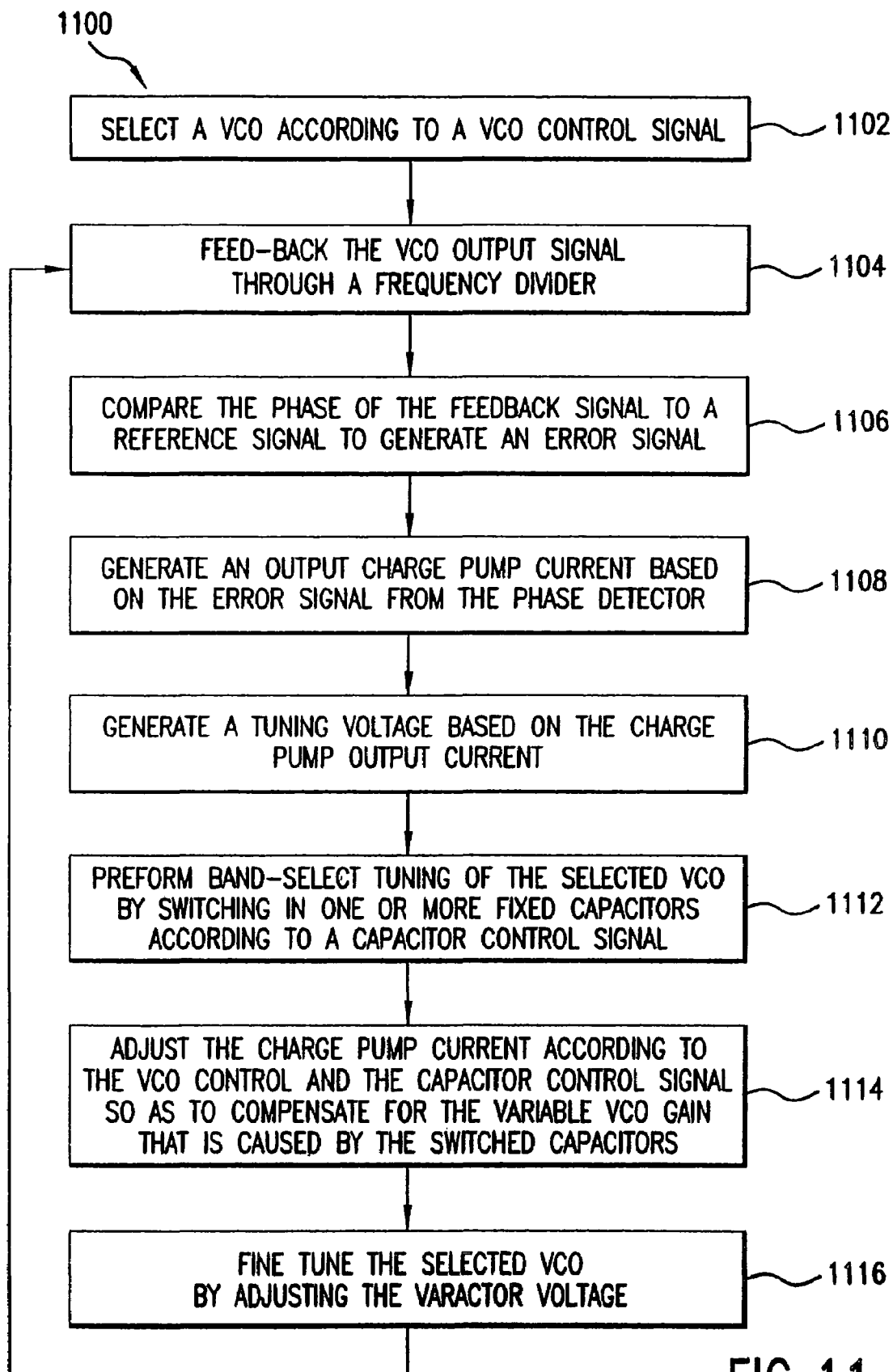


FIG. 11

1200

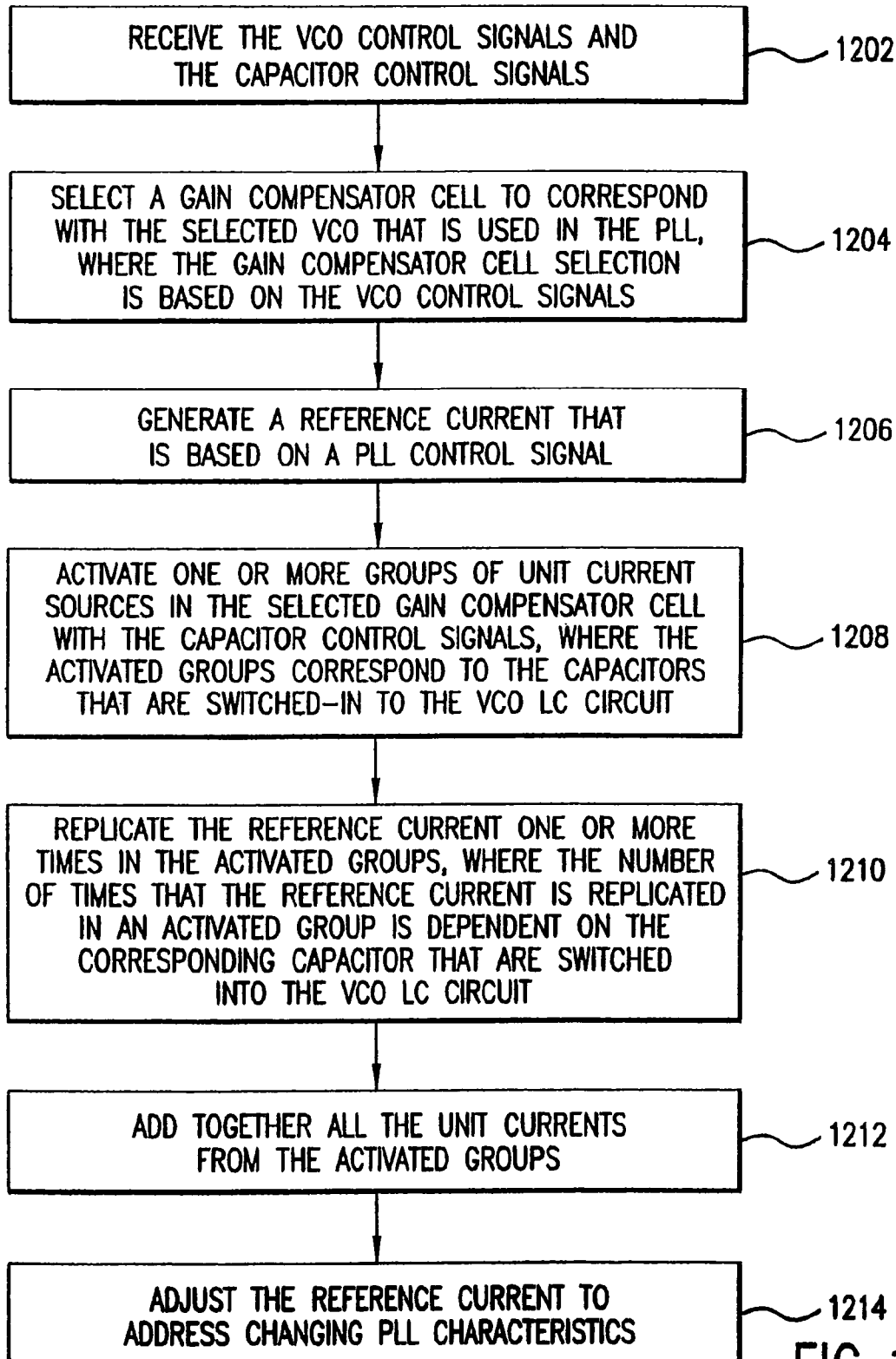


FIG. 12

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APPARATUS AND METHOD FOR PHASE LOCK LOOP GAIN CONTROL USING UNIT CURRENT SOURCES

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a divisional of U.S. application Ser. No. 11/019,451, filed Dec. 23, 2004, which is a continuation of U.S. application Ser. No. 10/443,741, filed May 23, 2003 (now issued U.S. Pat. No. 6,838,947 B2), which is a continuation of U.S. application Ser. No. 09/811,611, filed Mar. 20, 2001 (now issued U.S. Pat. No. 6,583,675 B2). The above-identified applications are hereby incorporated herein by reference in their entirety.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention generally relates to gain control in a phase lock loop, and more specifically to phase lock loop gain control using scaled unit current sources.

2. Background Art

Radio frequency (RF) transmitters and receivers perform frequency translation by mixing an input signal with a local oscillator (LO) signal. Preferably, the LO signal should have a frequency spectrum that is as close to a pure tone as possible in order to maximize system performance during the signal mixing operation. The deviation of the LO signal from a pure tone is quantified as phase noise or phase jitter, and is generally referred to as spectral purity. In other words, a LO signal with good spectral purity has low phase noise.

Phase-locked loops (PLLs) are often used in frequency synthesizers to generate the LO signal. A PLL frequency synthesizer produces an output signal, typically a sinewave or square wave, that is a frequency multiple of an input reference signal. The PLL output signal is also in phase synchronization with the input reference signal. PLLs are feedback loops, and therefore are susceptible to instability. Therefore, loop stability is a key performance parameter for PLLs, in addition to spectral purity of the output signal.

A resonant-tuned voltage controlled oscillator (VCO) is typically utilized in a PLL to generate the PLL output signal. A resonant tuned VCO includes an active device and a resonant LC circuit, where the impedance of the resonant LC circuit becomes a short or an open at a resonant frequency. When the resonant circuit is connected in parallel with the active device, a positive feedback path is created in the active device at the resonant frequency of the LC circuit. The positive feedback path causes the active device to oscillate at the resonant frequency of the LC circuit.

The resonant tuned LC circuit typically includes multiple fixed capacitors that can be switched in or out of the LC circuit, a varactor diode, and at least one inductor. The resonant frequency of the LC circuit (and therefore the oscillation frequency of the VCO) is tuned via a coarse tuning mechanism and a fine tuning mechanism. Coarse frequency tuning (or band-selection) is performed by switching one or more of the fixed capacitors in the LC circuit. Whereas, fine frequency tuning is performed by changing the voltage across the varactor diode, which produces a capacitance that varies depending on the applied tuning voltage. Both tuning mechanisms operate by changing the capacitance, and therefore the resonant frequency of the LC circuit. The varactor tuning range is slightly larger than one fixed capacitor, and therefore provides some overlap between the fixed capacitors.

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VCO gain is defined as the VCO frequency shift per unit change in the varactor tuning voltage. A problem with varactor-tuned VCOs is that the VCO gain versus fixed capacitance is variable. In other words, the VCO frequency shift versus tuning voltage is dependent on the fixed capacitance that is switched-in to the LC circuit. The variable VCO gain creates difficulties when designing a PLL because the entire PLL loop gain, bandwidth, and damping response varies with respect to the oscillator frequency. This in turn makes it difficult to optimize the output phase noise and reduces overall spectral purity. Therefore, it is desirable to compensate for the variable VCO gain, in order to maintain the overall PLL gain at a desired optimum value.

In addition to the VCO gain, it is desirable to adjust or tune other PLL characteristics, such as loop bandwidth, reference frequency, and damping factor, without having to tune or replace PLL components.

BRIEF SUMMARY OF THE INVENTION

The gain compensator invention compensates for gain variation in a varactor-tuned VCO in order to maintain the overall PLL gain at a desired level over frequency. The VCO includes a LC circuit that has multiple fixed capacitors that are arranged in parallel with the varactor diode and the active portion of the VCO. The fixed capacitors are switched-in to the LC circuit by corresponding capacitor control signals. Coarse frequency tuning (also called band-select tuning) is performed by adding or subtracting one or more of the fixed capacitors to the LC circuit according to the capacitor control signal. Fine frequency tuning is performed by adjusting the tuning voltage on the varactor diode, where the VCO gain is defined as the frequency shift per unit change in varactor tuning voltage. VCO gain varies with the fixed capacitance that is switched-in to the LC circuit, and therefore changes with band-select tuning of the VCO. The gain compensator compensates for the variable VCO gain by generating a reference charge pump current for the PLL based on information that is carried in the capacitor control signal. Therefore, the gain compensator is able to simultaneously adjust the charge pump current to maintain an overall flat PLL gain as fixed capacitors are incrementally added to (or subtracted from) the LC circuit.

The gain compensator includes one or more cells that each correspond to a particular VCO that can be switched into the PLL at a given time. A VCO control signal selects a particular VCO for the PLL based on frequency, and also activates the appropriate cell. Each cell includes a plurality of unit current sources, where each unit current source substantially replicates (or copies) a pre-defined reference scale current. The unit current sources are arranged into one or more groups, where each group corresponds to a fixed capacitor in the LC circuit. Each group of unit current sources generates a portion of the total pump current when the corresponding capacitor is switched-in to the LC circuit. The number of unit current sources in each group is determined to compensate for the variable VCO gain that occurs when the corresponding fixed capacitor is switched-in to the LC circuit. Each group of unit current sources is activated by the same capacitor control signal that controls the corresponding fixed capacitor. Therefore, when a fixed capacitor is switched-in to the LC circuit, the corresponding group of unit current sources is simultaneously activated and switched-in to the cell to compensate for the variable VCO gain that is caused by the fixed capacitor.

An advantage of the gain compensator invention is that the number of unit current sources that are activated for a

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corresponding fixed capacitor is arbitrary, but the current produced is linearly proportional to the reference scale current. In other words, there is no predefined relationship between the number of unit current sources in each group that would restrict the relative amount of current produced by each group. Therefore, the total pump current can be freely optimized to incrementally adjust for the variable VCO gain that is associated with various combinations of fixed capacitors.

A further advantage of the gain compensator invention is that the reference scale current for the gain compensator cells is generated based on a PLL control signal. The PLL control signal specifies various PLL characteristics, such as the frequency of the reference signal, the PLL bandwidth, and the PLL damping factor, etc. Since the unit current sources are configured to replicate the reference scale current, all of the unit current sources can be simultaneously adjusted by changing the reference scale current. Therefore, the charge pump current can be efficiently adjusted to tune the mentioned characteristics of PLL for different operating conditions, without requiring the replacement of PLL components.

Further features and advantages of the present invention, as well as the structure and operation of various embodiments of the present invention, are described in detail below with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS/FIGURES

The present invention is described with reference to the accompanying drawings. In the drawings, like reference numbers indicate identical or functionally similar elements. Additionally, the left-most digit(s) of a reference number identifies the drawing in which the reference number first appears.

FIG. 1A illustrates a tuner 100 that is an example tuner environment for the present invention;

FIG. 1B illustrates dual frequency conversion that is performed by the tuner 100;

FIG. 2 illustrates a PLL 200 that can be used with the tuner 100;

FIG. 3 illustrates a VCO 300 that can be used with the PLL 200;

FIG. 4 illustrates variable VCO gain;

FIG. 5 illustrates a PLL 500 that includes a gain compensator 502, according to embodiments of the present invention;

FIG. 6 illustrates a ROMDAC 600 that is one embodiment of a gain compensator, according to embodiments of the present invention;

FIG. 7 illustrates a ROMDAC 700 having an expanded look-up table 701, according to embodiments of the present invention;

FIG. 8 illustrates a gain compensator 800 having a current scaler 804 that forms a current mirror configuration with one or more gain compensator cells 806, according to embodiments of the present invention;

FIG. 9 illustrates a gain compensator cell 806 having multiple unit current sources, according to embodiments of the present invention;

FIG. 10 illustrates the current scaler 804, according to embodiments of the present invention;

FIG. 11 illustrates a flowchart 1100 that describes the operation of a PLL having compensation for nonlinear VCO gain, according to embodiments of the present invention; and

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FIG. 12 illustrates a flowchart 1200 that describes the operation of a gain compensator cell, according to embodiments of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

1. Example Tuner Application

Before describing the invention in detail, it is useful to describe an example tuner application for the invention. The invention is not limited to the tuner application that is described here, and is applicable to other tuner and non-tuner applications as will be understood to those skilled in the relevant arts based on the discussions given herein.

FIG. 1A illustrates a schematic of a tuner assembly 100 that has an RF automatic gain control circuit (AGC) 102, and a tuner 134. The tuner assembly 100 receives an RF input signal 101 having multiple channels and down-converts a selected channel to an IF frequency, to produce an IF signal 133. For instance, the RF input signal 101 can include multiple TV channels that typically have 6 MHz frequency spacings and cover a range of 57–860 MHz, and where the selected channel is down-converted to an IF frequency at 44 MHz, 36 MHz or some other desired IF frequency for further processing. The structure and operation of the AGC circuit 102 and the tuner 134 are described in further detail below.

The AGC circuit 102 provides automatic gain control using a variable resistor 104 and a low noise amplifier (LNA) 106. The variable resistor 104 attenuates the RF input signal 101 according to a control signal 103. In embodiments, the control signal 103 is based on the signal amplitude of the IF signal 133 so that the RF front-end gain can be adjusted to achieve a desired amplitude for the IF signal 133. The LNA 106 provides low noise amplification and converts a single-ended input signal to a differential RF signal 107.

The tuner 134 has a dual conversion architecture (one up-conversion, one down-conversion) that includes an input mixer 108 and an image reject mixer 118. The input mixer 108 is driven by a first phase locked loop (PLL) 110 that has coarse tuning capability from 1270–2080 MHz. The image reject mixer 118 has two component mixers 120a and 120b that are driven in quadrature by a second PLL 124 through a quadrature polyphase filter 122. The PLL 124 has a relatively fixed frequency of 1176 MHz (for a 44 MHz IF) and has fine frequency tuning capability. A polyphase filter 126 is coupled to the output of the image reject mixer 118 to combine the quadrature outputs of the mixers 120. Two separate off-chip surface acoustic wave (SAW) filters 114 and 130 are used to perform IF filtering in the tuner 134. The first SAW filter 114 is connected between the first mixer 108 and the image reject mixer 118. The passband of the SAW filter 114 is centered at 1220 MHz, and is only a few channels wide (e.g. 1–3 channels wide or 18 MHz for 6 MHz TV channel spacings). The second SAW filter 130 has a passband at 44 MHz and is coupled to the output of the polyphase filter 126. Additionally, various on-chip amplifiers 108, 116, 128, and 132 are included throughout the tuner 134 to provide signal amplification, as necessary.

The operation of the tuner 134 is described as follows and in reference to the frequency spectrum that is illustrated in FIG. 1B. The first mixer 108 mixes the RF signal 107 with a LO signal 109 that is generated by the PLL 110. Since to a first IF 111 having a frequency that is above the 57–860 MHz input frequency band. The first IF 111 is sent off-chip

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to the SAW filter **114**, which has a narrow passband window centered at 1220 MHz. The first SAW filter **114** selects a desired channel **115** that is within its narrow passband window, and substantially rejects all of the remaining channels. Therefore, a particular channel is selected by varying the frequency of the LO signal **109** so that the desired channel is up-converted into the narrow passband of the IF filter **114**. The desired channel **115** (at 1220 MHz) is sent back on-chip to the image reject mixer **118** that is driven by a quadrature LO signal **119** from the polyphase filter **122**. The image reject mixer **118** down-converts the desired channel **115** to a 44 MHz IF signal **127** that appears at the output of the polyphase filter **126**, where I and Q components of the IF signal **127** are combined in the polyphase filter **126**. Finally, the IF signal **127** is filtered a second time by the bandpass SAW filter **130** to reject any unwanted frequency harmonics, producing the output IF signal **133** at 44 MHz and carrying the information in the desired channel.

The specific frequencies mentioned in the description of the tuner assembly **100**, and throughout this application, are given for example purposes only and are not meant to be limiting. Those skilled in the arts will recognize other frequency applications for the tuner assembly **100** based on the discussion given herein. These other frequency applications are within the scope and spirit of the present invention.

2. Phase Lock Loop:

The first PLL **110** and the second PLL **124** are represented by the PLL **200** that is illustrated in FIG. 2. The PLL **200** generates a PLL output signal **227** that is a frequency multiple of a reference signal **201**, and where the output signal **227** is phase-locked to the reference signal **201**. The PLL **200** self-corrects for any phase (and therefore frequency) variations between the reference signal **201** and the output signal **227** via a feedback mechanism that is described as follows. The structure and operation of the PLL **200** are described as follows.

The PLL **200** structure includes: a phase detector **202**, a charge pump **204**, a frequency divider **206**, a loop filter **208**, a coarse tuning circuit **214**, a VCO assembly **222**, and a LC resonant circuit **228**. The loop filter **208** includes a variable resistor **210** and a variable capacitor **212** that are controlled by an I²C signal **207**. The coarse tuning circuit **214** includes a comparator **216** and a shift register **218**. The VCO assembly **222** includes multiple component VCOs **226a-c**, where each VCO **226** preferably covers a particular frequency band. A VCO **226** is switched-in to the PLL **200** by closing a corresponding switch **224**. The switches **224a-c** are controlled by corresponding control signals **223a-c** that make-up a VCO control bus **220**. The LC resonant circuit **228** is connected in parallel with the VCO assembly **222** and includes: multiple fixed capacitors **232a-n** having corresponding switches **230a-n**, a varactor **234**, and an inductor **236**. One or more of the fixed capacitors **232** are switched in-parallel with the selected VCO **226** by closing the corresponding switch(s) **230**. The switches **230** are controlled by corresponding control signals **239a-n** that make-up a capacitor control bus **238**.

Each VCO **226** is a resonant tuned oscillator whose oscillation frequency is controlled by the resonant frequency of the parallel LC circuit **228**. The resonant frequency of the LC circuit **228** is determined by the relative total capacitance and inductance according to the equation:

$$f_0 = (1/2\pi) \cdot 1/\sqrt{LC} \quad \text{Eq. 1}$$

As discussed further below, coarse frequency tuning (e.g. band-selection) of the selected VCO **226** is performed by

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switching in one or more of the fixed capacitors **232** into the LC circuit **228**. This changes the resonant frequency of the LC circuit **228**, and therefore the oscillation frequency of the selected VCO **226**. Fine frequency tuning is performed by changing the control voltage on the varactor **234**, which has a variable capacitance that changes with applied voltage. The VCO gain is defined as the change in the VCO output frequency per unit change in the voltage across the varactor **234**.

The PLL **200** operates based on known PLL feedback principles. A VCO **226** is selected based on the desired frequency of operation for the PLL **200**, and is switched-in to the PLL **200** by closing the appropriate switch **224** using the appropriate control signal **223**. The PLL output signal **227** from the selected VCO **226** is fed back to a phase detector **202** through the frequency divider **206**. The frequency divider **206** normalizes the frequency of the output signal **227** to that of the reference signal **201** for comparison in the phase detector **202**. The phase detector **202** compares the phase of the output signal **227** to the reference signal **201**, and generates a DC error signal **203** that represents the phase difference between the two signals. The charge pump **204** receives the error signal **203** and a reference pump current **205**. The charge pump **204** sources (or sinks) a percentage of the pump current **205** based on the error signal **203**, as will be understood by those skilled in the arts. The output current of the charge pump **204** drives the loop filter **208** to produce a tuning voltage **209**. Part of the tuning voltage **209** is dropped across the variable capacitor **212** to generate a tuning voltage **211**. As discussed further below, the tuning voltages **209** and **211** control the oscillation frequency of the selected VCO **226**.

The tuning voltages **209** and **211** adjust the resonant frequency of the LC circuit **228** (and therefore the oscillation frequency of the selected VCO **226**) via a coarse tuning mechanism and a fine tuning mechanism, respectively. More specifically, the coarse tuning circuit **214** adds (or subtracts) one or more of the fixed capacitors **232a-n** to the LC circuit **228** based on the tuning voltage **211**. Similarly, the tuning voltage **209** directly adjusts the voltage (and therefore the capacitance) of the varactor **234** to implement fine frequency tuning. Both tuning mechanisms adjust the oscillation frequency of the VCO **226** by changing the capacitance of the LC circuit **228**, which shifts the resonant frequency of the LC circuit **228**. The tuning range of the varactor **234** is slightly larger than one fixed capacitor **232**, and therefore provides some tuning overlap between the fixed capacitors **232**. The coarse tuning circuit **214** is described further below.

The coarse tuning circuit **214** includes a window comparator **216** and a bi-directional shift register **218**. The window comparator **216** receives the tuning voltage **211** and also receives input reference voltages v_1 and v_2 . The window comparator **216** determines if the voltage **211** is within a voltage "window" that is defined between the input reference voltages v_1 and v_2 , and generates a control signal **217** that controls the bi-directional shift register **218** based on this determination. The shift register **218** stores a series of bits that control the capacitor switches **230** via the control bus **238** to add (or subtract) the corresponding capacitors **232** to (or from) the LC circuit **228**. A "1" bit on the control line **239** causes the corresponding switch **230** to close and thereby adds the corresponding capacitor **232** to the LC circuit **228**. A "0" bit on the control line **239** causes the switch **230** to open and thereby subtracts the corresponding capacitor **232** from the LC circuit **228**.

The coarse tuning circuit **214** operates to self-correct coarse variations in the oscillation frequency of the selected VCO **226** by adding or subtracting capacitors **232**, based on the tuning voltage **211**. If the comparator **216** determines that the voltage **211** is below v_1 , then the comparator **216** causes a series of "1"s to be shifted through the shift register **218**, which incrementally adds capacitors **232** to the LC circuit **228** until the tuning voltage **211** is within the v_1 -to- v_2 voltage window. If the comparator **216** determines that the voltage **211** is above the voltage v_2 , then the comparator **216** causes a series of "0"s to be shifted through the shift register **218**, which incrementally subtracts capacitors **232** from the LC circuit **228** until the tuning voltage **211** is within the v_1 -to- v_2 voltage window. As described above, the frequency of the selected oscillator **226** changes whenever capacitance is added to, or subtracted from, the LC circuit **228**. If the comparator **216** determines that the voltage **211** is within the voltage window defined by v_1 and v_2 , then no action is taken and the fixed capacitance in the LC circuit **228** remains unchanged. In other words, the tuning voltage **211** is within an acceptable voltage range (or "window"), and correspondingly, the frequency of the output signal **227** is within an acceptable frequency range. Therefore the number of the fixed capacitors **232** that are switched-in to the LC circuit **228** is not changed.

3. Example VCO Configuration

FIG. 3 illustrates a differential VCO **300** as one embodiment of VCO **226** and the LC resonant circuit **228**. The VCO **300** is meant for example purposes only and is not meant to limit the invention in any way. Other oscillator configurations could be utilized to practice the invention, as will be understood by those skilled in the relevant arts based on the discussions given herein.

The VCO **300** includes the active VCO portion **226** and the resonant LC circuit **228**. The active portion includes a pair of cross coupled transistors **302a** and **302b** that oscillate at the resonant frequency of LC circuit **228**. In this cross-coupled configuration, the drain of transistor **302a** is connected to the gate of transistor **302b**. Likewise, the drain of transistor **302b** is connected to the gate of the transistor **302a**. The LC circuit **228** is also coupled to the drains of the transistors **302**. At resonance, the LC circuit **228** causes a positive feedback path between the cross-coupled transistors **302**, which causes the transistors to oscillate at the resonant frequency of the LC circuit **228**, producing the differential output signal **227**.

The oscillation frequency of the VCO **300** can be tuned by two mechanisms. Coarse frequency tuning (or band selection) is performed by adding or subtracting the fixed capacitors **232** using the corresponding switches **230**. Fine frequency tuning is performed by the tuning voltage **209**, which varies the capacitance produced by the series-connected varactor diodes **234a** and **234b** that are attached to the drains of the transistors **302**. The frequency change of VCO **300** per unit change in varactor **234** voltage is defined as the VCO gain. As stated above, the tuning range of the varactor **234** is slightly larger than the capacitance of one fixed capacitor **232**, and therefore provides some tuning overlap between the fixed capacitors **232**.

In one embodiment, the varactors **234** are PN junction varactors, and in an alternate embodiment these varactors **234** are MOSFET varactors, depending on the designer's preference.

4. PLL Gain Compensation

PLL gain is defined as the frequency change of the output signal verses the phase difference between the feedback signal and the reference signal. The forward PLL gain is determined as follows:

$$G(s) = K_{PHI} (R_{LF} + 1/sC_{LF}) K_{VCO}/s; \quad \text{Eq. 2}$$

where:

K_{PHI} = Phase detector gain (mA/radian)

R_{LF} = Loop filter resistance

C_{LF} = Loop filter capacitance

K_{VCO} = VCO gain (MHZ/volt)

s represents frequency

The feedback PLL gain $H(s) = 1/N$, where N is the feedback frequency division ratio. The overall open loop gain is $G(s)H(s)$, and the overall closed-loop gain is $G(s)/[1+G(s)H(s)]$.

As described above, the PLL **200** performs coarse frequency tuning by incrementally adding (or subtracting) one or more of the fixed capacitors **232** that are in-parallel with the selected VCO **226**. Fine frequency tuning is performed by adjusting the voltage on the varactor **234**, where the VCO gain is defined as the frequency shift per unit change in the tuning voltage **209**. A problem with varactor-tuned VCOs is that the VCO gain verses the fixed capacitance **232** is variable. FIG. 4 illustrates this characteristic with a graph of VCO gain **402** verses fixed capacitance. As shown, the VCO gain curve **402** is reduced for a large fixed capacitance and is increased for a small fixed capacitance. Variable VCO gain is undesirable because it causes the PLL forward gain to change according to Eq. 2. In VCO applications with a large minimum-to-maximum capacitance tuning range, this VCO gain variability can cause loop instability, and reduced spectral purity in the PLL output signal. In a preferred embodiment, the VCO gain variability is compensated for by a compensator gain **404** so that the overall PLL gain **406** remains relatively flat for variations in fixed capacitance (and therefore VCO frequency). More specifically, the charge pump current **205** is compensated to counter the variable VCO gain so that the overall PLL gain is flat.

FIG. 5 illustrates a PLL **500** that has a gain compensator **502** to adjust the charge pump current **205** in order to linearize (and flatten) the overall PLL gain of the PLL **500**. The gain compensator **502** generates the pump current **205** based on the control information carried by the VCO control bus **220** and the capacitor control bus **238**. As discussed above, the VCO control bus **220** selects the appropriate VCO **226** based on the desired frequency range for the PLL output signal **227**. The capacitor control bus **238** selects the fixed capacitors **232** that are switched-in parallel with the selected VCO **226** for coarse frequency tuning of the VCO **226**. Therefore, the gain compensator **502** can tailor the reference pump current **205** for a specified VCO **226** at a specified fixed capacitance **232** value, and thereby compensate for the variable VCO gain vs. fixed capacitance.

FIG. 6 illustrates a read only memory digital-to-analog converter (ROMDAC) **600** that is one example embodiment of the gain compensator **502**, according to embodiments of the invention. Referring to FIG. 6, the ROMDAC **600** includes a look-up table **602** and a current digital-to-analog converter **610**. The lookup table **602** stores pump current values **604a-n** that are indexed by the selected VCO **226** and a fixed capacitance total **606**, where the fixed capacitance total **606** is the parallel sum of the capacitors **232** that are switched-in to the LC circuit **228**. The pump current values **604** are selected to compensate for the variable VCO gain vs.

capacitance, given an identified VCO 226 and the fixed capacitance total 606. Preferably, the PLL 200 is characterized beforehand for each VCO 226 to determine the pump current values 604 that produces a flat overall PLL gain for various capacitance totals 606. The look-up table 602 outputs a pump current value 608 that corresponds to identified VCO 226 and the fixed capacitance total 606. The DAC 610 converts the pump current value 608 to the actual analog pump current 205 that drives the charge pump 204. As capacitors 232 are added to or subtracted from the LC circuit 228, the lookup table 602 selects the appropriate pump current value 604 so as to maintain a flat overall PLL gain. Therefore, the pump current 205 is adjusted for various total capacitance 606 to counteract the variable gain of the selected VCO 226, and thereby flatten the overall gain of the PLL 500.

An advantage of the ROMDAC 600 is that the pump current values 604 can be totally arbitrary and mathematically unrelated to each other. In other words, the pump currents 604 can be individually selected to produce an optimum overall PLL gain for a given VCO 226 and capacitance total 606, without being restricted by any mathematical relationship. In an alternate embodiment, the various pump currents 604 are mathematically related to each other, or to the VCO control signal 220 or the capacitor control signal 238.

In addition to PLL gain, it is desirable to tune various other PLL characteristics, such input reference frequency, loop bandwidth, damping factor, etc. This allows the same PLL to be used in different operating environments. For instance, it is often desirable to have a PLL configuration that is operable with a number of different reference frequencies. If the frequency of the reference signal 201 increases by factor of two, the PLL loop gain should preferably be adjusted to compensate for this increase so that the PLL loop remains stable and accurate. The PLL loop gain can be appropriately adjusted by reducing the frequency division of the frequency divider 206 by a factor of two. However, this would require replacement of the frequency divider 206 for each possible reference frequency, or the use of a programable frequency divider. Alternatively, the charge pump current could be reduced by a factor of two to get the same effect.

FIG. 7 illustrates a ROMDAC 700 as another embodiment of the gain compensator 502, according to embodiments of the present invention. The ROMDAC 700 has an expanded lookup table 701 that has multiple sets 710a-d of pump current values, where the sets 710 tune various PLL characteristics in addition to compensating for variable VCO gain. Some PLL characteristics include, but are not limited to, PLL reference signal frequency, loop bandwidth, loop damping, etc. For example, sets 710a and 710b have pump current values 702a-n and 704a-n, respectively, which are customized for different reference frequencies. The pump current values 702a-n can correspond to a first reference signal 201 frequency, and the pump current values 704a-n can correspond to a second reference signal 201 frequency. Therefore, if the frequency of the reference signal 201 changes, then the pump current value 608 can be selected from the appropriate pump current set 710. In another example, the pump current sets 710c and 710d are customized to maintain loop bandwidth for different loop damping factors. The loop damping factor is increased or decreased by adjusting the variable resistor 210 in the loop filter 208, which also determines the loop bandwidth. If the damping factor is changed, then the loop bandwidth can be held constant by selecting the appropriate set 710c or 710d that

adjusts the charge pump current 205 to sufficiently counter the effect on the loop bandwidth.

To summarize, by storing multiple sets 710 of charge pump values in the lookup table 701, multiple PLL characteristics can be adjusted or tuned in addition to PLL gain. This allows the same PLL 500 to be used under different PLL operating conditions, without replacing PLL components. The number of pump current sets 710 can be expanded to adjust any number of PLL characteristics, assuming there is sufficient memory space in the look-up table 701.

FIG. 8 illustrates a gain compensator 800 that is another embodiment of the gain compensator 502 in FIG. 5. The gain compensator 800 includes: a voltage generator 801, gain compensator cells 806a-c that correspond to VCOs 226a-c, and PFETs 808a-c that correspond to the gain compensator cells 806a-c. Each gain compensator cell 806 generates a prospective pump current 807 that compensates for the variable VCO gain of its corresponding VCO 226 caused by the fixed capacitors 232. Since only one VCO 226 is operational at a given time, only one prospective pump current 807 becomes the actual pump current 205 that feeds the charge pump 204. The PFETs 808 operate as switches that are controlled by the VCO control signals 239 and select the appropriate prospective pump current 807 to correspond with the selected VCO 226. For example, if the VCO 226a is the selected VCO 226, then the control signal 239a causes the PFET 808a to conduct so that the current 807a becomes the feed for the pump current 205. Accordingly, control signals 239b and 239c cutoff their respective PFETs 808b and 808c, and therefore only the current 807a feeds the pump current 205.

The structure of the gain compensator cell 806 is shown in FIG. 9 and includes: switches 902a-d that are controlled by the respective capacitor control signals 239a-d, and unit current sources 906a-j that are arranged in groups 904a-d. Preferably, each unit current source 906 generates substantially the same amount of unit current (within transistor tolerances), where the amount of unit current is based on a gate voltage 805 that is generated by the voltage generator 801. Each group 904 corresponds to a capacitor 232, and generates a portion of the total pump current 205 when the respective capacitor 232 is switched-in to the LC circuit 228. The number of unit current sources 906 in each group 904 is selected to compensate for the variable VCO gain that occurs when the corresponding capacitor 232 is switched-in to the LC circuit 228. For example, group 904a corresponds to capacitor 232a, and has 4 unit current sources 906 to compensate for variable VCO gain that is caused by the capacitor 232a. Whereas, group 904b only has 2 unit current sources 906 to address the variable VCO gain caused by the capacitor 232b, and so on. Note that the number of current sources 4,2,3,1 that are shown in FIG. 9 for the groups 902a-d are for illustration purposes only, and is not meant to be limiting. Furthermore, the number of groups 904, namely 4 as shown, is not meant to be limiting. In embodiments of the invention, the number of groups 904 should be less than or equal to the number of fixed capacitors 232.

A group 904 is switched into the gain compensator cell 806 when the corresponding switch 902 connects Vg 805 to the unit current sources 906 in the group 904. Once connected to a group 904, the Vg 805 activates the current sources 906 and determines the current produced by each current source 906. The switches 902 are controlled by the same capacitor control signals 239 that switches-in the respective capacitors 232 into the LC circuit 228. Therefore, when a capacitor 232 is switched-in to the LC circuit 228,

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the corresponding group 904 will be switched-in to the gain compensator cell 806, and therefore contribute to the prospective pump current 807. For instance, if the capacitor 232a is switched-in to the LC circuit 228 by the capacitor control signal 239a, then the group 904a of unit current sources 906 will be switched-in to the gain compensator cell 806 by the same control signal 239a. Therefore, the current from the group 904a will contribute to the prospective pump current 807, and thereby compensate for the variable VCO gain that is caused by the capacitor 232a. If the capacitor 232b is then switched-in to the LC circuit 228, then the group 904b is switched-in to the gain compensator cell 806 to compensate for the variable VCO gain that is caused by the capacitor 232b. As such, the charge pump current 205 is simultaneously adjusted to maintain a flat overall PLL as the capacitors 232 are incrementally added to (or subtracted from) the LC circuit 228.

Each unit current source 906 is preferably a PFET transistor, as shown. However, other transistor devices and configurations could be used for the unit current sources 906, including N-FET transistors, as will be understood by those skilled in the relevant arts based on the discussions given herein. These other transistor devices and configurations are within the scope and spirit of the present invention. For example, simultaneous use of NFET and PPET current sources would permit the gain compensator to compensate for a non-monotonic VCO gain verses fixed capacitance characteristic.

The voltage generator 801 and the current sources 906 operate as a "current mirror", where the drain currents of the selected unit current sources 906 copy or "mirror" a reference scale current 812. More specifically, the current scaler 804 sets the reference scale current 812, which operates as a current sink for the PFET 802. The PFET 802 operates as a diode because the gate and drain of the PFET 802 are shorted together by a conductor 813. The drain current 814 of the PFET 802 is substantially the same as the reference scale current 812 because there is substantially zero current on the conductor 813. The diode-connected PFET 802 generates the gate voltage 805 at its gate terminal to correspond with the drain current 814, and therefore to the reference scale current 812. If the drain current 814 deviates from the reference scale current 812 for some reason, then charge flows to/from the gate of the PFET 802 to bring the current 814 and the scale current 812 back in-line with each other. The gate voltage 805 is applied to the gate of the current sources 906 when their respective group 904 is selected by the capacitor control signals 239. The current sources 906 will reproduce (or "mirror") the drain current 814 due to the common gate voltage 805, if the device characteristics of the current sources 906 are sufficiently similar to those of the PFET 802. This current mirror effect occurs because two or more FETs that have a common gate-to-source voltage and similar device characteristics will generate substantially the same drain current. If a group 904 is not switched-in by the corresponding capacitor control signal 239 (because the corresponding capacitor 232 is not switched in the LC circuit 228), then the gates of the corresponding current sources 906 are connected to Vcc by the corresponding switch 902. When connected to Vcc, these non-selected current sources 906 are cutoff and do not generate a unit current.

Preferably, the PFET 802 and the current sources 906 are fabricated on the same semiconductor wafer using the same process, which improves the commonality of device characteristics. However, if the size of the unit current sources 906 is scaled relative to the size of the PFET 802, then the

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unit current sources 906 will generate a current that is proportional to the scale factor, as will be understood by those skilled in the relevant arts. This increases the flexibility of the gain compensator cell 806, as the current sources 906 can be scaled relative to the PFET 802 as well as relative to each other.

The current scaler 804 sets the reference scale current 812 based on a PLL control signal 810, where the PLL control signal 810 dictates various PLL characteristics such as the frequency of the reference signal 201, the PLL loop bandwidth, and PLL loop damping, etc. FIG. 10 illustrates one embodiment of the current scaler 804 and includes weighted current sources 1002a-n. The weighted current sources 1002a-n sink currents 1004a-n based the PLL variables in the PLL control signal 810. For example, the current source 1002a can be adapted to generate a current 1004a that is proportional to the frequency of the reference signal 201, and the current source 1002b can be adapted to generate a current 1004b that is proportional to the desired loop bandwidth, etc. The currents 1004a-n are summed together to form the reference scale current 812 that feeds the diode-connected PFET 802. Therefore, changes in the PLL variables are reflected in the reference scale current 812, and ultimately in the drain currents of the unit current sources 906 because of the current mirror effect described herein. More specifically, the PFET drain current 814 is substantially the same as the reference scale current 812, and gets copied to the drain currents of the unit current sources 906.

An advantage of using the current scaler 800 is that all of the current sources 906 (that are in a selected group 904) are simultaneously adjusted for changing PLL characteristics, in addition to compensating for variable VCO gain. Therefore, the prospective pump current 807 (and ultimately the final pump current 205) can be efficiently tuned to compensate for changing PLL characteristics. This allows the same PLL to be utilized under different operating conditions. Furthermore, the current scaler 804 reduces the size of the overall gain compensator because multiple sets of current sources 906 are not needed to address changing PLL characteristics. In contrast, the ROMDAC 700 requires multiple sets 710 of current values to address changing PLL characteristics, which increases the size of the ROMDAC 700.

The following examples illustrate the flexibility of the PLL 500 when using the current scaler 804 to adjust for changing PLL characteristics (besides VCO gain). In a first example, the frequency of the reference signal 201 increases by a factor of two, but the frequency divider 206 ratio is to remain constant. The same the frequency divider 206 can be used in the PLL 500 if the charge pump current 205 is reduced by approximately a factor of two. This is accomplished by reducing the reference scale current 812 that is generated by the current scaler 804, causing a corresponding reduction in the gate voltage 805. Through the current mirror effect, the current produced by the selected current sources 906 will be proportionally reduced by a factor of two. Therefore, the prospective current 807 (and the pump 205) will also be reduced by a factor of two as desired, and the same PLL 500 can be reused for the new reference frequency.

In a second example, the PLL damping factor ζ is to be increased, but the PLL bandwidth is to be held constant. The PLL damping factor ζ is increased by increasing the resistance of the variable resistor 210 in the loop filter 208. However, this also changes the loop bandwidth as will be understood by those skilled in the arts. To compensate, the current scaler 804 adjusts the reference scale current 812,

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and therefore the unit current sources **906** to produce a reference pump current **205** that compensates for the loop bandwidth.

In summary, and based on the examples herein, the gain compensator **800** is able to compensate for variable VCO gain and simultaneously tune other PLL characteristics by using the current mirror configuration described herein. These other PLL characteristics include but are not limited to changes in reference frequency, damping factor, and bandwidth.

The flowchart **1100** further describes the operation of the gain compensator **800** and VCO gain compensation according to embodiments of the present invention. The order of the steps in the flowchart **1100** is not limiting as all or some of the steps can be performed simultaneously or in a different order, as will be understood by those skilled in the arts.

In step **1102**, a VCO **226** is selected from the VCO **226a-c** based on the desired frequency of the output signal **227**. The selection is made by closing the appropriate switch **230** using the control signals **239** to switch-in the desired VCO **226**.

In step **1104**, the VCO output signal **227** is fed back to the phase detector **202** through a frequency divider **206**. The frequency divider **206** normalizes the frequency of the output signal **227** to that of the reference signal **201** for comparison in the phase detector **202**.

In step **1106**, the phase detector **202** compares the phase of the output signal **227** to the reference signal **201**, and generates a DC error signal **203** that represents the phase difference between the two signals.

In step **1108**, the charge pump **204** sources or sinks a percentage of a reference pump current **205** based the error signal **203**.

In step **1110**, the output current from the charge pump **204** drives the loop filter **208** to produce a tuning voltage **209**.

In step **1112**, one or more fixed capacitors **232** are switched-in to (or switched-out of) the LC resonant circuit **228** based on the tuning voltage **209**, to perform coarse frequency tuning of the selected VCO **226**. The fixed capacitors **232** perform coarse frequency tuning by shifting the resonant frequency of the LC circuit **228**, and therefore the selected VCO **226**. The fixed capacitors **232** are switched-in to (or switched-out of) the LC circuit **228** by switching the corresponding switches **230** using the control signals **239**.

In step **1114**, the gain compensator **800** adjusts the charge pump reference current **205** to compensate for variable VCO gain that is caused by adding or subtracting the fixed capacitors **232**. The reference current **205** is adjusted based on the VCO control signals **239** and also the capacitor control signals **239**. In embodiments, the reference current **205** is adjusted simultaneously with the switching of the fixed capacitors **232** by the capacitor control signals **239**.

In step **1116**, the tuning voltage **209** fine tunes the frequency of the selected VCO **226** by changing voltage across the varactor **234**. The VCO gain vs. fixed capacitance is substantially linearized by the gain compensator **800** in step **1114**, thereby flattening the PLL gain and improving the PLL spectral purity.

Flowchart **1200** further describes step **1114**, where the gain compensator **800** adjusts the charge pump current to compensate for variable VCO gain. The order of the steps in the flowchart **1200** is not limiting as all or some of the steps can be performed simultaneously or in a different order, as will be understood by those skilled in the arts.

In step **1202**, the gain compensator **800** receives the VCO control signals **239** and the capacitor control signals **239**.

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The VCO control signals **239** determine which VCO **226** is switched-in to the PLL **500**. The capacitor control signals **239** determine which fixed capacitors **232** are switched-in to the LC circuit **228**.

In step **1204**, a gain compensator cell **806** is selected to correspond to the VCO **226** that is switched-in to the PLL **500**, as indicated by the VCO control signals **239**. More specifically, the control signals **239** turn-on the appropriate P-FET **808** for the gain compensator cell **806** that corresponds to the selected VCO **226**.

In step **1206**, the current scaler **804** generates a reference scale current **812** that is based on a PLL control signal **810**, where the PLL control signal **810** defines certain PLL characteristics including reference frequency, loop bandwidth, and damping factor.

In step **1208**, the switches **902** activate one or more groups **904** of unit current sources **906** according to the capacitor control signals **239**. The groups **904** that are activated correspond to the capacitors **232** that are switched-in to the LC circuit **228**, as indicated by the capacitor control signals **239**. The remaining (non-selected) current sources **906** are cutoff.

In step **1210**, the activated groups **904** replicate (or copy) the reference scale current **812** one or more times, where the number of times that the reference scale current **812** is replicated is dependent on the capacitors **232** that are switched-in to the LC circuit **228**. More specifically, the activated groups **904** replicate the reference scale current enough times to sufficiently compensate the variable VCO gain that is caused by the corresponding capacitors **232**.

In step **1212**, the currents from the activated current sources **906** are added together to generate the charge pump reference current **205**.

In step **1214**, the current scaler **804** adjusts the reference scale current **812** to address changing PLL characteristics, such as reference frequency, loop bandwidth, and damping factor. By adjusting the reference scale current **812**, all of the replicated currents in step **1210** are simultaneously adjusted to address the changing PLL characteristics.

5. Other Applications

The gain compensation invention described herein has been discussed in reference to a tuner application. However, the gain compensation invention is not limited to tuners, and is applicable to other non-tuner applications that can benefit from flat PLL gain. Additionally, the gain compensation invention is applicable to other non-PLL circuits that can benefit from compensating for variable VCO gain. The application of the gain compensation invention to these non-PLL circuits will be understood by those skilled in the relevant arts based on the discussions given herein, and are within the scope and spirit of the present invention.

6. CONCLUSION

Example embodiments of the methods, systems, and components of the present invention have been described herein. As noted elsewhere, these example embodiments have been described for illustrative purposes only, and are not limiting. Other embodiments are possible and are covered by the invention. Such other embodiments will be apparent to persons skilled in the relevant art(s) based on the teachings contained herein. Thus, the breadth and scope of the present invention should not be limited by any of the above-described exemplary embodiments, but should be defined only in accordance with the following claims and their equivalents.

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What is claimed is:

1. A method of compensating the gain of a phase lock loop (PLL), comprising:

receiving a first control signal that is representative of an output frequency of said PLL;

receiving a second control signal that is representative of a characteristic of said PLL; and

generating a charge pump current for said PLL based on said first control signal and said second control signal, wherein said generating comprises:

selecting a charge pump current value from a plurality of charge pump current values based on said first control signal and said second control signal, and converting said selected charge pump current value from a digital value to analog.

2. The method of claim 1, wherein said characteristic of said PLL comprises one of a reference frequency, a loop bandwidth, and a damping factor of said PLL.

3. The method of claim 1, wherein said plurality of charge pump current values correspond to different combinations of characteristics of said PLL.

4. The method of claim 1, wherein said plurality of charge pump current values correspond to different output frequencies of said PLL.

5. The method of claim 1, wherein said plurality of charge pump current values comprise multiple sets of charge pump current values, each set of charge pump current values corresponding to a different output frequency of said PLL.

6. The method of claim 5, wherein individual charge pump current values in said set of charge pump current values correspond to different combination of characteristics of said PLL, but have a common output frequency of said PLL.

7. The method of claim 1, wherein said PLL comprises a voltage controlled oscillator (VCO) comprising a number of capacitors forming a resonant circuit for said VCO, and said first control signal represents a capacitor switched into said resonant circuit of said VCO.

8. The method of claim 7, wherein each of said plurality of charge pump current values is determined so as to compensate for variable VCO gain that occurs when a corresponding capacitor of said number of capacitors is switched into said VCO.

9. A circuit that compensates for the gain of a phase lock loop (PLL), comprising:

means for receiving a first control signal that is representative of an output frequency of said PLL;

means for receiving a second control signal that is representative of a characteristic of said PLL; and

means for generating a charge pump current for said PLL based on said first control signal and said second control signal,

wherein said generating means comprises:

means for selecting a charge pump current value from a plurality of charge pump current values based on said first control signal and said second control signal, and

means for converting said selected charge pump current value from a digital value to analog.

10. The circuit of claim 9, wherein said plurality of charge pump current values correspond to different output frequencies of said PLL.

11. The circuit of claim 9, wherein said plurality of charge pump current values comprise multiple sets of charge pump

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current values, each set of charge pump current values corresponding to a different output frequency of said PLL.

12. The circuit of claim 9, wherein individual charge pump current values in said set of charge pump current values correspond to different combination of characteristics of said PLL, but have a common output frequency of said PLL.

13. The circuit of claim 9, wherein said PLL comprises a voltage controlled oscillator (VCO) comprising a number of capacitors forming a resonant circuit for said VCO, and said first control signal represents a capacitor switched into said resonant circuit of said VCO.

14. The circuit of claim 9, wherein each of said plurality of charge pump current values is determined so as to compensate for variable VCO gain that occurs when a corresponding capacitor of said number of capacitors is switched into said VCO.

15. A gain compensation circuit, comprising:

a memory device; and

a digital-to-analog converter operatively coupled to the memory device,

wherein the memory device receives a first control signal that is representative of an output frequency of a phase lock loop (PLL),

wherein the memory device receives a second control signal that is representative of a characteristic of the PLL,

wherein the memory device selects a charge pump current value from a plurality of charge pump current values based on the first control signal and the second control signal, and

wherein the digital-to-analog converter converts the selected charge pump current value from a digital value into an analog charge pump current.

16. The gain compensation circuit according to claim 15, wherein the plurality of charge pump current values correspond to different output frequencies of the PLL.

17. The circuit gain compensation circuit according to claim 15, wherein the plurality of charge pump current values comprise multiple sets of charge pump current values, each set of charge pump current values corresponding to a different output frequency of the PLL.

18. The circuit gain compensation circuit according to claim 15, wherein individual charge pump current values in the set of charge pump current values correspond to different combinations of characteristics of the PLL, but have a common output frequency of the PLL.

19. The circuit gain compensation circuit according to claim 15,

wherein the PLL comprises a voltage controlled oscillator (VCO) that comprises a number of capacitors forming a resonant circuit for the VCO, and

wherein the first control signal represents a capacitor switched into the resonant circuit of the VCO.

20. The circuit gain compensation circuit according to claim 15, wherein each of the plurality of charge pump current values is determined so as to compensate for variable VCO gain that occurs when a corresponding capacitor of the number of capacitors is switched into the VCO.

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